

2018 Annual Groundwater Monitoring and Corrective Action Report

CCR Landfill

***R.M. Heskett Station
Mandan, North Dakota***

Prepared for
Montana-Dakota Utilities Co.

January 2019



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Mandan, North Dakota

January 31, 2019

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Acronyms

Acronym	Description
ASD	Alternative Source Demonstration
CCR	Coal Combustion Residuals
CFR	Code of Federal Regulations
MDU	Montana Dakota Utilities Co.
SSI	Statistically Significant Increase
TDF	Tire-derived fuel
TDS	Total dissolved solids

1.0 Introduction

MDU owns and operates R.M. Heskett Station, a coal-fired generating station and a gas fired turbine located in Mandan, North Dakota (Figure 1). One CCR landfill, as defined by 40 CFR 257.53, is located on the property. Wastes contained in the CCR landfill primarily consist of coal combustion by-products, asbestos wastes generated from construction activity associated with MDU-owned facilities, and ash derived from the burning of TDF at the facility.

This 2018 Annual Groundwater Monitoring and Corrective Action Report (Annual Report) describes the monitoring program and results for the CCR landfill at MDU's R.M. Heskett Station (Site).

1.1 Purpose

As stated in Section §257.90 (e), the Annual Report must:

- Document the status of groundwater monitoring and any corrective action programs for the CCR unit,
- Summarize key actions completed,
- Describe any problems encountered,
- Discuss actions to resolve the problems, and
- Project key activities for the upcoming year.

1.2 CCR Rule Requirements

Additional requirements for the Annual Report, as outlined in §257.90 (e) of the CCR Rule and this Site's compliance with the CCR Rule, are summarized in Table 1.

Table 1 CCR Rule Requirements and Compliance

CCR Rule Reference	Content Required in Report	Location
§257.90(e)(1)	Monitoring System Figure: A map, aerial image, or diagram showing the CCR unit and all background (or upgradient) and downgradient monitoring wells, to include the well identification numbers, that are part of the groundwater monitoring program for the CCR unit;	Section 2.1 Groundwater Monitoring System; see Figure 1.
§257.90(e)(2)	Monitoring System Adjustments: Identification of any monitoring wells that were installed or decommissioned during the preceding year, along with a narrative description of why those actions were taken;	Section 2.1 Groundwater Monitoring System
§257.90(e)(3)	Data and Collection Summary: In addition to all the monitoring data obtained under §257.90 through §257.98, a summary including the number of groundwater samples that were collected, and whether the sample was required by the detection monitoring or assessment monitoring programs;	Section 2.3 Monitoring and Analytical Results
§257.90(e)(4)	Monitoring Program: A narrative discussion of any transition between monitoring programs (e.g. the date and circumstances for transitioning from detection monitoring to assessment monitoring in addition to identifying the constituent(s) detected at a statistically significant increase over background levels); and	Section 2.3 Monitoring and Analytical Results
§257.90(e)(5)	<p>Other Information: Other information required, if applicable, to be included in the annual report as specified in §257.90 through §257.98.</p> <ul style="list-style-type: none"> - Alternative Monitoring Frequency Demonstration (§257.94(d) and §257.95 (c)(3)) - Appendix III Alternative Source Demonstration Report (§257.94(e)(2)) - Assessment Monitoring Results and Discussion (§257.95(d)(3)) - Appendix IV Alternative Source Demonstration Report (§257.95(g)(3)(ii)) - Demonstration for Additional Time for Assessment or Corrective Measures (§257.96(a)) 	Section 2.3 Monitoring and Analytical Results

2.0 Groundwater Monitoring Program

This section documents the status of the groundwater monitoring and corrective action program for the CCR unit in 2018. The groundwater monitoring system is described in Section 2.1, key actions completed and problems encountered are described in Section 2.2, the monitoring and analytical results are described in Section 2.3, and key activities planned for 2019 are described in Section 2.4.

2.1 Groundwater Monitoring System

The groundwater monitoring system is consistent with the Groundwater Monitoring System Certification (Barr, 2017a); no adjustments or changes were made to the groundwater monitoring system in 2018.

2.2 Actions Completed/Problems Encountered

The following actions were completed in 2018:

- **Detection Monitoring Sampling:** Groundwater samples were collected from each well in the groundwater monitoring system on April 2-4, 2018 and October 1-4, 2018; samples were analyzed for Appendix III constituents, per the detection monitoring program of the CCR Rule (§257.94).
- **SSI Evaluation:** SSI evaluations were conducted in accordance with the Groundwater Statistical Method Selection Certification (Statistical Certification; Barr, 2017b) for the October 2017 and April 2018 detection monitoring events, both of which resulted in potential SSIs.
- **Verification Retesting:** Retesting was conducted, per the Statistical Certification (Barr, 2017b) on the potential SSIs for the October 2017 detection monitoring event (in January 2018) and April 2018 detection monitoring event (in August 2018). All SSIs were verified.
- **Alternative Source Demonstration (ASD):** ASDs were conducted on the verified SSIs for the October 2017 and April 2018 detection monitoring events. Both ASDs were able to demonstrate an alternative source, as allowed by the CCR rule (§257.94(e)(2)). More details are provided in Section 2.4.

During the October 2018 sampling event, no sample was collected from MW3-90 due to the water level being located below the base of the dedicated pump (situated approximately two feet above the bottom of the well to minimize turbidity issues). Historically, water levels have been recorded lower than the current base of the pump (prior to installation), but not with any consistency. However, if this problem persists, the dedicated pump may be lowered. No other problems were encountered during the report period.

2.3 Data and Collection Summary

2.3.1 October 2017 Detection Monitoring Event

As mentioned in the 2017 Annual Report, an SSI evaluation was to be conducted on the results of the October 2017 detection monitoring event. Four potential SSIs (pH at MW-80R, chloride at MW-105, and sulfate and TDS at MW-104) were identified and subsequently verified through retesting conducted on

January 22, 2018, per our Statistical Certification. Field data sheets and analytical laboratory reports for detection monitoring sampling and verification resampling are included in Appendix A.

An Appendix III ASD was conducted on the verified SSIs and was able to successfully demonstrate that a “source other than the CCR unit” caused the SSIs, that the SSIs resulted from analytical error, or natural variations in groundwater quality, as allowed by §257.94(e)(4). The Alternative Source Demonstration: October 2017 Event Report is included in Appendix B.

2.3.2 April 2018 Detection Monitoring Event

Groundwater samples were collected from all 12 monitoring wells at the Site on April 2, 3, and 4, 2018. Four potential SSIs (fluoride at MW2-90, chloride at MW-105, and sulfate and TDS at MW-104) were identified and subsequently verified through resampling on August 13, 2018. Field data sheets and analytical laboratory reports for detection monitoring sampling and verification resampling are included in Appendix A.

An Appendix III ASD Report was prepared for the verified SSIs and as reported, a “source other than the CCR unit” caused the SSIs. The SSIs resulted from analytical error, or natural variations in groundwater quality, as allowed by §257.94(e)(4). The Alternative Source Demonstration: April 2018 Event is included in Appendix B.

2.3.3 October 2018 Detection Monitoring Event

Groundwater samples were collected from 11 monitoring wells at the Site on October 1, 2, 3, and 4, 2018. No sample was collected from MW3-90 due to the water level being located below the base of the dedicated pump. Field data sheets and analytical laboratory reports for detection monitoring sampling are included in Appendix A.

2.4 Activities for Upcoming Year

No significant events are planned for 2019 other than semi-annual detection monitoring per the CCR Rule.

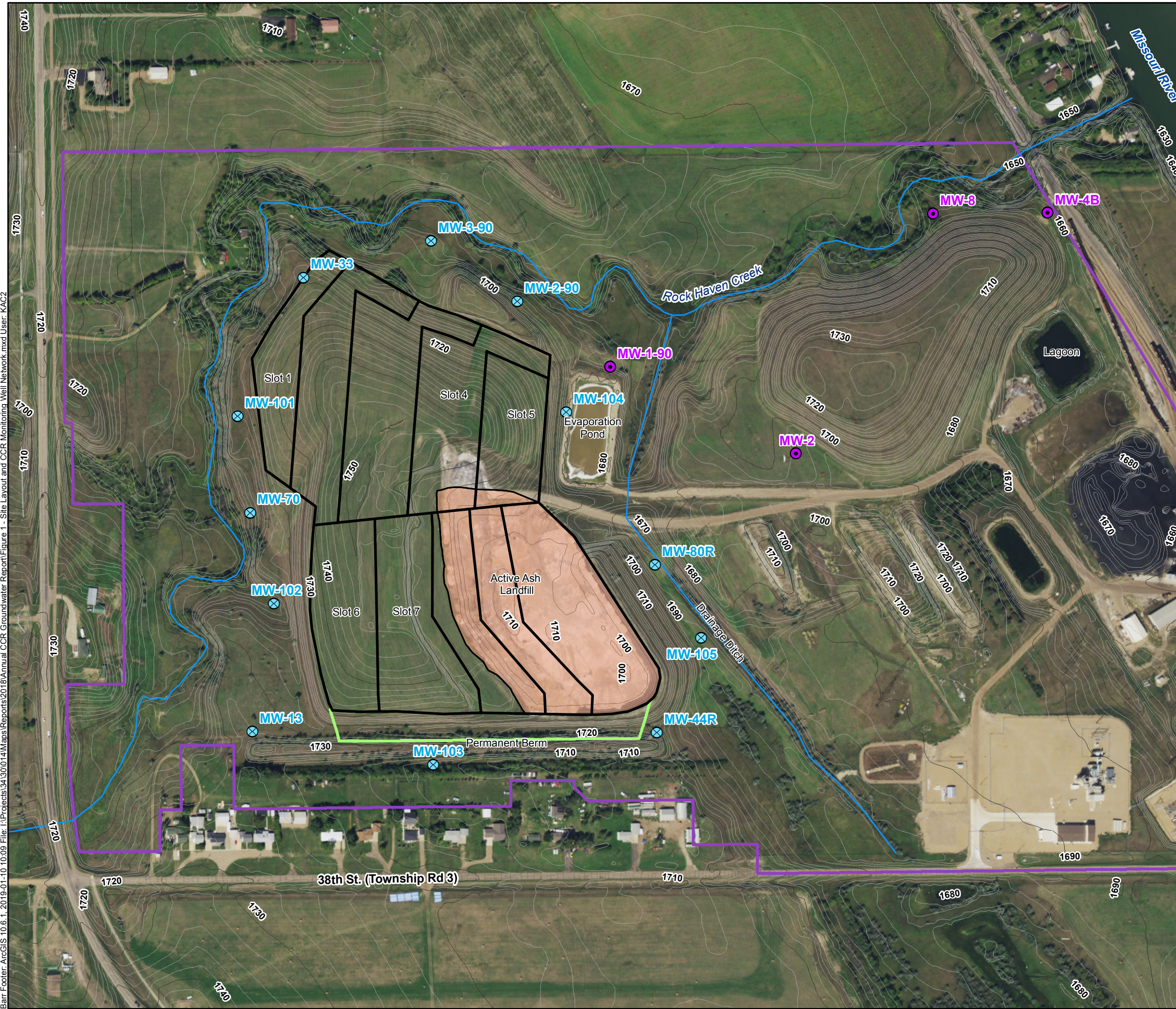
3.0 References

Barr Engineering Co. (Barr), 2017a, Groundwater Monitoring System Certification, October 2017.

Barr, 2017b, Statistical Method Selection Certification, October 2017.

Figures

Barr Footer: ArcGIS 10.6.1, 2019-01-10 10:09 File: I:\Projects\34130014\Maps\Reports\2018\Annual CCR Groundwater Report\Figure 1 - Site Layout and CCR Monitoring Well Network.mxd User: KAC2



- Monitoring Well Location
- Monitoring Well Location - Water Level Only
- Existing Slot Boundaries
- Streams
- Property Line
- Future Landfill Boundary
- 10ft Contours
- 2ft Contours
- Active Portion of Landfill

Image Source: 2017 Statewide Imagery (ND GIS Hub)

CAD Data Source: Slot Linework.dwg

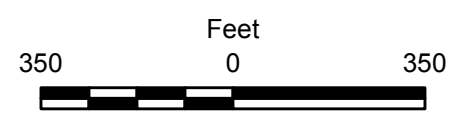


Figure 1

**SITE LAYOUT AND CCR
MONITORING WELL NETWORK**
R. M. Heskett Station
2018 CCR Groundwater Monitoring Report
Montana Dakota Utilities
Mandan, North Dakota

Appendix A

Laboratory Reports and Field Sheets



January 24, 2018

Montana Dakota Utilities
Attn: Samantha Marshall
400 N. 4th St.
Bismarck, ND 58501

RE: Groundwater Sampling Event - MDU Heskett Ash Site

Dear Ms. Marshall:

On January 22, 2018, MVTL Laboratories' Field Services division collected groundwater samples at the MDU Heskett site near Mandan, ND for the Heskett Coal Combustion Rule Appendix III.

4 wells were purged and sampled during this event. Wells were located and were found to be in generally good condition. The wells for CCR were purged and sampled using a dedicated bladder pump and BARR's SOP for low flow purging and sampling. The samples collected were, placed on ice and transported back to the MVTL laboratory in Bismarck, ND for analysis. The field data report for the sampling event accompanies this letter.

Thank you for your trust and support of our services. If you have any questions, please call me at (800) 279-6885.

Sincerely,

Jeremy Meyer
MVTL Field Services



Field Data Report

MDU Heskett
GROUNDWATER SAMPLING
Attn: Samantha Marshall
400 N. 4th St
Bismarck, ND 58501
701-222-7829

WO# 82-0130

WELL ID	PURGE DATE	START PURGE TIME	SAMPLE DATE	TIME OF SAMPLE	WELL CASING ELEVATION	STATIC WATER LEVEL (ft)	WATER LEVEL START	WATER LEVEL END	VOLUME REMOVED (mL)	SAMPLE METHOD	TEMP (°C)	EC	pH	Turbidity NTU	SAMPLE APPEARANCE OR COMMENT
80R	22-Jan-18	11:03	22-Jan-18	11:43	NA	NA	13.74	13.97	4000.0	Bladder	6.29	5698	7.12	4.39	clear
44R	22-Jan-18	9:02	22-Jan-18	9:37	NA	NA	26.82	26.93	3500.0	Bladder	6.48	9251	6.58	2.33	clear
104	22-Jan-18	10:05	22-Jan-18	10:45	NA	NA	13.76	14.00	4000.00	Bladder	6.16	14348	6.94	1.28	clear
105	22-Jan-18	12:18	22-Jan-18	13:03	NA	NA	11.88	NR	4500.0	Bladder	5.07	7048	6.76	1.45	clear

NR = Not Recorded on Field Sheet NA = Not Applicable



Field Datasheet

Groundwater Assessment

2616 E. Broadway Ave, Bismarck, ND
Phone: (701) 258-9720

Company: MDU Heskett
Event: January 2018
Sample ID: 44R
Sampling Personal: Parren Nierway

Weather Conditions: Temp: 14 °F Wind: west @ 6 Precip: Sunny / Partly Cloudy / Cloudy

Well Information

Well Locked?	Yes <input checked="" type="checkbox"/>	No <input type="checkbox"/>	
Well Labeled?	Yes <input checked="" type="checkbox"/>	No <input type="checkbox"/>	
Casing Straight?	Yes <input checked="" type="checkbox"/>	No <input type="checkbox"/>	
Grout Seal Intact?	Yes <input checked="" type="checkbox"/>	No <input type="checkbox"/>	Not Visible
Repairs Necessary:			
Casing Diameter:	2"		
Water Level Before Purge:	26.82		ft
Depth to Top of Pump:	35.16		ft
Water Level After Sample:	26.93		ft
Measurement Method:	Electric Water Level Indicator		

Sampling Information

Purging Method:	Bladder		Control Settings
Sampling Method:	Bladder		
Dedicated Equip?:	Yes <input checked="" type="checkbox"/>	No <input type="checkbox"/>	
Duplicate Sample?:	Yes <input type="checkbox"/>	No <input checked="" type="checkbox"/>	
Duplicate Sample ID:			
Purge Date:	22 Jan 18	Time Purging Began:	0902 am/pm
Well Purged Dry?	Yes <input checked="" type="checkbox"/>	No <input type="checkbox"/>	Time Purged Dry:
Sample Date:	22 Jan 18	Time of Sampling:	0937 am/pm
Bottle List:	1L Raw 500mL Nitric		

Field Measurements

Stabilization (3 consecutive)	Temp (°C)	Spec. Cond.	pH	DO (mg/L)	ORP (mV)	Turbidity (NTU)	Water Level (ft)	Pumping Rate	mL Removed	Description:	
SEQ #	Time	±5%	±0.1	±10%	±20 mV	±10%	0.25 ft	ml/min		Clarity, Color, Odor, Ect. Clear, Slightly Turbid, Turbid	
1	0907	5.28	9338	6.59	5.05	53.2	5.83	26.89	100	500	clear
2	0912	5.22	9325	6.59	2.37	49.6	3.49	26.88	100	500	clear
3	0917	4.67	9339	6.60	6.22	49.4	2.16	26.88	100	500	clear
4	0922	0.96	9459	6.64	4.68	52.0	2.29	26.90	100	500	clear
5	0927	2.33	9296	6.62	4.92	50.0	2.55	26.93	100	500	clear
6	0932	6.22	9286	6.59	4.87	49.5	2.35	26.93	100	500	clear
7	0937	6.48	9251	6.58	4.91	49.5	2.33	26.93	100	500	clear
8											
9											
10											

Stabilized: Yes No

Total Volume Removed: 3500 mL

Comments: At 0922 line was freezing w/ had to unthaw.



Field Datasheet

Groundwater Assessment

2616 E. Broadway Ave, Bismarck, ND
Phone: (701) 258-9720

Company: MDU Heskett
Event: January 2018
Sample ID: 80R
Sampling Personal: Darren Nieswaag

Weather Conditions: Temp: 18 °F Wind: west @ 5 Precip: Sunny / Partly Cloudy / Cloudy

Well Information

Well Locked?	Yes	<input checked="" type="radio"/> No	
Well Labeled?	<input checked="" type="radio"/> Yes	No	
Casing Straight?	<input checked="" type="radio"/> Yes	No	
Grout Seal Intact?	<input checked="" type="radio"/> Yes	No	Not Visible
Repairs Necessary:	—		
Casing Diameter:	2"		
Water Level Before Purge:	13.74 ft		
Depth to Top of Pump:	19.30 ft		
Water Level After Sample:	13.97 ft		
Measurement Method:	Electric Water Level Indicator		

Sampling Information

Purging Method:	Bladder		Control Settings	
Sampling Method:	Bladder		Purge:	3 sec.
Dedicated Equip?:	<input checked="" type="radio"/> Yes	No	Recover:	27 sec.
Duplicate Sample?:	<input checked="" type="radio"/> Yes	No	PSI:	—
Duplicate Sample ID:	Dup-1			
Purge Date:	22 Jan 18	Time Purging Began:	1103	am/pm
Well Purged Dry?	Yes	<input checked="" type="radio"/> No	Time Purged Dry:	— am/pm
Sample Date:	22 Jan 18	Time of Sampling:	1143	am/pm
Bottle List:	1L Raw 1- 500mL Nitric			

Field Measurements

SEQ #	Stabilization (3 consecutive) Time	Temp (°C)	Spec. Cond. ±5%	pH ±0.1	DO (mg/L) ±10%	ORP (mV) ±20 mV	Turbidity (NTU) ±10%	Water Level (ft) 0.25 ft	Pumping Rate ml/min	mL Removed	Description:
											Clarity, Color, Odor, Ect. Clear, Slightly Turbid, Turbid
1	1108	7.20	5684	7.13	6.63	51.9	5.31	13.97	100	500	clear
2	1113	6.03	5709	7.14	4.87	51.9	2.31	14.03	100	500	clear
3	1118	5.56	5707	7.12	3.20	51.4	2.04	13.99	100	500	clear
4	1123	5.69	5709	7.12	1.81	51.4	2.31	13.99	100	500	clear
5	1128	5.59	5709	7.12	1.00	51.4	2.22	13.99	100	500	clear
6	1133	5.65	5711	7.12	1.05	51.3	4.74	13.99	100	500	clear
7	1138	5.94	5708	7.12	1.13	51.4	4.60	13.97	100	500	clear
8	1143	6.29	5698	7.12	1.03	51.4	4.39	13.97	100	500	clear
9											
10											

Stabilized: Yes No
Comments:

Total Volume Removed: 4000 mL



Field Datasheet

Groundwater Assessment

2616 E. Broadway Ave, Bismarck, ND
Phone: (701) 258-9720

Company: MDU Heskett
Event: January 2018
Sample ID: 104
Sampling Personal: Darren Niesway

Weather Conditions: Temp: 14 °F Wind: West @ 6 Precip: Sunny / Partly Cloudy / Cloudy

Well Information

Well Locked?	Yes	<u>No</u>	
Well Labeled?	<u>Yes</u>	No	
Casing Straight?	<u>Yes</u>	No	
Grout Seal Intact?	<u>Yes</u>	No	Not Visible
Repairs Necessary:	-		
Casing Diameter:	2"		
Water Level Before Purge:	13.76 ft		
Depth to Top of Pump:	-		
Water Level After Sample:	14.00 ft		
Measurement Method:	Electric Water Level Indicator		

Sampling Information

Purging Method:	Bladder		Control Settings	
Sampling Method:	Bladder		Purge:	3 sec.
Dedicated Equip?:	<u>Yes</u>	No	Recover:	27 sec.
Duplicate Sample?:	Yes	<u>No</u>	PSI:	-
Duplicate Sample ID:	-			
Purge Date:	22 Jan 18	Time Purging Began:	1005	am/pm
Well Purged Dry?	Yes	<u>No</u>	Time Purged Dry:	- am/pm
Sample Date:	22 Jan 18	Time of Sampling:	1045	am/pm
Bottle List:	1L Raw 500mL Nitric			

Field Measurements

Stabilization (3 consecutive)	Temp (°C)	Spec. Cond. ±5%	pH ±0.1	DO (mg/L) ±10%	ORP (mV) ±20 mV	Turbidity (NTU) ±10%	Water Level (ft) 0.25 ft	Pumping Rate ml/min	mL Removed	Description: Clarity, Color, Odor, Ect. Clear, Slightly Turbid, Turbid	
1	1010	6.01	14340	6.95	4.82	51.7	6.23	13.97	100	500	cl
2	1015	6.12	14337	6.95	3.95	51.8	3.43	13.97	100	500	cl
3	1020	5.67	14288	6.95	3.02	51.5	2.11	13.97	100	500	cl
4	1025	5.89	14313	6.95	3.68	51.9	1.41	13.97	100	500	cl
5	1030	6.04	14325	6.95	4.97	52.1	1.31	14.02	100	500	cl
6	1035	6.02	14323	6.94	1.71	51.9	1.34	14.02	100	500	cl
7	1040	6.18	14343	6.95	1.86	52.2	1.21	14.05	100	500	cl
8	1045	6.16	14348	6.94	1.81	52.2	1.28	14.05	100	500	cl
9											
10											

Stabilized: Yes No
Comments:

Total Volume Removed: 4000 mL



Field Datasheet

Groundwater Assessment

2616 E. Broadway Ave, Bismarck, ND
Phone: (701) 258-9720

Company: MDU Heskett
Event: January 2018
Sample ID: 105
Sampling Personal: Darren Nieswaag

Weather Conditions: Temp: 23 °F Wind: West @ 5 Precip: Sunny / Partly Cloudy / Cloudy

Well Information

Well Locked?	Yes <input checked="" type="checkbox"/> No <input checked="" type="checkbox"/>	
Well Labeled?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	
Casing Straight?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	
Grout Seal Intact?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	Not Visible
Repairs Necessary:		
Casing Diameter:	2"	
Water Level Before Purge:	11.88	ft
Depth to Top of Pump:	21.24	ft
Water Level After Sample:		ft
Measurement Method:	Electric Water Level Indicator	

Sampling Information

Purging Method:	Bladder		Control Settings	
Sampling Method:	Bladder		Purge:	3 sec.
Dedicated Equip?:	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>		Recover:	27 sec.
Duplicate Sample?:	Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>		PSI:	-
Duplicate Sample ID:				
Purge Date:	22 Jan 18	Time Purging Began:	12:18	am/pm
Well Purged Dry?	Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>	Time Purged Dry:		am/pm
Sample Date:	22 Jan 18	Time of Sampling:	1303	am/pm
Bottle List:	1L Raw 500mL Nitric			

Field Measurements

Stabilization (3 consecutive)	Temp (°C)	Spec. Cond. ±5%	pH ±0.1	DO (mg/L) ±10%	ORP (mV) ±20 mV	Turbidity (NTU) ±10%	Water Level (ft) 0.25 ft	Pumping Rate ml/min	mL Removed	Description: Clarity, Color, Odor, Ect. Clear, Slightly Turbid, Turbid	
1	1223	4.50	6442	6.82	0.98	53.0	2.72	11.96	100	500	clear
2	1228	4.95	6117	6.81	1.47	53.0	1.70	11.98	100	500	clear
3	1233	5.71	6071	6.79	3.35	52.0	2.12	11.98	100	500	clear
4	1238	5.29	6186	6.79	2.25	52.1	1.41	11.98	100	500	clear
5	1243	5.61	6445	6.78	2.68	52.1	1.07	12.00	100	500	clear
6	1248	5.72	6558	6.77	2.74	52.0	1.15	12.00	100	500	clear
7	1253	5.08	6813	6.76	0.72	52.6	1.58	12.03	100	500	clear
8	1258	5.61	6923	6.76	0.74	52.3	1.47	12.03	100	500	clear
9	1303	5.07	7048	6.76	0.75	52.6	1.45	12.03	100	500	clear
10											

Stabilized: Yes No
Comments: * 8N 22 Jan 18 A

Total Volume Removed: 4500 mL



CASE NARRATIVE

MVTL Lab Reference No/SDG: 201882-0130
Client: Montana Dakota Utilities
Location: MDU Heskett
Project Identification: CCR January 2018
MVTL Laboratory Identifications: 18-W101 through 18-W106
Page 1 of 1

Table with 2 columns: MDU Sample Identification, MVTL Laboratory #. Rows include 44R, 80R, 104, 105, Dup1, FB1.

I. RECEIPT

- All samples were received at the laboratory on 23 Jan 18 at 1358.
Samples were collected and hand delivered by MVTL Field Service personnel to the laboratory.
Samples were received on ice and evidence of cooling had begun.
Temperature of samples upon receipt was 6.1°C.
All samples were properly preserved unless noted here and/or flagged on the individual analytical laboratory report.
No other exceptions on sample receipt were encountered on this sample set unless noted here.

II. HOLDING TIMES

- With the exception of pH, all holding times were met for both preparation and analysis unless noted here.

III. METHODS

- Approved methodology was followed for all sample analyses.

IV. ANALYSIS

- All acceptance criteria was met for calibration, method blanks, laboratory control samples, laboratory fortified matrix/matrix duplicates unless noted here and/or flagged on the individual analytical laboratory report.

All laboratory data has been approved by MVTL Laboratories.

SIGNED: Claudette Carroll DATE: 1 FEB 18
Claudette Carroll - MVTL Bismarck Laboratory Manager



MINNESOTA VALLEY TESTING LABORATORIES, INC.

1126 N. Front St. ~ New Ulm, MN 56073 ~ 800-782-3557 ~ Fax 507-359-2890
2616 E. Broadway Ave. ~ Bismarck, ND 58502 ~ 800-279-6885 ~ Fax 701-258-9724
1201 Lincoln Highway ~ Nevada, IA 50201 ~ 800-362-0855 ~ Fax 515-382-3885
www.mvttl.com

MEMBER
ACIL

Page: 1 of 1

Quality Control Report

Lab IDs: 18-W101 to 18-W106

Project: MDU Heskett

Work Order: 201882-0130

Analyte	LCS Spike Amt	LCS Rec %	LCS % Rec Limits	Matrix Spike Amt	Matrix Spike ID	Matrix Spike Orig Result	Matrix Spike Result	Matrix Spike Rec %	Matrix Spike % Rec Limits	MSD/ Dup Orig Result	MSD/ Dup Result	MSD Rec %	MSD/ Dup RPD	MSD/ Dup RPD Limit (<)	Known Rec (%)	Known % Rec Limits	Method Blank
Boron - Total mg/l	0.40	102	80-120	2.00	18-W101	0.56	2.34	89	75-125	2.34	2.31	88	1.3	20	-	-	< 0.1 < 0.1
Calcium - Total mg/l	20.0	110	80-120	500	18W101q	456	945	98	75-125	945	950	99	0.5	20	-	-	< 1 < 1
Chloride mg/l	30.0 30.0	91 92	80-120 80-120	30.0	18-W71	37.2	69.1	106	80-120	69.1	68.3	104	1.2	20	-	-	< 1 < 1
Fluoride mg/l	0.50 0.50	104 106	90-110 90-110	0.500	18-W101	0.66	1.09	86	80-120	1.09	1.09	86	0.0	20	-	-	< 0.1 < 0.1
pH units	-	-	-	-	-	-	-	-	-	7.3	7.3	-	0.0	20	-	-	-
Sulfate mg/l	100	105	80-120	100	18-W93	72.6	162	89	80-120	162	164	91	1.2	20	-	-	< 5
Total Dissolved Solids mg/l	- - -	- - -	- - -	- - -	- - -	- - -	- - -	- - -	- - -	655 381 < 10	636 384 < 10	- - -	2.9 0.8 0.0	20 20 20	- - -	- - -	< 10

Approved by: C. Cawley
1 FEB 18



MINNESOTA VALLEY TESTING LABORATORIES, INC.

1126 North Front St. ~ New Ulm, MN 56073 ~ 800-782-3557 ~ Fax 507-359-2890
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CERTIFICATE of ANALYSIS - CCR

Samantha Marshall
Montana Dakota Utilities
400 N 4th St
Bismarck ND 58501

Report Date: 30 Jan 18
Lab Number: 18-W105
Work Order #: 82-0130
Account #: 002800
Date Sampled: 22 Jan 18
Date Received: 22 Jan 18 13:58
Sampled By: MVTL Field Services

Project Name: MDU Heskett
Sample Description: Dupl

Temp at Receipt: 6.1C ROI

Event and Year: January 2018

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
Metal Digestion				EPA 200.2	22 Jan 18	SVS
pH	* 7.3	units	0.1	SM4500 H+ B	22 Jan 18 17:00	SVS
Fluoride	0.32	mg/l	0.10	SM4500-F-C	22 Jan 18 17:00	SVS
Sulfate	3180	mg/l	5.00	ASTM D516-07	25 Jan 18 16:06	RAG
Chloride	159	mg/l	1.0	SM4500-Cl-E	23 Jan 18 14:41	RAG
Total Dissolved Solids	5100	mg/l	10	I1750-85	24 Jan 18 9:14	SVS
Calcium - Total	287	mg/l	1.0	6010D	29 Jan 18 14:20	SZ
Boron - Total	< 0.5 @	mg/l	0.10	6010D	26 Jan 18 15:33	SZ

* Holding time exceeded

Approved by:

Claudette K. Carroll ^{cc} 1/25/18

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

The reporting limit was elevated for any analyte requiring a dilution as coded below:

@ = Due to sample matrix # = Due to concentration of other analytes
! = Due to sample quantity + = Due to internal standard response

CERTIFICATION: ND # ND-00016



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CERTIFICATE of ANALYSIS - CCR

Samantha Marshall
Montana Dakota Utilities
400 N 4th St
Bismarck ND 58501

Report Date: 30 Jan 18
Lab Number: 18-W106
Work Order #: 82-0130
Account #: 002800
Date Sampled: 22 Jan 18
Date Received: 22 Jan 18 13:58
Sampled By: MVTL Field Services

Project Name: MDU Heskett
Sample Description: FB1

Temp at Receipt: 6.1C ROI

Event and Year: January 2018

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
Metal Digestion				EPA 200.2	22 Jan 18	SVS
pH	* 6.2	units	0.1	SM4500 H+ B	22 Jan 18 17:00	SVS
Fluoride	< 0.1	mg/l	0.10	SM4500-F-C	22 Jan 18 17:00	SVS
Sulfate	< 5	mg/l	5.00	ASTM D516-07	25 Jan 18 16:06	RAG
Chloride	< 1	mg/l	1.0	SM4500-Cl-E	23 Jan 18 14:41	RAG
Total Dissolved Solids	< 10	mg/l	10	I1750-85	24 Jan 18 9:14	SVS
Calcium - Total	< 1	mg/l	1.0	6010D	29 Jan 18 14:20	SZ
Boron - Total	< 0.1	mg/l	0.10	6010D	26 Jan 18 15:33	SZ

* Holding time exceeded

Approved by:

Claudette K. Carroll ^{CC} 1/25/18

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

The reporting limit was elevated for any analyte requiring a dilution as coded below:

@ = Due to sample matrix # = Due to concentration of other analytes
! = Due to sample quantity + = Due to internal standard response

CERTIFICATION: ND # ND-00016



Laboratories, Inc.

2616 E. Broadway
Bismarck, ND 58501
Phone (701) 258-9720

Chain of Custody Record

Project Name: MDU Heskett	Event: January 2018	Work Order Number: 82-0130
Report To: MDU Attn: Samantha Marshall Address: 400 N. 4th St Bismarck, ND 58501 phone: 701-222-7829 email:	Carbon Copy: Attn: Address:	Name of Sampler(s): <i>Darren Nieswaag</i>

Sample Information					Bottle Type			Field Parameters			Analysis
Lab Number	Sample ID	Date	Time	Sample Type	1 liter	500mL Nitric	500mL Nitric (filtered)	Temp (°C)	Spec. Cond.	PH	Analysis Required
<i>W101</i>	44R	<i>22 Jan 18</i>	<i>0937</i>	GW	X	X		<i>6.48</i>	<i>9251</i>	<i>6.58</i>	MDU Appendix 3 List
<i>W102</i>	80R	<i>22 Jan 18</i>	<i>1143</i>	GW	X	X		<i>6.29</i>	<i>5698</i>	<i>7.12</i>	
<i>W103</i>	104	<i>22 Jan 18</i>	<i>1045</i>	GW	X	X		<i>6.16</i>	<i>14348</i>	<i>6.94</i>	
<i>W104</i>	105	<i>22 Jan 18</i>	<i>1303</i>	GW	X	X		<i>5.07</i>	<i>7048</i>	<i>6.76</i>	
<i>W105</i>	Dup1	<i>22 Jan 18</i>	<i>-</i>	GW	X	X		<i>-</i>	<i>-</i>	<i>-</i>	
<i>W106</i>	FB1	<i>22 Jan 18</i>	<i>-</i>	GW	X	X		<i>-</i>	<i>-</i>	<i>-</i>	

Comments:

Relinquished By:		Sample Condition:	
Name:	Date/Time	Location:	Temp (°C)
<i>Darren Nieswaag</i>	<i>22 Jan 18</i> <i>1358</i>	<i>Log In</i> Walk In #2	<i>ROF 6.1</i> TM562 TM588
1			
2			

Received by:	
Name:	Date/Time
<i>N. Buchmann</i>	<i>22 Jan 18</i> <i>1358</i>



CASE NARRATIVE

MVTL Lab Reference No/SDG: 201882-0637
Client: Montana Dakota Utilities
Location: MDU Heskett
Project Identification: CCR April 2018
MVTL Laboratory Identifications: 18-W453 through 18-W460
Page 1 of 2

MDU Sample Identification	MVTL Laboratory #
13	18-W453
Dup1	18-W454
102	18-W455
70	18-W456
101	18-W457
103	18-W458
44R	18-W459
FB1	18-W460

I. RECEIPT

- All samples were received at the laboratory on 4 Apr 18 at 0800.
- Samples were collected and hand delivered by MVTL Field Service personnel to the laboratory.
- Samples were received on ice and evidence of cooling had begun.
 - Temperature of samples upon receipt was 1.6°C.
- All samples were properly preserved unless noted here and/or flagged on the individual analytical laboratory report.
- No other exceptions on sample receipt were encountered on this sample set unless noted here.

II. HOLDING TIMES

- With the exception of pH, all holding times were met for both preparation and analysis unless noted here.

III. METHODS

- Approved methodology was followed for all sample analyses.



CASE NARRATIVE

MVTL Lab Reference No/SDG: 201882-0637
Client: Montana Dakota Utilities
Location: MDU Heskett
Project Identification: CCR April 2018
MVTL Laboratory Identifications: 18-W453 through 18-W460
Page 2 of 2

IV. ANALYSIS

- All acceptance criteria was met for calibration, method blanks, laboratory control samples, laboratory fortified matrix/matrix duplicates unless noted here and/or flagged on the individual analytical laboratory report.
 - For some analytes, the reported results were elevated due to additional dilutions required to minimize the effects of sample matrix.

All laboratory data has been approved by MVTL Laboratories.

SIGNED: Claudette Carroll DATE: 26 April 18
Claudette Carroll - MVTL Bismarck Laboratory Manager

Quality Control Report

Lab IDs: 18-W453 to 18-W460

Project: MDU Heskett Active Ash

Work Order: 201882-0637

Analyte	LCS Spike Amt	LCS Rec %	LCS % Rec Limits	Matrix Spike Amt	Matrix Spike ID	Matrix Spike Orig Result	Matrix Spike Result	Matrix Spike Rec %	Matrix Spike % Rec Limits	MSD/ Dup Orig Result	MSD/ Dup Result	MSD Rec %	MSD/ Dup RPD	MSD/ Dup RPD Limit (<)	Known Rec (%)	Known % Rec Limits	Method Blank
Boron - Total mg/l	0.40	95	80-120	0.400	18-D999	< 0.1	0.41	102	75-125	0.41	0.42	105	2.4	20	-	-	< 0.1
	0.40	105	80-120	0.400	18-D1035	< 0.1	0.39	98	75-125	0.39	0.40	100	2.5	20	-	-	< 0.1
	0.40	108	80-120	2.00	18-W453	0.66	2.38	86	75-125	2.38	2.42	88	1.7	20	-	-	< 0.1
				0.400	18-W460	< 0.1	0.38	95	75-125	0.38	0.38	95	0.0	20	-	-	< 0.1
Calcium - Total mg/l	20.0	108	80-120	500	18M633q	1000	1460	92	75-125	1460	1420	84	2.8	20	-	-	< 1
	20.0	112	80-120	500	18W454q	402	870	94	75-125	870	870	94	0.0	20	-	-	< 1
				500	18W455q	445	915	94	75-125	915	905	92	1.1	20	-	-	< 1
Chloride mg/l	30.0	101	80-120	30.0	18-W453	77.3	106	96	80-120	106	105	92	0.9	20	-	-	< 1
	30.0	101	80-120	30.0	18-W460	< 1	28.8	96	80-120	28.8	29.1	97	1.0	20	-	-	< 1
	30.0	101	80-120												-	-	< 1
Fluoride mg/l	0.50	100	90-110	0.500	18-M631	2.55	3.08	106	80-120	3.08	3.06	102	0.7	20	-	-	< 0.1
				0.500	18-W456	0.30	0.82	104	80-120	0.82	0.82	104	0.0	20	-	-	< 0.1
pH units	-	-	-	-	-	-	-	-	-	7.3	7.4	-	1.4	20	-	-	-
	-	-	-	-	-	-	-	-	-	7.2	7.2	-	0.0	20	-	-	-
Sulfate mg/l	100	102	80-120	100	18-W460	< 5	96.6	97	80-120	96.6	93.0	93	3.8	20	-	-	< 5
Total Dissolved Solids mg/l	-	-	-	-	-	-	-	-	-	835	818	-	2.1	20	-	-	< 10
	-	-	-	-	-	-	-	-	-	< 10	< 10	-	0.0	*	-	-	< 10

* Due to result < 10 mg/L, data reported based on acceptance criteria of Relative % Difference of ± 3 mg/L.

Approved by: _____

C. Cantor

25 Aug 18



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CERTIFICATE of ANALYSIS - CCR

Samantha Marshall
Montana Dakota Utilities
400 N 4th St
Bismarck ND 58501

Report Date: 19 Apr 18
Lab Number: 18-W454
Work Order #: 82-0637
Account #: 002800
Date Sampled: 2 Apr 18 11:46
Date Received: 4 Apr 18 8:00
Sampled By: MVTl Field Services

Project Name: MDU Heskett Active Ash
Sample Description: Dupl

Temp at Receipt: 1.6C

Event and Year: Spring 2018

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
Metal Digestion				EPA 200.2	4 Apr 18	SVS
pH	* 7.3	units	0.1	SM4500 H+ B	4 Apr 18 17:00	SVS
Fluoride	0.88	mg/l	0.10	SM4500-F-C	4 Apr 18 17:00	SVS
Sulfate	6510	mg/l	5.00	ASTM D516-07	11 Apr 18 13:17	RAG
Chloride	77.3	mg/l	1.0	SM4500-Cl-E	5 Apr 18 11:18	RAG
Total Dissolved Solids	9980	mg/l	10	I1750-85	4 Apr 18 10:44	SVS
Calcium - Total	402	mg/l	1.0	6010D	6 Apr 18 10:21	BT
Boron - Total	0.66	mg/l	0.10	6010D	5 Apr 18 11:23	SZ

* Holding time exceeded

Approved by:

Claudette K. Carroll

25 April 18

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

The reporting limit was elevated for any analyte requiring a dilution as coded below:

@ = Due to sample matrix # = Due to concentration of other analytes
! = Due to sample quantity + = Due to internal standard response

CERTIFICATION: ND # ND-00016



MINNESOTA VALLEY TESTING LABORATORIES, INC.

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CERTIFICATE of ANALYSIS - CCR

Samantha Marshall
 Montana Dakota Utilities
 400 N 4th St
 Bismarck ND 58501

Report Date: 19 Apr 18
 Lab Number: 18-W456
 Work Order #: 82-0637
 Account #: 002800
 Date Sampled: 2 Apr 18 14:57
 Date Received: 4 Apr 18 8:00
 Sampled By: MVTl Field Services

Project Name: MDU Heskett Active Ash
 Sample Description: 70

Temp at Receipt: 1.6C

Event and Year: Spring 2018

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
Metal Digestion				EPA 200.2	4 Apr 18	SVS
pH - Field	7.01	units	NA	SM 4500 H+ B	2 Apr 18 14:57	DJN
pH	* 7.5	units	0.1	SM4500 H+ B	4 Apr 18 17:00	SVS
Temperature - Field	5.23	Degrees C	NA	SM 2550B	2 Apr 18 14:57	DJN
Conductivity - Field	3834	umhos/cm	1	EPA 120.1	2 Apr 18 14:57	DJN
Fluoride	0.30	mg/l	0.10	SM4500-F-C	4 Apr 18 17:00	SVS
Sulfate	1810	mg/l	5.00	ASTM D516-07	11 Apr 18 13:17	RAG
Chloride	45.9	mg/l	1.0	SM4500-Cl-E	5 Apr 18 11:18	RAG
Total Dissolved Solids	3120	mg/l	10	I1750-85	4 Apr 18 10:44	SVS
Calcium - Total	343	mg/l	1.0	6010D	6 Apr 18 11:21	BT
Boron - Total	0.43	mg/l	0.10	6010D	5 Apr 18 11:23	SZ

* Holding time exceeded

Approved by:

Claudette K. Carroll ^{CC} 25 Apr 18

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

The reporting limit was elevated for any analyte requiring a dilution as coded below:
 @ = Due to sample matrix # = Due to concentration of other analytes
 ! = Due to sample quantity + = Due to internal standard response

CERTIFICATION: ND # ND-00016



2616 E. Broadway Ave, Bismarck, ND

Phone: (701) 258-9720

Field Datasheet

Groundwater Assessment

Company: MDU Heskett
 Event: 2017
 Sample ID: 13
 Sampling Personal: Darren Nieswaag
 Date: 2 Apr 18

Field Measurements

Stabilization (3 consecutive)		Temp (°C)	Spec. Cond. ±5%	pH ±0.1	DO (mg/L) ±10%	ORP (mV) ±20 mV	Turbidity (NTU) ±10%	Water Level (ft) 0.25 ft	mL Removed	Discription: Clarity, Color, Odor, Ect. clear, slightly turbid, turbid
SEQ #	Time									
11	1136	3.99	10428	6.95	2.40	95.4	2.81	32.04	500	cl
12	1141	2.78	10438	6.97	2.45	95.5	2.72	32.04	500	cl
13	1146	3.35	10394	6.96	2.46	95.0	2.64	32.04	500	cl
14										
15										
16										
17										
18										
19										
20										
21										
22										
23										
24										
25										
26										
27										
28										
29										
30										

Stabilized: Yes No

Total Volume Removed: 9000 mL

Comments:



Field Datasheet

Groundwater Assessment

2616 E. Broadway Ave, Bismarck, ND
Phone: (701) 258-9720

Company: MDU Heskett
Event: Spring 2018
Sample ID: 102
Sampling Personal: Darren J. [Signature]

Weather Conditions: Temp: 20 °F Wind: NE @ 15 Precip: Sunny / Partly Cloudy / Cloudy

Well Information

Well Locked?	Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>	
Well Labeled?	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	
Casing Straight?	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	
Grout Seal Intact?	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	Not Visible
Repairs Necessary:		
Casing Diameter:	2"	
Water Level Before Purge:	18.55	ft
Depth to Top of Pump:	27.05	ft
Water Level After Sample:	20.51	ft
Measurement Method:	Electric Water Level Indicator	

Sampling Information

Purging Method:	Bladder		Control Settings	
Sampling Method:	Bladder		Purge:	5 sec.
Dedicated Equip?:	<input checked="" type="checkbox"/> Yes	<input type="checkbox"/> No	Recover:	55 sec.
Duplicate Sample?:	<input type="checkbox"/> Yes	<input checked="" type="checkbox"/> No	PSI:	
Duplicate Sample ID:				
Purge Date:	2 Apr 18	Time Purging Began:	1237	am/pm
Well Purged Dry?	<input checked="" type="checkbox"/> Yes	<input type="checkbox"/> No	Time Purged Dry:	
Sample Date:	2 Apr 18	Time of Sampling:	1322	am/pm
Bottle List:	1L Raw	250mL Sulfuric		
	500mL Nitric	500mL Nitric (filtered)		

Field Measurements

SEQ #	Stabilization (3 consecutive) Time	Temp (°C)	Spec. Cond. ±5%	pH ±0.1	DO (mg/L) ±10%	ORP (mV) ±20 mV	Turbidity (NTU) ±10%	Water Level (ft) 0.25 ft	Pumping Rate ml/min	mL Removed	Description:
											Clarity, Color, Odor, Ect. Clear, Slightly Turbid, Turbid
1	1242	5.25	10023	6.91	1.20	-3.6	5.86	19.33	100	500	Clear
2	1252	4.39	10041	6.90	0.95	-4.6	1.72	19.67	100	1000	Clear
3	1302	4.78	9767	6.86	0.84	-2.2	1.33	19.87	100	1000	Clear
4	1307	4.74	9640	6.86	0.91	-2.3	1.16	19.92	100	500	Clear
5	1312	4.35	9535	6.85	0.70	-0.6	1.07	20.04	100	500	Clear
6	1317	3.97	9318	6.83	0.74	2.8	1.04	20.09	100	500	Clear
7	1322	4.49	9274	6.83	0.67	3.2	0.98	20.11	100	500	Clear
8											
9											
10											

Stabilized: Yes No
Comments:

Total Volume Removed: 4500 mL



Field Datasheet

Groundwater Assessment

2616 E. Broadway Ave, Bismarck, ND
Phone: (701) 258-9720

Company: MDU Heskett
Event: Spring 2018
Sample ID: 103
Sampling Personal: Jason Nieswagg

Weather Conditions: Temp: 16 °F Wind: N @ 7 Precip: Sunny / Partly Cloudy / Cloudy

Well Information

Well Locked?	Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>	
Well Labeled?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	
Casing Straight?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	
Grout Seal Intact?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	Not Visible
Repairs Necessary:		
Casing Diameter:	2"	
Water Level Before Purge:	32.49	ft
Depth to Top of Pump:	40.85	ft
Water Level After Sample:	34.53	ft
Measurement Method:	Electric Water Level Indicator	

Sampling Information

Purging Method:	Bladder			
Sampling Method:	Bladder			
Dedicated Equip?:	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>			
Duplicate Sample?:	Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>			
Duplicate Sample ID:				
		Control Settings		
		Purge:	5	sec.
		Recover:	55	sec.
		PSI:		
Purge Date:	3 Apr 18	Time Purging Began:	1246	am/pm
Well Purged Dry?	Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>	Time Purged Dry:		
Sample Date:	3 Apr 18	Time of Sampling:	1321	am/pm
Bottle List:	1L Raw	250mL Sulfuric		
	500mL Nitric	500mL Nitric (filtered)		

Field Measurements

SEQ #	Stabilization (3 consecutive) Time	Temp (°C)	Spec. Cond. ±5%	pH ±0.1	DO (mg/L) ±10%	ORP (mV) ±20 mV	Turbidity (NTU) ±10%	Water Level (ft) 0.25 ft	Pumping Rate ml/min	mL Removed	Description:
											Clarity, Color, Odor, Ect. Clear, Slightly Turbid, Turbid
1	1251	5.70	5204	6.76	2.68	76.9	3.69	33.16	100	500	clear
2	1306	5.43	5224	6.72	0.99	73.6	3.92	33.62	100	1500	clear
3	1311	5.48	5220	6.72	1.00	73.5	3.01	33.71	100	500	ch
4	1316	5.49	5221	6.72	1.01	73.2	2.87	33.81	100	500	ch
5	1321	5.59	5224	6.72	0.94	72.9	2.81	33.93	100	500	ch
6											
7											
8											
9											
10											

Stabilized: Yes No
Comments:

Total Volume Removed: 3500 mL



Field Datasheet

Groundwater Assessment

2616 E. Broadway Ave, Bismarck, ND

Phone: (701) 258-9720

Company: MDU Heskett

Event: Spring 2018

Sample ID: 44R

Sampling Personal: Darren Nicolson

Weather Conditions: Temp: 21 °F Wind: NW @ 12 Precip: Sunny / Partly Cloudy / Cloudy

Well Information

Well Locked?	Yes <input checked="" type="checkbox"/>	No <input type="checkbox"/>	
Well Labeled?	Yes <input checked="" type="checkbox"/>	No <input type="checkbox"/>	
Casing Straight?	Yes <input checked="" type="checkbox"/>	No <input type="checkbox"/>	
Grout Seal Intact?	Yes <input checked="" type="checkbox"/>	No <input type="checkbox"/>	Not Visible
Repairs Necessary:			
Casing Diameter:	2"		
Water Level Before Purge:	26.67	ft	
Depth to Top of Pump:	35.11	ft	
Water Level After Sample:	26.95	ft	
Measurement Method:	Electric Water Level Indicator		

Sampling Information

Purging Method:	Bladder			
Sampling Method:	Bladder			
Dedicated Equip?:	Yes <input checked="" type="checkbox"/>	No <input type="checkbox"/>	Control Settings	
Duplicate Sample?:	Yes <input type="checkbox"/>	No <input checked="" type="checkbox"/>	Purge:	5 sec.
Duplicate Sample ID:			Recover:	55 sec.
			PSI:	
Purge Date:	3 Apr 18	Time Purging Began:	15:11	am/pm
Well Purged Dry?:	Yes <input checked="" type="checkbox"/>	No <input type="checkbox"/>	Time Purged Dry:	
Sample Date:	3 Apr 18	Time of Sampling:	16:21	am/pm
Bottle List:	1L Raw	250mL Sulfuric		
	500mL Nitric	500mL Nitric (filtered)		

Field Measurements

SEQ #	Stabilization (3 consecutive) Time	Temp (°C)	Spec. Cond. ±5%	pH ±0.1	DO (mg/L) ±10%	ORP (mV) ±20 mV	Turbidity (NTU) ±10%	Water Level (ft) 0.25 ft	Pumping Rate ml/min	mL Removed	Description:
											Clarity, Color, Odor, Ect. Clear, Slightly Turbid, Turbid
1	1516	6.60	9345	6.61	2.91	69.7	55.6	26.76	100	500	slightly turbid
2	1531	6.57	9356	6.60	1.62	70.6	37.3	26.75	100	1500	st
3	1546	6.21	9377	6.59	1.71	69.5	17.1	26.75	100	1500	clear
4	1661	6.23	9395	6.60	1.33	70.7	8.85	26.77	100	1500	clear
5	1606	6.71	9398	6.60	1.56	69.4	5.33	26.75	100	500	clear
6	1611	6.87	9379	6.59	1.51	68.8	4.42	26.75	100	500	clear
7	1616	6.45	9389	6.60	1.48	69.4	4.51	26.75	100	500	clear
8	1621	6.54	9397	6.60	1.44	69.5	4.65	26.77	100	500	clear
9											
10											

Stabilized: Yes No

Total Volume Removed: 7000 mL

Comments: well was frozen took a while to unthaw



Laboratories, Inc.

2616 E. Broadway
Bismarck, ND 58501
Phone (701) 258-9720

Chain of Custody Record

Project Name: MDU Heskett	Event: Spring 2018	Work Order Number: <i>82-0637</i>
Report To: MDU Attn: Samantha Marshall Address: 400 N. 4th St Bismarck, ND 58501 phone: 701-222-7829 email:	Carbon Copy: Attn: Address:	Name of Sampler(s): <i>Darren Nieswaag</i>

Sample Information					Bottle Type				Field Parameters			Analysis
Lab Number	Sample ID	Date	Time	Sample Type	1 liter	500mL Nitric	500mL Nitric (filtered)	250 mL Sulfuric	Temp (°C)	Spec. Cond.	pH	Analysis Required
W453	13	2 Apr 18	1146	GW	X	X	X	X	3.35	10394	6.96	MDU List AA & MDU Appendix 3 List
W454	Dup1	2 Apr 18	1146	GW	X	X	X	X	-	-	-	
W455	102	2 Apr 18	1322	GW	X	X	X	X	4.49	9274	6.83	
W456	70	2 Apr 18	1457	GW	X	X	X	X	5.23	3834	7.01	
W457	101	3 Apr 18	1210	GW	X	X	X	X	5.69	4900	6.73	
W458	103	3 Apr 18	1321	GW	X	X	X	X	5.59	5224	6.72	
W459	44R	3 Apr 18	1621	GW	X	X	X	X	6.54	9377	6.60	
W460	FB1	3 Apr 18	-	GW	X	X	X	X	-	-	-	

Comments:

Relinquished By:		Sample Condition:	
Name:	Date/Time	Location:	Temp (°C)
<i>[Signature]</i>	3 Apr 18 1720	Log In Walk In #2	1.6°C (TM562 / TM588)
1			
2			

Received by:	
Name:	Date/Time
<i>[Signature]</i>	0900 4 Apr 18



CASE NARRATIVE – AMENDED 9 MAY 18 (Analysis Flag)

MVTL Lab Reference No/SDG: 201882-0663
Client: Montana Dakota Utilities
Location: MDU Heskett
Project Identification: CCR April 2018
MVTL Laboratory Identifications: 18-W497 through 18-W504
Page 1 of 1

Table with 2 columns: MDU Sample Identification and MVTL Laboratory #. Rows include samples 33, 3-90, Dup2, 2-90, 104, 80R, 105, and FB2 with corresponding lab numbers 18-W497 through 18-W504.

I. RECEIPT

- All samples were received at the laboratory on 5 Apr 18 at 1505.
Samples were collected and hand delivered by MVTL Field Service personnel to the laboratory.
Samples were received on ice and evidence of cooling had begun.
Temperature of samples upon receipt was 2.4°C.
All samples were properly preserved unless noted here and/or flagged on the individual analytical laboratory report.
No other exceptions on sample receipt were encountered on this sample set unless noted here.

II. HOLDING TIMES

- With the exception of pH, all holding times were met for both preparation and analysis unless noted here.

III. METHODS

- Approved methodology was followed for all sample analyses.

IV. ANALYSIS

- All acceptance criteria was met for calibration, method blanks, laboratory control samples, laboratory fortified matrix/matrix duplicates unless noted here and/or flagged on the individual analytical laboratory report.
For some analytes, the reported results were elevated due to additional dilutions required to minimize the effects of sample matrix.

All laboratory data has been approved by MVTL Laboratories.

SIGNED: Claudette Carroll DATE: 9 May 18
Claudette Carroll - MVTL Bismarck Laboratory Manager



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 1201 Lincoln Highway ~ Nevada, IA 50201 ~ 800-362-0855 ~ Fax 515-382-3885
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MEMBER
ACIL

Quality Control Report

Lab IDs: 18-W497 to 18-W504

Project: MDU Heskett Active Ash

Work Order: 201882-0663

Analyte	LCS Spike Amt	LCS Rec %	LCS % Rec Limits	Matrix Spike Amt	Matrix Spike ID	Matrix Spike Orig Result	Matrix Spike Result	Matrix Spike Rec %	Matrix Spike % Rec Limits	MSD/ Dup Orig Result	MSD/ Dup Result	MSD Rec %	MSD/ Dup RPD	MSD/ Dup RPD Limit (<)	Known Rec (%)	Known % Rec Limits	Method Blank
Boron - Total mg/l	0.40	102	80-120	2.00	18-W503	< 0.5	2.22	111	75-125	2.22	2.24	112	0.9	20	-	-	< 0.1 < 0.1
Calcium - Total mg/l	20.0 20.0	108 107	80-120 80-120	500 500	18W498q 18W502q	445 292	960 790	103 100	75-125 75-125	960 790	950 800	101 102	1.0 1.3	20 20	- - - -	- - - -	< 1 < 1 < 1 < 1 < 1
Chloride mg/l	30.0 30.0 30.0	98 99 99	80-120 80-120 80-120	30.0 1200	18-W499 18-W548	37.8 2880	67.4 4110	99 102	80-120 80-120	67.4 4110	67.9 4150	100 106	0.7 1.0	20 20	- - -	- - -	< 1 < 1 < 1
Fluoride mg/l	0.50	104	90-110	0.500 0.500	18-W498 18-W502	0.13 0.29	0.62 0.77	98 96	80-120 80-120	0.62 0.77	0.62 0.77	98 96	0.0 0.0	20 20	- -	- -	< 0.1 < 0.1
pH units	- -	- -	- -	- -	- -	- -	- -	- -	- -	7.2 7.1	7.2 7.2	- -	0.0 1.4	20 20	- -	- -	- -
Sulfate mg/l	100 100 100	104 94 97	80-120 80-120 80-120	4000 500 4000	18-W498 18-W548 18-M875	2020 201 744	5970 652 5330	99 90 115	80-120 80-120 80-120	5970 652 5330	5780 656 5180	94 91 111	3.2 0.6 2.9	20 20 20	- - -	- - -	< 5 < 5 < 5
Total Dissolved Solids mg/l	-	-	-	-	-	-	-	-	-	< 10	< 10	-	0.0	*	-	-	< 10

* Due to result < 10 mg/L, data reported based on acceptance criteria of Relative % Difference of +/- 3 mg/L.

Approved by: C. Cantor
4 May 18



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www.mvttl.com



CERTIFICATE of ANALYSIS - CCR

Samantha Marshall
Montana Dakota Utilities
400 N 4th St
Bismarck ND 58501

Report Date: 1 May 18
Lab Number: 18-W499
Work Order #: 82-0663
Account #: 002800
Date Sampled: 4 Apr 18
Date Received: 5 Apr 18 15:05
Sampled By: MVTL Field Services

Project Name: MDU Heskett Active Ash
Sample Description: Dup2

Temp at Receipt: 2.4C

Event and Year: Spring 2018

Table with 6 columns: As Received Result, Method RL, Method Reference, Date Analyzed, Analyst. Rows include Metal Digestion, pH, Fluoride, Sulfate, Chloride, Total Dissolved Solids, Calcium - Total, and Boron - Total.

* Holding time exceeded

Approved by: Claudette K. Carroll 4 May 18

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

The reporting limit was elevated for any analyte requiring a dilution as coded below:
@ = Due to sample matrix # = Due to concentration of other analytes
! = Due to sample quantity + = Due to internal standard response

CERTIFICATION: ND # ND-00016



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Page: 1 of 1

CERTIFICATE of ANALYSIS - CCR

Samantha Marshall
 Montana Dakota Utilities
 400 N 4th St
 Bismarck ND 58501

Report Date: 23 Apr 18
 Lab Number: 18-W501
 Work Order #: 82-0663
 Account #: 002800
 Date Sampled: 5 Apr 18 11:36
 Date Received: 5 Apr 18 15:05
 Sampled By: MVTL Field Services

Project Name: MDU Heskett Active Ash
 Sample Description: 104

Temp at Receipt: 2.4C

Event and Year: Spring 2018

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
Metal Digestion				EPA 200.2	5 Apr 18	SVS
pH - Field	6.92	units	NA	SM 4500 H+ B	5 Apr 18 11:36	DJN
pH	* 7.3	units	0.1	SM4500 H+ B	6 Apr 18 17:00	SVS
Temperature - Field	6.60	Degrees C	NA	SM 2550B	5 Apr 18 11:36	DJN
Conductivity - Field	14041	umhos/cm	1	EPA 120.1	5 Apr 18 11:36	DJN
Fluoride	0.54	mg/l	0.10	SM4500-F-C	6 Apr 18 17:00	SVS
Sulfate	10700	mg/l	5.00	ASTM D516-07	18 Apr 18 15:15	RAG
Chloride	103	mg/l	1.0	SM4500-Cl-E	10 Apr 18 14:43	RAG
Total Dissolved Solids	17400	mg/l	10	I1750-85	9 Apr 18 12:00	SVS
Calcium - Total	431	mg/l	1.0	6010D	10 Apr 18 10:57	SZ
Boron - Total	0.90	mg/l	0.10	6010D	9 Apr 18 14:38	SZ

* Holding time exceeded

Approved by:

Claudette K. Carroll

*CC
4 May 18*

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

The reporting limit was elevated for any analyte requiring a dilution as coded below:
 @ = Due to sample matrix # = Due to concentration of other analytes
 ! = Due to sample quantity + = Due to internal standard response

CERTIFICATION: ND # ND-00016



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CERTIFICATE of ANALYSIS - CCR

Samantha Marshall
Montana Dakota Utilities
400 N 4th St
Bismarck ND 58501

Report Date: 1 May 18
Lab Number: 18-W502
Work Order #: 82-0663
Account #: 002800
Date Sampled: 5 Apr 18 12:31
Date Received: 5 Apr 18 15:05
Sampled By: MVTL Field Services

Project Name: MDU Heskett Active Ash
Sample Description: 80R

Temp at Receipt: 2.4C

Event and Year: Spring 2018

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
Metal Digestion				EPA 200.2	5 Apr 18	SVS
pH - Field	7.10	units	NA	SM 4500 H+ B	5 Apr 18 12:31	DJN
pH	* 7.4	units	0.1	SM4500 H+ B	6 Apr 18 17:00	SVS
Temperature - Field	5.54	Degrees C	NA	SM 2550B	5 Apr 18 12:31	DJN
Conductivity - Field	5743	umhos/cm	1	EPA 120.1	5 Apr 18 12:31	DJN
Fluoride	0.29	mg/l	0.10	SM4500-F-C	6 Apr 18 17:00	SVS
Sulfate	3260	mg/l	5.00	ASTM D516-07	19 Apr 18 10:30	RAG
Chloride	157	mg/l	1.0	SM4500-Cl-E	18 Apr 18 9:12	RAG
Total Dissolved Solids	5730	mg/l	10	I1750-85	9 Apr 18 12:00	SVS
Calcium - Total	292	mg/l	1.0	6010D	10 Apr 18 11:57	SZ
Boron - Total	< 0.5 @	mg/l	0.10	6010D	9 Apr 18 14:38	SZ

* Holding time exceeded

Approved by:

Claudette K. Carroll ^{CC}
4 May 18

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

The reporting limit was elevated for any analyte requiring a dilution as coded below:

@ = Due to sample matrix # = Due to concentration of other analytes
! = Due to sample quantity + = Due to internal standard response

CERTIFICATION: ND # ND-00016



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CERTIFICATE of ANALYSIS - CCR

Samantha Marshall
 Montana Dakota Utilities
 400 N 4th St
 Bismarck ND 58501

Report Date: 1 May 18
 Lab Number: 18-W504
 Work Order #: 82-0663
 Account #: 002800
 Date Sampled: 5 Apr 18
 Date Received: 5 Apr 18 15:05
 Sampled By: MVTL Field Services

Project Name: MDU Heskett Active Ash

PO #: 169918

Sample Description: FB2

Temp at Receipt: 2.4C

Event and Year: Spring 2018

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
Metal Digestion				EPA 200.2	5 Apr 18	SVS
pH	* 6.0	units	0.1	SM4500 H+ B	6 Apr 18 17:00	SVS
Fluoride	< 0.1	mg/l	0.10	SM4500-F-C	6 Apr 18 17:00	SVS
Sulfate	< 5	mg/l	5.00	ASTM D516-07	19 Apr 18 10:30	RAG
Chloride	< 1	mg/l	1.0	SM4500-Cl-E	18 Apr 18 9:12	RAG
Total Dissolved Solids	< 10	mg/l	10	I1750-85	9 Apr 18 12:00	SVS
Calcium - Total	< 1	mg/l	1.0	6010D	10 Apr 18 11:57	SZ
Boron - Total	< 0.1	mg/l	0.10	6010D	9 Apr 18 14:38	SZ

* Holding time exceeded

Approved by:

Claudette K. Carroll *4 May 18*

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

The reporting limit was elevated for any analyte requiring a dilution as coded below:

@ = Due to sample matrix # = Due to concentration of other analytes
 ! = Due to sample quantity + = Due to internal standard response

CERTIFICATION: ND # ND-00016



Field Datasheet

Groundwater Assessment

2616 E. Broadway Ave, Bismarck, ND

Phone: (701) 258-9720

Company: MDU Heskett

Event: Spring 2018

Sample ID: 33

Sampling Personal: *Parren Nieswae*

Weather Conditions: Temp: 27 °F Wind: 5 @ 17 Precip: Sunny / Partly Cloudy / Cloudy

Well Information

Well Locked?	Yes	No	
Well Labeled?	Yes	No	
Casing Straight?	Yes	No	
Grout Seal Intact?	Yes	No	Not Visible
Repairs Necessary:			
Casing Diameter:	2"		
Water Level Before Purge:	41.60 ft		
Depth to Top of Pump:	44.48 ft		
Water Level After Sample:	41.73 ft		
Measurement Method:	Electric Water Level Indicator		

Sampling Information

Purging Method:	Bladder			
Sampling Method:	Bladder			
Dedicated Equip?:	Yes	No		
Duplicate Sample?:	Yes	No		
Duplicate Sample ID:				
Purge Date:	4 Apr 18	Time Purging Began:	1115	am/pm
Well Purged Dry?:	Yes	No		
Sample Date:	4 Apr 18	Time of Sampling:	1235	am/pm
Bottle List:	1L Raw	250mL Sulfuric		
	500mL Nitric	500mL Nitric (filtered)		

Control Settings		
Purge:	5	sec.
Recover:	55	sec.
PSI:		

Field Measurements

Stabilization (3 consecutive)	Temp (°C)	Spec. Cond. ±5%	pH ±0.1	DO (mg/L) ±10%	ORP (mV) ±20 mV	Turbidity (NTU) ±10%	Water Level (ft) 0.25 ft	Pumping Rate ml/min	mL Removed	Description: Clarity, Color, Odor, Ect. Clear, Slightly Turbid, Turbid	
1	1120	5.04	4999	7.02	11.73	21.9	41.6	41.81	100	500	Slightly turbid
2	1135	7.00	5046	6.67	2.46	28.0	75.6	41.72	100	1500	ST
3	1150	7.09	4876	6.34	3.01	25.6	41.5	41.72	100	1500	ST
4	1205	7.10	4840	6.61	2.17	248.0	9.78	41.72	100	1500	Clear
5	1215	7.33	4831	6.59	2.01	48.4	4.39	41.74	100	1000	Clear
6	1220	7.41	4838	6.59	2.00	48.3	2.61	41.72	100	500	Clear
7	1225	7.25	4839	6.59	2.03	48.3	1.60	41.75	100	500	Clear
8	1230	7.16	4844	6.59	2.07	48.5	1.68	41.73	100	500	Clear
9	1235	7.17	4834	6.60	2.09	48.8	1.73	41.73	100	500	Clear
10											

Stabilized: Yes No

Total Volume Removed: 8000 mL

Comments: Had to pull pump check ball on the pump was stuck.



Field Datasheet

Groundwater Assessment

2616 E. Broadway Ave, Bismarck, ND
Phone: (701) 258-9720

Company: MDU Heskett
Event: Spring 2018
Sample ID: 104
Sampling Personal: Darren Nieswender

Weather Conditions: Temp: 23 °F Wind: N @ 10 Precip: Sunny / Partly Cloudy / Cloudy

Well Information

Well Locked?	Yes	<input checked="" type="radio"/> No	
Well Labeled?	<input checked="" type="radio"/> Yes	No	
Casing Straight?	<input checked="" type="radio"/> Yes	No	
Grout Seal Intact?	<input checked="" type="radio"/> Yes	No	Not Visible
Repairs Necessary:			
Casing Diameter:	2"		
Water Level Before Purge:	13.66 ft		
Depth to Top of Pump:	-		
Water Level After Sample:	13.95 ft		
Measurement Method:	Electric Water Level Indicator		

Sampling Information

Purging Method:	Bladder		Control Settings	
Sampling Method:	Bladder		Purge:	5 sec.
Dedicated Equip?:	<input checked="" type="radio"/> Yes	No	Recover:	55 sec.
Duplicate Sample?:	Yes	<input checked="" type="radio"/> No	PSI:	
Duplicate Sample ID:				
Purge Date:	5 Apr 18	Time Purging Began:	1051	am/pm
Well Purged Dry?	Yes	<input checked="" type="radio"/> No	Time Purged Dry:	
Sample Date:	5 Apr 18	Time of Sampling:	1136	am/pm
Bottle List:	1L Raw	250mL Sulfuric		
	500mL Nitric	500mL Nitric (filtered)		

Field Measurements

SEQ #	Stabilization (3 consecutive) Time	Temp (°C)	Spec. Cond. ±5%	pH ±0.1	DO (mg/L) ±10%	ORP (mV) ±20 mV	Turbidity (NTU) ±10%	Water Level (ft) 0.25 ft	Pumping Rate ml/min	mL Removed	Description: Clarity, Color, Odor, Ect. Clear, Slightly Turbid, Turbid
1	1056	7.08	14066	6.99	5.49	69.5	5.18	13.84	100	500	cl
2	1111	6.26	14071	6.92	1.65	63.4	0.85	13.86	100	1500	cl
3	1116	6.71	14051	6.92	1.30	63.2	0.59	13.88	100	500	cl
4	1126	6.17	14063	6.93	1.74	62.8	0.65	13.91	100	1000	cl
5	1131	6.61	14021	6.92	1.68	62.8	0.58	13.92	100	500	cl
6	1136	6.60	14041	6.92	1.60	62.1	0.55	13.95	100	500	cl
7											
8											
9											
10											

Stabilized: Yes No
Comments:

Total Volume Removed: 4500 mL



Field Datasheet

Groundwater Assessment

2616 E. Broadway Ave, Bismarck, ND
Phone: (701) 258-9720

Company: MDU Heskett
Event: Spring 2018
Sample ID: 105
Sampling Personal: Darren Nieswager

Weather Conditions: Temp: 27 °F Wind: N @ 15 Precip: Sunny / Partly Cloudy / Cloudy

Well Information

Well Locked?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	
Well Labeled?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	
Casing Straight?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	
Grout Seal Intact?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	Not Visible
Repairs Necessary:	<input type="checkbox"/>	
Casing Diameter:	2"	
Water Level Before Purge:	11.56	ft
Depth to Top of Pump:	21.24	ft
Water Level After Sample:	11.65	ft
Measurement Method:	Electric Water Level Indicator	

Sampling Information

Purging Method:	Bladder	
Sampling Method:	Bladder	
Dedicated Equip?:	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	
Duplicate Sample?:	Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>	
Duplicate Sample ID:		
Purge Date:	5 April	Time Purging Began: 1302 am/pm
Well Purged Dry?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	Time Purged Dry: am/pm
Sample Date:	5 April	Time of Sampling: 1357 am/pm
Bottle List:	1L Raw 500mL Nitric	250mL Sulfuric 500mL Nitric (filtered)

Control Settings		
Purge:	5	sec.
Recover:	5.5	sec.
PSI:		

Field Measurements

SEQ #	Stabilization (3 consecutive) Time	Temp (°C)	Spec. Cond. ±5%	pH ±0.1	DO (mg/L) ±10%	ORP (mV) ±20 mV	Turbidity (NTU) ±10%	Water Level (ft) 0.25 ft	Pumping Rate ml/min	mL Removed	Description:
											Clarity, Color, Odor, Ect. Clear, Slightly Turbid, Turbid
1	1307	6.11	6665	6.74	1.25	58.8	1.25	11.61	100	500	cl
2	1317	5.92	6779	6.77	1.06	57.5	1.52	11.64	100	1000	cl
3	1322	5.78	6718	6.77	1.19	57.5	0.83	11.65	100	500	cl
4	1332	5.88	7253	6.74	1.39	57.2	1.32	11.65	100	1000	cl
5	1342	6.13	7503	6.74	0.97	56.8	1.70	11.65	100	1000	cl
6	1347	6.42	7512	6.73	0.78	56.8	1.73	11.65	100	500	cl
7	1352	6.49	7540	6.73	0.83	56.7	1.65	11.65	100	500	cl
8	1357	6.27	7596	6.72	0.80	56.7	1.59	11.65	100	500	cl
9											
10											

Stabilized: Yes No

Total Volume Removed: 5500 mL

Comments: *DN 5 APR 18 (A)

MVTL Calibration Worksheet

Site: MDU Heskett

Technician: Parren Nieswang

Instrument
(Circle One):

#1 650 MDS 08F100203

#2 650 MDS 04H14736

#3 556 MPS T2E102056

Pre Site Calibration						
Date:	<u>2 APR 18</u>		Time: <u>0744</u>			
pH	Temp °C	Pre Cal	Post Cal	Post Cal Range	mv	mv Range +/- 50
Buffer 7	<u>19.32</u>	<u>7.00</u>	<u>7.00</u>	6.95-7.05	<u>-31.9</u>	0 +/- 50
Buffer 10	<u>19.26</u>	<u>10.03</u>	<u>10.00</u>	9.95-10.05	<u>-212.0</u>	-180 +/- 50
Conductivity						Check
Buffer 10000	<u>19.20</u>	<u>9961</u>	<u>10002</u>	±10%	Buffer 5000	<u>4992</u>
ORP						
231 mV @ 25C	<u>7.25</u>	<u>232.7</u>	<u>231.0</u>	±10 mV		
DO						
	<u>19.60</u>	<u>8.41</u>	<u>8.58</u>	Barometric Pressure (mm Hg)		
				mg/L	<u>711.5</u>	

Post Site Check		
Time:	<u>1600</u>	
pH	Temp °C	Reading
Buffer 7	<u>18.35</u>	<u>6.99</u>
Conductivity		
Buffer 5000	<u>18.32</u>	<u>5024</u>

Pre Site Calibration						
Date:	<u>3 APR 18</u>		Time: <u>0800</u>			
pH	Temp °C	Pre Cal	Post Cal	Post Cal Range	mv	mv Range +/- 50
Buffer 7	<u>18.64</u>	<u>7.02</u>	<u>7.00</u>	6.95-7.05	<u>-33.2</u>	0 +/- 50
Buffer 10	<u>18.53</u>	<u>996</u>	<u>10.00</u>	9.95-10.05	<u>-209.5</u>	-180 +/- 50
Conductivity						Check
Buffer 10000	<u>17.93</u>	<u>10120</u>	<u>10001</u>	±10%	Buffer 5000	<u>4990</u>
ORP						
231 mV @ 25C	<u>7.29</u>	<u>226.6</u>	<u>231.1</u>	±10 mV		
DO						
	<u>17.18</u>	<u>7.37</u>	<u>9.10</u>	Barometric Pressure (mm Hg)		
				mg/L	<u>720.8</u>	

Post Site Check		
Time:	<u>1723</u>	
pH	Temp °C	Reading
Buffer 7	<u>15.89</u>	<u>7.01</u>
Conductivity		
Buffer 5000	<u>18.33</u>	<u>5025</u>

MVTL Calibration Worksheet

Site: MDU Heskett

Technician: Parren Nieswaag

Instrument
(Circle One):

#1 650 MDS 08F100203

#2 650 MDS 04H14736

#3 556 MPS 12E102056

Pre Site Calibration						
Date:	<u>4 Apr 18</u>		Time: <u>0800</u>			
pH	Temp °C	Pre Cal	Post Cal	Post Cal Range	mv	mv Range +/- 50
Buffer 7	<u>18.35</u>	<u>6.99</u>	<u>7.00</u>	6.95-7.05	<u>-32.3</u>	0 +/- 50
Buffer 10	<u>18.54</u>	<u>10.01</u>	<u>10.00</u>	9.95-10.05	<u>-209.1</u>	-180 +/- 50
Conductivity						Check
Buffer 10000	<u>17.86</u>	<u>10264</u>	<u>10003</u>	±10%	Buffer 5000	<u>4999</u>
ORP						
231 mV @ 25C	<u>6.37</u>	<u>230.0</u>	<u>231.4</u>	±10 mV		
DO						
	<u>17.57</u>	<u>8.90</u>	<u>9.03</u>	Barometric Pressure (mm Hg)		
				mg/L	<u>718.6</u>	

Post Site Check		
Time:	<u>1714</u>	
pH	Temp °C	Reading
Buffer 7	<u>19.29</u>	<u>7.01</u>
Conductivity		
Buffer 5000	<u>18.44</u>	<u>5008</u>

Pre Site Calibration						
Date:	<u>5 Apr 18</u>		Time: <u>0800</u>			
pH	Temp °C	Pre Cal	Post Cal	Post Cal Range	mv	mv Range +/- 50
Buffer 7	<u>19.45</u>	<u>7.03</u>	<u>7.00</u>	6.95-7.05	<u>-34.1</u>	0 +/- 50
Buffer 10	<u>19.43</u>	<u>9.98</u>	<u>10.00</u>	9.95-10.05	<u>-210.3</u>	-180 +/- 50
Conductivity						Check
Buffer 10000	<u>18.98</u>	<u>9968</u>	<u>9999</u>	±10%	Buffer 5000	<u>4984</u>
ORP						
231 mV @ 25C	<u>6.60</u>	<u>229.4</u>	<u>231.4</u>	±10 mV		
DO						
	<u>18.83</u>	<u>8.54</u>	<u>8.76</u>	Barometric Pressure (mm Hg)		
				mg/L	<u>715.7</u>	

Post Site Check		
Time:	<u>1454</u>	
pH	Temp °C	Reading
Buffer 7	<u>18.86</u>	<u>7.00</u>
Conductivity		
Buffer 5000	<u>17.77</u>	<u>5014</u>



Laboratories, Inc.

2616 E. Broadway
Bismarck, ND 58501
Phone (701) 258-9720

Chain of Custody Record

Project Name: MDU Heskett	Event: Spring 2018	Work Order Number: <i>82-0663</i>
Report To: MDU Attn: Samantha Marshall Address: 400 N. 4th St Bismarck, ND 58501 phone: 701-222-7829 email:	Carbon Copy: Attn: Address:	Name of Sampler(s): <i>Darren Niesway</i>

Lab Number	Sample ID	Date	Time	Sample Type	Bottle Type				Field Parameters			Analysis Required
					1 liter	500mL Nitric	500mL Nitric (filtered)	250 mL Sulfuric	Temp (°C)	Spec. Cond.	pH	
W497	33	4 Apr 18	1235	GW	X	X	X	X	7.17	4834	6.60	MDU List AA & MDU Appendix 3 List
W498	3-90	4 Apr 18	1350	GW	X	X	X	X	7.21	4640	6.91	
W499	Dup2	4 Apr 18	-	GW	X	X	X	X	-	-	-	
W500	2-90	4 Apr 18	1512	GW	X	X	X	X	6.76	7110	6.96	
W501	104	5 Apr 18	1136	GW	X	X	X	X	6.60	14041	6.92	
W502	80R	5 Apr 18	1231	GW	X	X	X	X	5.54	5743	7.10	
W503	105	5 Apr 18	1357	GW	X	X	X	X	6.27	7596	6.72	
W504	FB2	5 Apr 18	-	GW	X	X	X	X	-	-	-	

Comments:

Relinquished By:		Sample Condition:	
Name:	Date/Time	Location:	Temp (°C)
<i>Darren Niesway</i>	5 Apr 18 1505	Log In Walk In #2	1 2.4 (TM562) TM588

Received by:	
Name:	Date/Time
<i>Mudman</i>	1505 5 Apr 18



CASE NARRATIVE

MVTL Lab Reference No/SDG: 201882-2048
Client: Montana Dakota Utilities
Location: MDU Heskett
Project Identification: CCR August 2018
MVTL Laboratory Identifications: 18-W2547
Page 1 of 1

MDU Sample Identification	MVTL Laboratory #
2-90	18-W2547

I. RECEIPT

- All samples were received at the laboratory on 13 Aug 18 at 0955.
- Samples were collected and hand delivered by MVTL Field Service personnel to the laboratory.
- Samples were received on ice and evidence of cooling had begun.
 - Temperature of samples upon receipt was 5.8°C.
- All samples were properly preserved unless noted here and/or flagged on the individual analytical laboratory report.
- No other exceptions on sample receipt were encountered on this sample set unless noted here.

II. HOLDING TIMES

- With the exception of pH, all holding times were met for both preparation and analysis unless noted here.

III. METHODS

- Approved methodology was followed for all sample analyses.

IV. ANALYSIS

- All acceptance criteria was met for calibration, method blanks, laboratory control samples, laboratory fortified matrix/matrix duplicates unless noted here and/or flagged on the individual analytical laboratory report.

All laboratory data has been approved by MVTL Laboratories.

SIGNED: Claudette Carroll DATE: 15 Aug 18
Claudette Carroll - MVTL Bismarck Laboratory Manager

Quality Control Report

Lab ID: 18-W2547

Project:

Work Order: 201882-2048

Analyte	LCS Spike Amt	LCS Rec %	LCS % Rec Limits	Matrix Spike Amt	Matrix Spike ID	Matrix Spike Orig Result	Matrix Spike Result	Matrix Spike Rec %	Matrix Spike % Rec Limits	MSD/ Dup Orig Result	MSD/ Dup Result	MSD Rec %	MSD/ Dup RPD	MSD/ Dup RPD Limit (<=)	Known Rec (%)	Known % Rec Limits	Method Blank
Fluoride mg/l	0.50	102	90-110	0.500	18-W2527	0.20	0.71	102	80-120	0.71	0.70	100	1.4	20	-	-	< 0.1
				0.500	18-W2547	1.03	1.46	86	80-120	1.46	1.46	86	0.0	20	-	-	< 0.1

Approved by: _____

C. Cantel

15 Aug 18



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Page: 1 of 1

CERTIFICATE of ANALYSIS - CCR

Samantha Marshall
Montana Dakota Utilities
5181 Southgate Dr
Billings MT 59102

Report Date: 15 Aug 18
Lab Number: 18-W2547
Work Order #: 82-2048
Account #: 002800
Date Sampled: 13 Aug 18 9:12
Date Received: 13 Aug 18 9:55
Sampled By: MVTL Field Services

Sample Description: 2-90
Sample Site: MDU Heskett
Event and Year: August 2018

Temp at Receipt: 5.8C ROI

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
pH - Field	6.89	units	NA	SM 4500 H+ B	13 Aug 18 9:12	DJN
Temperature - Field	12.1	Degrees C	NA	SM 2550B	13 Aug 18 9:12	DJN
Conductivity - Field	7281	umhos/cm	1	EPA 120.1	13 Aug 18 9:12	DJN
Fluoride	1.03	mg/l	0.10	SM4500-F-C	13 Aug 18 17:00	SVS

Approved by:

CC
Claudette K. Carroll 15 Aug 18

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

The reporting limit was elevated for any analyte requiring a dilution as coded below:
@ = Due to sample matrix # = Due to concentration of other analytes
! = Due to sample quantity + = Due to internal standard response

CERTIFICATION: ND # ND-00016



Field Datasheet

Groundwater Assessment

2616 E. Broadway Ave, Bismarck, ND

Phone: (701) 258-9720

Company: MDU Heskett
 Event: August 2018
 Sample ID: 2-90
 Sampling Personal: Darren Nieswalg

Weather Conditions: _____ Temp: _____ °F Wind: Light @ Precip: Sunny / Partly Cloudy / Cloudy

Well Information

Well Locked?	Yes	No	
Well Labeled?	Yes	No	
Casing Straight?	Yes	No	
Grout Seal Intact?	Yes	No	<u>Not Visible</u>
Repairs Necessary:			
Casing Diameter:	2"		
Water Level Before Purge:	<u>22.19</u>		ft
Depth to Top of Pump:	<u>22.35</u>		ft
Water Level After Sample:	<u>22.35 Top</u>		ft
Measurement Method:	Electric Water Level Indicator		

Sampling Information

Purging Method:	Bladder		Control Settings
Sampling Method:	Bladder		
Dedicated Equip?:	Yes	No	
Duplicate Sample?:	Yes	No	
Duplicate Sample ID:	—		
Purge Date:	<u>13 Aug 18</u>	Time Purging Began:	<u>0842</u> am/pm
Well Purged Dry?	Yes	No	Time Purged Dry: — am/pm
Sample Date:	<u>13 Aug 18</u>	Time of Sampling:	<u>0912</u> am/pm
Bottle List:	1L Raw		

Field Measurements

SEQ #	Stabilization (3 consecutive) Time	Temp (°C)	Spec. Cond. ±5%	pH ±0.1	DO (mg/L) ±10%	ORP (mV) ±20 mV	Turbidity (NTU) ±10%	Water Level (ft) 0.25 ft	Pumping Rate ml/min	mL Removed	Description:
											Clarity, Color, Odor, Ect. Clear, Slightly Turbid, Turbid
1	<u>0847</u>	<u>10.15</u>	<u>7219</u>	<u>6.85</u>	<u>7.77</u>	<u>26.7</u>	<u>1.44</u>	<u>22.35</u>	<u>100</u>	<u>500</u>	<u>clear</u>
2	<u>0857</u>	<u>12.31</u>	<u>7261</u>	<u>6.87</u>	<u>4.25</u>	<u>4.3</u>	<u>1.54</u>	<u>22.35</u>	<u>100</u>	<u>1000</u>	<u>clear</u>
3	<u>0902</u>	<u>12.18</u>	<u>7264</u>	<u>6.88</u>	<u>4.78</u>	<u>0.8</u>	<u>0.907</u>	<u>22.35</u>	<u>100</u>	<u>500</u>	<u>clear</u>
4	<u>0907</u>	<u>12.03</u>	<u>7255</u>	<u>6.88</u>	<u>4.96</u>	<u>-5.8</u>	<u>0.94</u>	<u>22.35</u>	<u>100</u>	<u>500</u>	<u>clear</u>
5	<u>0912</u>	<u>12.12</u>	<u>7281</u>	<u>6.89</u>	<u>4.56</u>	<u>-8.9</u>	<u>0.93</u>	<u>22.35</u>	<u>100</u>	<u>500</u>	<u>clear</u>
6											
7											
8											
9											
10											

Stabilized: Yes No
 Comments: _____

Total Volume Removed: 3,000 mL

MVTL Calibration Worksheet

Site: MDU Heskett

Technician: Darren Nieswaag

Instrument
(Circle One):

#1 650 MDS 08F100203

#2 650 MDS 04H14736

#3 556 MPS 12E102056

Pre Site Calibration						
Date:	13 Aug 18		Time:	0745		
	pH	Temp °C	Pre Cal	Post Cal	Post Cal Range	mv Range +/-
Buffer 7		21.84	6.94	7.00	6.95-7.05	0 +/- 50
Buffer 10		21.94	10.04	10.00	9.95-10.05	-180 +/- 50
Conductivity						Check
Buffer 10000		22.17	10012	10001	±10%	Buffer 5000
ORP						
231 mV @ 25C		9.00	236.7	231.4	±10 mV	5009
DO						
		21.70	8.04	8.28	Barometric Pressure (mm Hg)	
					mg/L	713.6

Post Site Check			
Time:	0953		
	pH	Temp °C	Reading
Buffer 7		21.80	7.01
Conductivity			
Buffer 5000		21.13	4983

Date:			Time:			
	pH	Temp °C	Pre Cal	Post Cal	Post Cal Range	mv Range +/-
Buffer 7					6.95-7.05	0 +/- 50
Buffer 10					9.95-10.05	-180 +/- 50
Conductivity						Check
Buffer 10000					±10%	Buffer 5000
ORP						
231 mV @ 25C					±10 mV	
DO						
					Barometric Pressure (mm Hg)	
					mg/L	

Time:			
	pH	Temp °C	Reading
Buffer 7			
Conductivity			
Buffer 5000			

**Laboratories, Inc.**2616 E. Broadway
Bismarck, ND 58501
Phone (701) 258-9720

Chain of Custody Record

Project Name: MDU Heskett	Event: Aug 2018	Work Order Number: 82-2018
Report To: MDU Attn: Samantha Marshall Address: 400 N. 4th St Bismarck, ND 58501 phone: 701-222-7829 email:	Carbon Copy: Attn: Address:	Name of Sampler(s): Darren Nieswag

Sample Information					Bottle Type				Field Parameters			Analysis
Lab Number	Sample ID	Date	Time	Sample Type	1 liter	500mL Nitric	500mL Nitric (filtered)	250 mL Sulfuric	Temp (°C)	Spec. Cond.	pH	Analysis Required
W2547	2-90	13 Aug 18	0912	GW	X				12.12	17281	6.89	Fluoride

Comments:

Relinquished By:		Sample Condition:	
Name:	Date/Time	Location:	Temp (°C)
1 <i>[Signature]</i>	13 Aug 18 0955	Log In Walk In #2	5.8 01 ice TM562 / TM588
2			

Received by:	
Name:	Date/Time
<i>N. Buchmann</i>	13 Aug 18 0955



CASE NARRATIVE – AMENDED 29 JAN 19 (REPORTING)

MVTL Lab Reference No/SDG: 201882-2588
Client: Montana Dakota Utilities
Location: MDU Heskett
Project Identification: CCR October 2018
MVTL Laboratory Identifications: 18-W3236 through 18-W3243
Page 1 of 2

MDU Sample Identification	MVTL Laboratory #
13	18-W3236
Dup1	18-W3237
102	18-W3238
70	18-W3239
101	18-W3240
103	18-W3241
44R	18-W3242
FB1	18-W3243

I. RECEIPT

- All samples were received at the laboratory on 2 Oct 18 at 1406.
- Samples were collected and hand delivered by MVTL Field Service personnel to the laboratory.
- Samples were received on ice and evidence of cooling had begun.
 - Temperature of samples upon receipt was 4.0°C.
- All samples were properly preserved unless noted here and/or flagged on the individual analytical laboratory report.
- No other exceptions on sample receipt were encountered on this sample set unless noted here.

II. HOLDING TIMES

- With the exception of pH, all holding times were met for both preparation and analysis unless noted here.

III. METHODS

- Approved methodology was followed for all sample analyses.

IV. ANALYSIS

- All acceptance criteria were met for calibration, method blanks, laboratory control samples, laboratory fortified matrix/matrix duplicates unless noted here and/or flagged on the individual analytical laboratory report.
 - For some analytes, the reported results were elevated due to instrument performance at the lower limit of quantitation (LLOQ).
 - For some analytes, the reported results were elevated due to additional dilutions required to minimize the effects of sample matrix.



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CASE NARRATIVE – AMENDED 29 JAN 19 (REPORTING)

MVTL Lab Reference No/SDG: 201882-2588
Client: Montana Dakota Utilities
Location: MDU Heskett
Project Identification: CCR October 2018
MVTL Laboratory Identifications: 18-W3236 through 18-W3243
Page 2 of 2

V. REPORTING

- Per email dated 21 Jan 19 from Terri Olson with Barr, the reports were amended to report only Appendix III parameters on one report and only Appendix IV parameters on a separate report.

All laboratory data has been approved by MVTL Laboratories.

SIGNED: Claudette Carroll DATE: 29 Jan 19
Claudette Carroll - MVTL Bismarck Laboratory Manager



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MEMBER
ACIL

Quality Control Report – Amended 29 Jan 19

Lab IDs: 18-W3236 to 18-W3243

Project: MDU Heskett

Work Order: 201882-2588

Analyte	LCS Spike Amt	LCS Rec %	LCS % Rec Limits	Matrix Spike Amt	Matrix Spike ID	Matrix Spike Orig Result	Matrix Spike Result	Matrix Spike Rec %	Matrix Spike % Rec Limits	MSD/ Dup Orig Result	MSD/ Dup Result	MSD Rec %	MSD/ Dup RPD	MSD/ Dup RPD Limit (<)	Known Rec (%)	Known % Rec Limits	Method Blank
Boron - Total mg/l	0.40	108	80-120	2.00	18-D3537	1.48	3.62	107	75-125	3.62	3.68	110	1.6	20	-	-	< 0.1
	0.40	112	80-120	8.00	18-M2561	< 2	8.96	112	75-125	8.96	8.94	112	0.2	20	-	-	< 0.1
	0.40	108	80-120	2.00	18-W3236	0.66	2.62	98	75-125	2.62	2.58	96	1.5	20	-	-	< 0.1
	0.40	108	80-120	2.00	18-W3264	0.96	2.82	93	75-125	2.82	2.93	98	3.8	20	-	-	< 0.1
Calcium - Total mg/l	20.0	112	80-120	100	18W3220q	91.9	185	93	75-125	185	187	95	1.1	20	-	-	< 1
	20.0	114	80-120	500	18W3240q	386	935	110	75-125	935	940	111	0.5	20	-	-	< 1
															-	-	< 1
Chloride mg/l	30.0	100	80-120	30.0	18-W3202	17.0	47.0	100	80-120	47.0	48.0	103	2.1	20	-	-	< 1
	30.0	103	80-120	30.0	18-W3238	6.4	35.3	96	80-120	35.3	38.2	106	7.9	20	-	-	< 1
	30.0	101	80-120												-	-	< 1
	30.0	100	80-120												-	-	< 1
Fluoride mg/l	0.50	104	90-110	0.500	18-W3236	0.94	1.40	92	80-120	1.40	1.40	92	0.0	20	-	-	< 0.1
				0.500	18-W3239	0.34	0.84	100	80-120	0.84	0.84	100	0.0	20	-	-	< 0.1
pH units	-	-	-	-	-	-	-	-	-	7.4	7.4	-	0.0	20	-	-	-
	-	-	-	-	-	-	-	-	-	7.2	7.2	-	0.0	20	-	-	-
Sulfate mg/l	100	112	80-120	10000	18-W3238	5740	17500	118	80-120	17500	17500	118	0.0	20	-	-	< 5
	100	103	80-120	100	18-W3243	< 5	103	103	80-120	103	97.3	97	5.7	20	-	-	< 5
Total Dissolved Solids mg/l	-	-	-	-	-	-	-	-	-	< 10	< 10	-	0.0	20	-	-	< 10

Approved by: C. Cantel
29 Jan 19

Claudette Carroll

From: Terri A. Olson <TOlson@barr.com>
Sent: Monday, January 21, 2019 12:15 PM
To: Claudette Carroll
Cc: 'Marshall, Samantha'; Stephanie A. Theriault
Subject: Re: Reports revisions

Follow Up Flag: Follow up
Flag Status: Flagged

Hi Claudette,

We haven't emailed in a while, hope you're having a good new year.

For the two Heskett CCR reports (201882-2588 and 201882-2619), we will need the Appendix III and Appendix IV CCR analytes split into two reports. The field parameters (pH, temperature, conductivity) can be reported in only the Appendix III report or you can include in both.

- Appendix III – see 201882-0637 for example
 - Chloride
 - TDS
 - Fluoride
 - pH
 - Sulfate
 - Boron
 - Calcium
- Appendix IV
 - Antimony
 - Arsenic
 - Barium
 - Beryllium
 - Cadmium
 - Chromium
 - Cobalt
 - Lead
 - Lithium
 - Molybdenum
 - Selenium
 - Thallium
 - Mercury
 - Fluoride is in both lists so OK to have just in Appendix III since we wouldn't report Appendix IV only

We have discussed the report split with Sam at MDU and she was OK with it. I have copied her on this email. We need ASAP as our report is due at the end of this month.

Let me know if you have any questions.

Thank-you,

Terri A. Olson

Senior Data Quality Specialist
Minneapolis, MN office: 952.842.3578
TOlson@barr.com
www.barr.com

resourceful. naturally.



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Page: 3 of 8

Amended 29 Jan 19 (App III/App IV) - CCR

Samantha Davies
 Montana Dakota Utilities
 5181 Southgate Dr
 Billings MT 59102

Report Date: 19 Oct 18
 Lab Number: 18-W3238
 Work Order #: 82-2588
 Account #: 002800
 Date Sampled: 2 Oct 18 9:30
 Date Received: 2 Oct 18 14:06
 Sampled By: MVTL Field Services

Project Name: MDU Heskett

PO #: 169846 OP

Sample Description: 102

Temp at Receipt: 4.0C ROI

Event and Year: Fall 2018

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
pH - Field	6.77	units	NA	SM 4500 H+ B	2 Oct 18 9:30	JSM
pH	* 7.3	units	0.1	SM4500 H+ B	3 Oct 18 17:00	SVS
Temperature - Field	9.02	Degrees C	NA	SM 2550B	2 Oct 18 9:30	JSM
Conductivity - Field	9098	umhos/cm	1	EPA 120.1	2 Oct 18 9:30	JSM
Fluoride	0.16	mg/l	0.10	SM4500-F-C	3 Oct 18 17:00	SVS
Sulfate	5740	mg/l	5.00	ASTM D516-07	4 Oct 18 15:36	EV
Chloride	6.4	mg/l	1.0	SM4500-Cl-E	3 Oct 18 9:46	EMS
Total Dissolved Solids	8780	mg/l	10	I1750-85	5 Oct 18 8:20	SVS
Calcium - Total	472	mg/l	1.0	6010D	3 Oct 18 15:42	BMB
Boron - Total	1.51	mg/l	0.10	6010D	8 Oct 18 11:49	SZ

* Holding time exceeded

Approved by: Claudette K. Carroll ^{CC} 29 Jan 19

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

The reporting limit was elevated for any analyte requiring a dilution as coded below:
 @ = Due to sample matrix # = Due to concentration of other analytes
 ! = Due to sample quantity + = Due to internal standard response

CERTIFICATION: ND # ND-00016



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Amended 29 Jan 19 (App III/App IV) - CCR

Samantha Davies
 Montana Dakota Utilities
 5181 Southgate Dr
 Billings MT 59102

Report Date: 19 Oct 18
 Lab Number: 18-W3239
 Work Order #: 82-2588
 Account #: 002800
 Date Sampled: 2 Oct 18 11:05
 Date Received: 2 Oct 18 14:06
 Sampled By: MVTL Field Services

Project Name: MDU Heskett

PO #: 169846 OP

Sample Description: 70

Temp at Receipt: 4.0C ROI

Event and Year: Fall 2018

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
pH - Field	6.91	units	NA	SM 4500 H+ B	2 Oct 18 11:05	JSM
pH	* 7.5	units	0.1	SM4500 H+ B	3 Oct 18 17:00	SVS
Temperature - Field	9.79	Degrees C	NA	SM 2550B	2 Oct 18 11:05	JSM
Conductivity - Field	3704	umhos/cm	1	EPA 120.1	2 Oct 18 11:05	JSM
Fluoride	0.34	mg/l	0.10	SM4500-F-C	3 Oct 18 17:00	SVS
Sulfate	1940	mg/l	5.00	ASTM D516-07	4 Oct 18 15:36	EV
Chloride	49.6	mg/l	1.0	SM4500-Cl-E	3 Oct 18 9:46	EMS
Total Dissolved Solids	3100	mg/l	10	I1750-85	5 Oct 18 8:20	SVS
Calcium - Total	341	mg/l	1.0	6010D	3 Oct 18 16:42	BMB
Boron - Total	0.46	mg/l	0.10	6010D	8 Oct 18 11:49	SZ

* Holding time exceeded

Approved by:

Claudette K. Carroll

CE
29 Jan 19

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

The reporting limit was elevated for any analyte requiring a dilution as coded below:
 @ = Due to sample matrix # = Due to concentration of other analytes
 ! = Due to sample quantity + = Due to internal standard response

CERTIFICATION: ND # ND-00016



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Amended 29 Jan 19 (App III/App IV) - CCR

Samantha Davies
 Montana Dakota Utilities
 5181 Southgate Dr
 Billings MT 59102

Report Date: 19 Oct 18
 Lab Number: 18-W3240
 Work Order #: 82-2588
 Account #: 002800
 Date Sampled: 2 Oct 18 13:02
 Date Received: 2 Oct 18 14:06
 Sampled By: MVTL Field Services

Project Name: MDU Heskett

PO #: 169846 OP

Sample Description: 101

Temp at Receipt: 4.0C ROI

Event and Year: Fall 2018

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
pH - Field	6.62	units	NA	SM 4500 H+ B	2 Oct 18 13:02	JSM
pH	* 7.2	units	0.1	SM4500 H+ B	3 Oct 18 17:00	SVS
Temperature - Field	11.9	Degrees C	NA	SM 2550B	2 Oct 18 13:02	JSM
Conductivity - Field	4695	umhos/cm	1	EPA 120.1	2 Oct 18 13:02	JSM
Fluoride	0.10	mg/l	0.10	SM4500-F-C	3 Oct 18 17:00	SVS
Sulfate	3180	mg/l	5.00	ASTM D516-07	4 Oct 18 15:36	EV
Chloride	18.4	mg/l	1.0	SM4500-Cl-E	3 Oct 18 9:46	EMS
Total Dissolved Solids	4720	mg/l	10	I1750-85	5 Oct 18 8:20	SVS
Calcium - Total	386	mg/l	1.0	6010D	3 Oct 18 16:42	BMB
Boron - Total	1.08	mg/l	0.10	6010D	8 Oct 18 11:49	SZ

* Holding time exceeded

Approved by:

Claudette K. Carroll

*CC
29 Jan 19*

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

The reporting limit was elevated for any analyte requiring a dilution as coded below:
 @ = Due to sample matrix # = Due to concentration of other analytes
 ! = Due to sample quantity + = Due to internal standard response

CERTIFICATION: ND # ND-00016



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Amended 29 Jan 19 (App III/App IV) - CCR

Samantha Davies
 Montana Dakota Utilities
 5181 Southgate Dr
 Billings MT 59102

Report Date: 19 Oct 18
 Lab Number: 18-W3241
 Work Order #: 82-2588
 Account #: 002800
 Date Sampled: 1 Oct 18 13:20
 Date Received: 2 Oct 18 14:06
 Sampled By: MVTL Field Services

Project Name: MDU Heskett

PO #: 169846 OP

Sample Description: 103

Temp at Receipt: 4.0C ROI

Event and Year: Fall 2018

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
pH - Field	6.67	units	NA	SM 4500 H+ B	1 Oct 18 13:20	JSM
pH	* 7.2	units	0.1	SM4500 H+ B	3 Oct 18 17:00	SVS
Temperature - Field	9.17	Degrees C	NA	SM 2550B	1 Oct 18 13:20	JSM
Conductivity - Field	4960	umhos/cm	1	EPA 120.1	1 Oct 18 13:20	JSM
Fluoride	0.30	mg/l	0.10	SM4500-F-C	3 Oct 18 17:00	SVS
Sulfate	3180	mg/l	5.00	ASTM D516-07	4 Oct 18 15:36	EV
Chloride	109	mg/l	1.0	SM4500-Cl-E	3 Oct 18 9:46	EMS
Total Dissolved Solids	4780	mg/l	10	I1750-85	5 Oct 18 8:20	SVS
Calcium - Total	580	mg/l	1.0	6010D	3 Oct 18 16:42	BMB
Boron - Total	0.13	mg/l	0.10	6010D	8 Oct 18 11:49	SZ

* Holding time exceeded

Approved by:

Claudette K. Carroll

*CC
29 Jan 19*

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

The reporting limit was elevated for any analyte requiring a dilution as coded below:

@ = Due to sample matrix
 ! = Due to sample quantity

= Due to concentration of other analytes
 + = Due to internal standard response

CERTIFICATION: ND # ND-00016



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Amended 29 Jan 19 (App III/App IV) - CCR

Samantha Davies
 Montana Dakota Utilities
 5181 Southgate Dr
 Billings MT 59102

Report Date: 19 Oct 18
 Lab Number: 18-W3242
 Work Order #: 82-2588
 Account #: 002800
 Date Sampled: 1 Oct 18 14:35
 Date Received: 2 Oct 18 14:06
 Sampled By: MVTL Field Services

Project Name: MDU Heskett

PO #: 169846 OP

Sample Description: 44R

Temp at Receipt: 4.0C ROI

Event and Year: Fall 2018

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
pH - Field	6.52	units	NA	SM 4500 H+ B	1 Oct 18 14:35	JSM
pH	* 7.2	units	0.1	SM4500 H+ B	3 Oct 18 17:00	SVS
Temperature - Field	9.21	Degrees C	NA	SM 2550B	1 Oct 18 14:35	JSM
Conductivity - Field	8937	umhos/cm	1	EPA 120.1	1 Oct 18 14:35	JSM
Fluoride	0.67	mg/l	0.10	SM4500-F-C	3 Oct 18 17:00	SVS
Sulfate	6320	mg/l	5.00	ASTM D516-07	10 Oct 18 12:18	EV
Chloride	227	mg/l	1.0	SM4500-Cl-E	3 Oct 18 9:46	EMS
Total Dissolved Solids	10400	mg/l	10	I1750-85	5 Oct 18 8:20	SVS
Calcium - Total	456	mg/l	1.0	6010D	3 Oct 18 16:42	BMB
Boron - Total	< 0.5 @	mg/l	0.10	6010D	8 Oct 18 11:49	SZ

* Holding time exceeded

Approved by:

Claudette K. Carroll ^{CC} 29 Jan 19

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

The reporting limit was elevated for any analyte requiring a dilution as coded below:
 @ = Due to sample matrix # = Due to concentration of other analytes
 ! = Due to sample quantity + = Due to internal standard response

CERTIFICATION: ND # ND-00016



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Amended 29 Jan 19 (App III/App IV) - CCR

Samantha Davies
Montana Dakota Utilities
5181 Southgate Dr
Billings MT 59102

Report Date: 19 Oct 18
Lab Number: 18-W3243
Work Order #: 82-2588
Account #: 002800
Date Sampled: 2 Oct 18
Date Received: 2 Oct 18 14:06
Sampled By: MVTL Field Services

Project Name: MDU Heskett

PO #: 169846 OP

Sample Description: FB1

Temp at Receipt: 4.0C ROI

Event and Year: Fall 2018

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
pH	* 6.1	units	0.1	SM4500 H+ B	3 Oct 18 17:00	SVS
Fluoride	< 0.1	mg/l	0.10	SM4500-F-C	3 Oct 18 17:00	SVS
Sulfate	< 5	mg/l	5.00	ASTM D516-07	10 Oct 18 12:18	EV
Chloride	< 1	mg/l	1.0	SM4500-CL-E	3 Oct 18 9:46	EMS
Total Dissolved Solids	< 10	mg/l	10	I1750-85	5 Oct 18 8:20	SVS
Calcium - Total	< 1	mg/l	1.0	6010D	3 Oct 18 16:42	BMB
Boron - Total	< 0.1	mg/l	0.10	6010D	8 Oct 18 12:49	SZ

* Holding time exceeded

Approved by:

Claudette K. Carroll

*CC
29 Jan 19*

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

The reporting limit was elevated for any analyte requiring a dilution as coded below:

@ = Due to sample matrix # = Due to concentration of other analytes
! = Due to sample quantity + = Due to internal standard response

CERTIFICATION: ND # ND-00016



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Amended 29 Jan 19 (App III/App IV) - CCR

Samantha Davies
Montana Dakota Utilities
5181 Southgate Dr
Billings MT 59102

Report Date: 19 Oct 18
Lab Number: 18-W3236
Work Order #: 82-2588
Account #: 002800
Date Sampled: 1 Oct 18 9:05
Date Received: 2 Oct 18 14:06
Sampled By: MVTL Field Services

Project Name: MDU Heskett

PO #: 169846 OP

Sample Description: 13

Temp at Receipt: 4.0C ROI

Event and Year: Fall 2018

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
pH - Field	6.93	units	NA	SM 4500 H+ B	1 Oct 18 9:05	JSM
pH	* 7.3	units	0.1	SM4500 H+ B	3 Oct 18 17:00	SVS
Temperature - Field	8.90	Degrees C	NA	SM 2550B	1 Oct 18 9:05	JSM
Conductivity - Field	9887	umhos/cm	1	EPA 120.1	1 Oct 18 9:05	JSM
Fluoride	0.94	mg/l	0.10	SM4500-F-C	3 Oct 18 17:00	SVS
Sulfate	7300	mg/l	5.00	ASTM D516-07	4 Oct 18 15:36	EV
Chloride	76.1	mg/l	1.0	SM4500-Cl-E	3 Oct 18 9:13	EMS
Total Dissolved Solids	10400	mg/l	10	I1750-85	5 Oct 18 8:20	SVS
Calcium - Total	420	mg/l	1.0	6010D	3 Oct 18 15:42	BMB
Boron - Total	0.66	mg/l	0.10	6010D	8 Oct 18 11:49	SZ

* Holding time exceeded

Approved by:

Claudette K. Carroll

29 Jan 19

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

The reporting limit was elevated for any analyte requiring a dilution as coded below:
@ = Due to sample matrix # = Due to concentration of other analytes
! = Due to sample quantity + = Due to internal standard response

CERTIFICATION: ND # ND-00016



MINNESOTA VALLEY TESTING LABORATORIES, INC.

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Amended 29 Jan 19 (App III/App IV) - CCR

Samantha Davies
 Montana Dakota Utilities
 5181 Southgate Dr
 Billings MT 59102

Report Date: 19 Oct 18
 Lab Number: 18-W3237
 Work Order #: 82-2588
 Account #: 002800
 Date Sampled: 1 Oct 18
 Date Received: 2 Oct 18 14:06
 Sampled By: MVTL Field Services

Project Name: MDU Heskett

Sample Description: Dup1

PO #: 169846 OP

Event and Year: Fall 2018

Temp at Receipt: 4.0C ROI

	As Received Result	units	Method RL	Method Reference	Date Analyzed	Analyst
pH	* 7.4	units	0.1	SM4500 H+ B	3 Oct 18 17:00	SVS
Fluoride	0.95	mg/l	0.10	SM4500-F-C	3 Oct 18 17:00	SVS
Sulfate	7060	mg/l	5.00	ASTM D516-07	4 Oct 18 15:36	EV
Chloride	75.5	mg/l	1.0	SM4500-Cl-E	3 Oct 18 9:46	EMS
Total Dissolved Solids	10500	mg/l	10	I1750-85	5 Oct 18 8:20	SVS
Calcium - Total	442	mg/l	1.0	6010D	3 Oct 18 15:42	BMB
Boron - Total	0.64	mg/l	0.10	6010D	8 Oct 18 11:49	SZ

* Holding time exceeded

Approved by: Claudette K. Carroll ^{CC} 29 Jan 19

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

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 ! = Due to sample quantity + = Due to internal standard response

CERTIFICATION: ND # ND-00016



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Amended 29 Jan 19 (App III/App IV) - CCR

Samantha Davies
 Montana Dakota Utilities
 5181 Southgate Dr
 Billings MT 59102

Report Date: 19 Oct 18
 Lab Number: 18-W3238
 Work Order #: 82-2588
 Account #: 002800
 Date Sampled: 2 Oct 18 9:30
 Date Received: 2 Oct 18 14:06
 Sampled By: MVTL Field Services

Project Name: MDU Heskett

PO #: 169846 OP

Sample Description: 102

Temp at Receipt: 4.0C ROI

Event and Year: Fall 2018

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
pH - Field	6.77	units	NA	SM 4500 H+ B	2 Oct 18 9:30	JSM
pH	* 7.3	units	0.1	SM4500 H+ B	3 Oct 18 17:00	SVS
Temperature - Field	9.02	Degrees C	NA	SM 2550B	2 Oct 18 9:30	JSM
Conductivity - Field	9098	umhos/cm	1	EPA 120.1	2 Oct 18 9:30	JSM
Fluoride	0.16	mg/l	0.10	SM4500-F-C	3 Oct 18 17:00	SVS
Sulfate	5740	mg/l	5.00	ASTM D516-07	4 Oct 18 15:36	EV
Chloride	6.4	mg/l	1.0	SM4500-Cl-E	3 Oct 18 9:46	EMS
Total Dissolved Solids	8780	mg/l	10	I1750-85	5 Oct 18 8:20	SVS
Calcium - Total	472	mg/l	1.0	6010D	3 Oct 18 15:42	BMB
Boron - Total	1.51	mg/l	0.10	6010D	8 Oct 18 11:49	SZ

* Holding time exceeded

Approved by:

Claudette K. Carroll

*CC
29 Jan 19*

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

The reporting limit was elevated for any analyte requiring a dilution as coded below:

@ = Due to sample matrix
 ! = Due to sample quantity

= Due to concentration of other analytes
 + = Due to internal standard response

CERTIFICATION: ND # ND-00016



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Amended 29 Jan 19 (App III/App IV) - CCR

Samantha Davies
Montana Dakota Utilities
5181 Southgate Dr
Billings MT 59102

Report Date: 19 Oct 18
Lab Number: 18-W3239
Work Order #: 82-2588
Account #: 002800
Date Sampled: 2 Oct 18 11:05
Date Received: 2 Oct 18 14:06
Sampled By: MVTL Field Services

Project Name: MDU Heskett

PO #: 169846 OP

Sample Description: 70

Temp at Receipt: 4.0C ROI

Event and Year: Fall 2018

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
pH - Field	6.91	units	NA	SM 4500 H+ B	2 Oct 18 11:05	JSM
pH	* 7.5	units	0.1	SM4500 H+ B	3 Oct 18 17:00	SVS
Temperature - Field	9.79	Degrees C	NA	SM 2550B	2 Oct 18 11:05	JSM
Conductivity - Field	3704	umhos/cm	1	EPA 120.1	2 Oct 18 11:05	JSM
Fluoride	0.34	mg/l	0.10	SM4500-F-C	3 Oct 18 17:00	SVS
Sulfate	1940	mg/l	5.00	ASTM D516-07	4 Oct 18 15:36	EV
Chloride	49.6	mg/l	1.0	SM4500-Cl-E	3 Oct 18 9:46	EMS
Total Dissolved Solids	3100	mg/l	10	I1750-85	5 Oct 18 8:20	SVS
Calcium - Total	341	mg/l	1.0	6010D	3 Oct 18 16:42	BMB
Boron - Total	0.46	mg/l	0.10	6010D	8 Oct 18 11:49	SZ

* Holding time exceeded

Approved by:

Claudette K. Carroll

*CC
29 Jan 19*

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

The reporting limit was elevated for any analyte requiring a dilution as coded below:

@ = Due to sample matrix
! = Due to sample quantity

= Due to concentration of other analytes
+ = Due to internal standard response

CERTIFICATION: ND # ND-00016



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Amended 29 Jan 19 (App III/App IV) - CCR

Samantha Davies
Montana Dakota Utilities
5181 Southgate Dr
Billings MT 59102

Report Date: 19 Oct 18
Lab Number: 18-W3240
Work Order #: 82-2588
Account #: 002800
Date Sampled: 2 Oct 18 13:02
Date Received: 2 Oct 18 14:06
Sampled By: MVTL Field Services

Project Name: MDU Heskett

PO #: 169846 OP

Sample Description: 101

Temp at Receipt: 4.0C ROI

Event and Year: Fall 2018

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
pH - Field	6.62	units	NA	SM 4500 H+ B	2 Oct 18 13:02	JSM
pH	* 7.2	units	0.1	SM4500 H+ B	3 Oct 18 17:00	SVS
Temperature - Field	11.9	Degrees C	NA	SM 2550B	2 Oct 18 13:02	JSM
Conductivity - Field	4695	umhos/cm	1	EPA 120.1	2 Oct 18 13:02	JSM
Fluoride	0.10	mg/l	0.10	SM4500-F-C	3 Oct 18 17:00	SVS
Sulfate	3180	mg/l	5.00	ASTM D516-07	4 Oct 18 15:36	EV
Chloride	18.4	mg/l	1.0	SM4500-Cl-E	3 Oct 18 9:46	EMS
Total Dissolved Solids	4720	mg/l	10	I1750-85	5 Oct 18 8:20	SVS
Calcium - Total	386	mg/l	1.0	6010D	3 Oct 18 16:42	BMB
Boron - Total	1.08	mg/l	0.10	6010D	8 Oct 18 11:49	SZ

* Holding time exceeded

Approved by:

Claudette K. Carroll

*LC
29 Jan 19*

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

The reporting limit was elevated for any analyte requiring a dilution as coded below:

@ = Due to sample matrix # = Due to concentration of other analytes
! = Due to sample quantity + = Due to internal standard response

CERTIFICATION: ND # ND-00016



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Amended 29 Jan 19 (App III/App IV) - CCR

Samantha Davies
 Montana Dakota Utilities
 5181 Southgate Dr
 Billings MT 59102

Report Date: 19 Oct 18
 Lab Number: 18-W3243
 Work Order #: 82-2588
 Account #: 002800
 Date Sampled: 2 Oct 18
 Date Received: 2 Oct 18 14:06
 Sampled By: MVTL Field Services

Project Name: MDU Heskett

PO #: 169846 OP

Sample Description: FB1

Temp at Receipt: 4.0C ROI

Event and Year: Fall 2018

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
pH	* 6.1	units	0.1	SM4500 H+ B	3 Oct 18 17:00	SVS
Fluoride	< 0.1	mg/l	0.10	SM4500-F-C	3 Oct 18 17:00	SVS
Sulfate	< 5	mg/l	5.00	ASTM D516-07	10 Oct 18 12:18	EV
Chloride	< 1	mg/l	1.0	SM4500-Cl-E	3 Oct 18 9:46	EMS
Total Dissolved Solids	< 10	mg/l	10	I1750-85	5 Oct 18 8:20	SVS
Calcium - Total	< 1	mg/l	1.0	6010D	3 Oct 18 16:42	BMB
Boron - Total	< 0.1	mg/l	0.10	6010D	8 Oct 18 12:49	SZ

* Holding time exceeded

Approved by: Claudette K. Carroll *cc* *29 Jan 19*

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

The reporting limit was elevated for any analyte requiring a dilution as coded below:

@ = Due to sample matrix # = Due to concentration of other analytes
 ! = Due to sample quantity + = Due to internal standard response

CERTIFICATION: ND # ND-00016

MVTL Calibration Worksheet

Site: MDU Heskett

Technician: Jerry Ph

Instrument
(Circle One):

#1 650 MDS 08F400203

#2 650 MDS 04H14736

#3 556 MPS 12E102056

Pre Site Calibration							
Date: <u>1 Oct 18</u>		Time: <u>0810</u>					
pH	Temp °C	Pre Cal	Post Cal	Post Cal Range	mv	mv Range +/- 50	
Buffer 7	<u>17.16</u>	<u>7.16</u>	<u>7.00</u>	6.95-7.05	<u>-25.4</u>	0 +/- 50	
Buffer 10	<u>17.39</u>	<u>9.97</u>	<u>10.00</u>	9.95-10.05	<u>-199.4</u>	-180 +/- 50	
Buffer 4	<u>16.88</u>	<u>4.00</u>	<u>4.00</u>	4.95-5.05	<u>152.7</u>	180 +/- 50	
Conductivity						Check	
Buffer 1413	<u>17.40</u>	<u>1412</u>	<u>1413</u>	±10%	Buffer 5000	<u>4987</u>	
ORP						±10 mV	
231 mV @ 25C	<u>15.51</u>	<u>236.0</u>	<u>243.8</u>				
DO				Barometric Pressure (mm Hg)			
	<u>12.50</u>	<u>10.74</u>	<u>100.0%</u>	mg/L	<u>766.32</u>		

Post Site Check		
Time: <u>1500</u>		
pH	Temp °C	Reading
Buffer 7	<u>18.26</u>	<u>7.02</u>
Conductivity		
Buffer 5000	<u>18.13</u>	<u>4972</u>

Pre Site Calibration							
Date: <u>2 Oct 18</u>		Time: <u>0900</u>					
pH	Temp °C	Pre Cal	Post Cal	Post Cal Range	mv	mv Range +/- 50	
Buffer 7	<u>13.99</u>	<u>7.01</u>	<u>7.00</u>	6.95-7.05	<u>-23.6</u>	0 +/- 50	
Buffer 10	<u>13.69</u>	<u>9.96</u>	<u>10.00</u>	9.95-10.05	<u>-195.4</u>	-180 +/- 50	
Buffer 4	<u>12.86</u>	<u>3.99</u>	<u>4.00</u>	4.95-5.05	<u>147.9</u>	180 +/- 50	
Conductivity						Check	
Buffer 1413	<u>14.40</u>	<u>1421</u>	<u>1413</u>	±10%	Buffer 5000	<u>4979</u>	
ORP						±10 mV	
231 mV @ 25C	<u>12.64</u>	<u>250.7</u>	<u>244.0</u>				
DO				Barometric Pressure (mm Hg)			
	<u>11.01</u>	<u>11.03</u>	<u>100.0%</u>	mg/L	<u>760.22</u>		

Post Site Check		
Time: <u>1330</u>		
pH	Temp °C	Reading
Buffer 7	<u>18.52</u>	<u>7.03</u>
Conductivity		
Buffer 5000	<u>18.78</u>	<u>4963</u>



Field Datasheet

Groundwater Assessment

2616 E. Broadway Ave, Bismarck, ND
Phone: (701) 258-9720

Company: MDU Heskett
Event: Fall 2018
Sample ID: 13
Sampling Personal: Jerry Heskett

Weather Conditions: Temp: 40 °F Wind: S @ 5-10 Precip: Sunny / Partly Cloudy / Cloudy

Well Information

Well Locked?	Yes	No	
Well Labeled?	Yes	No	
Casing Straight?	Yes	No	
Grout Seal Intact?	Yes	No	Not Visible
Repairs Necessary:			
Casing Diameter:	2"		
Water Level Before Purge:	30.74		ft
Depth to Top of Pump:	— ft		
Water Level After Sample:	32.76		ft
Measurement Method:	Electric Water Level Indicator		

Sampling Information

Purging Method:	Bladder			
Sampling Method:	Bladder			
Dedicated Equip?:	Yes	No		
Duplicate Sample?:	Yes	No		
Duplicate Sample ID:	Dup 1			
Purge Date:	1 Oct 18	Time Purging Began:	0815	am/pm
Well Purged Dry?	Yes	No	Time Purged Dry:	— am/pm
Sample Date:	1 Oct 18	Time of Sampling:	0905	am/pm
Bottle List:	1L Raw	500mL Nitric	500mL Nitric (filtered)	250mL Sulfuric

Control Settings		
Purge:	5	sec.
Recover:	55	sec.
PSI:	30	

Field Measurements

Stabilization (3 consecutive)	Temp (°C)	Spec. Cond. ±5%	pH ±0.1	DO (mg/L) ±10%	ORP (mV) ±20 mV	Turbidity (NTU) ±10%	Water Level (ft) 0.25 ft	Pumping Rate ml/min	mL Removed	Description: Clarity, Color, Odor, Ect. Clear, Slightly Turbid, Turbid	
1	0820	8.99	9926	6.88	2.61	241.4	4.99	30.81	100.0	500.0	Clear
2	0850	8.96	9868	6.93	2.26	250.2	4.87	31.98	100.0	3000.0	Clear
3	0855	9.01	9860	6.93	2.32	258.3	4.52	32.16	100.0	500.0	Clear
4	0900	8.98	9867	6.93	2.38	263.0	4.63	32.27	100.0	500.0	Clear
5	0905	8.90	9887	6.93	2.39	265.1	4.37	32.33	100.0	500.0	Clear
6											
7											
8											
9											
10											

Stabilized: Yes No
Comments:

Total Volume Removed: ~~4500.0~~ 5000.0 mL



Field Datasheet

Groundwater Assessment

2616 E. Broadway Ave, Bismarck, ND

Phone: (701) 258-9720

Company: MDU Heskett
 Event: Fall 2018
 Sample ID: 102
 Sampling Personal: Jerry [Signature]

Weather Conditions: Temp: 50 °F Wind: S @ 5-10 Precip: Sunny / Partly Cloudy / ~~Cloudy~~

Well Information

Well Locked?	Yes <input checked="" type="checkbox"/>	No <input type="checkbox"/>	
Well Labeled?	Yes <input checked="" type="checkbox"/>	No <input type="checkbox"/>	
Casing Straight?	Yes <input checked="" type="checkbox"/>	No <input type="checkbox"/>	
Grout Seal Intact?	Yes <input checked="" type="checkbox"/>	No <input type="checkbox"/>	Not Visible
Repairs Necessary:			
Casing Diameter:	2"		
Water Level Before Purge:	18.80		ft
Depth to Top of Pump:	_____ ft		
Water Level After Sample:	20.08		ft
Measurement Method:	Electric Water Level Indicator		

Sampling Information

Purging Method:	Bladder			
Sampling Method:	Bladder			
Dedicated Equip?:	Yes <input checked="" type="checkbox"/>	No <input type="checkbox"/>	Control Settings	
Duplicate Sample?:	Yes <input type="checkbox"/>	No <input checked="" type="checkbox"/>	Purge:	5 sec.
Duplicate Sample ID:	_____		Recover:	55 sec.
			PSI:	20
Purge Date:	2 Oct 18	Time Purging Began:	0850	am/pm
Well Purged Dry?	Yes <input checked="" type="checkbox"/>	No <input type="checkbox"/>	Time Purged Dry:	_____ am/pm
Sample Date:	2 Oct 18	Time of Sampling:	0930	am/pm
Bottle List:	1L Raw	500mL Nitric	500mL Nitric (filtered)	250mL Sulfuric

Field Measurements

SEQ #	Stabilization (3 consecutive) Time	Temp (°C)	Spec. Cond. ±5%	pH ±0.1	DO (mg/L) ±10%	ORP (mV) ±20 mV	Turbidity (NTU) ±10%	Water Level (ft) 0.25 ft	Pumping Rate ml/min	mL Removed	Description: Clarity, Color, Odor, Ect. Clear, Slightly Turbid, Turbid
1	0855	9.13	9456	6.86	2.34	10.6	2.56	18.92	100.0	500.0	Clear
2	0915	8.70	9403	6.81	1.81	-11.2	1.31	19.64	100.0	200.0	Clear
3	0920	8.84	9079	6.78	1.47	-26.2	1.34	19.80	100.0	500.0	Clear
4	0925	8.75	9125	6.78	1.48	-26.8	1.40	19.85	100.0	500.0	Clear
5	0930	9.02	9098	6.77	1.41	-27.6	1.46	19.96	100.0	500.0	Clear
6											
7											
8											
9											
10											

Stabilized: Yes No

Total Volume Removed: 4,000.0 mL

Comments:



Field Datasheet

Groundwater Assessment

2616 E. Broadway Ave, Bismarck, ND

Phone: (701) 258-9720

Company: MDU Heskett

Event: Fall 2018

Sample ID: 70

Sampling Personal: Jerry Heskett

Weather Conditions: Temp: 50 °F Wind: S @ 5-10 Precip: Sunny (Partly Cloudy) / Cloudy

Well Information

Well Locked?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	
Well Labeled?	<u>Yes</u> No	
Casing Straight?	<u>Yes</u> No	
Grout Seal Intact?	<u>Yes</u> No	Not Visible
Repairs Necessary:		
Casing Diameter:	<u>2"</u>	
Water Level Before Purge:	<u>22.07</u>	ft
Depth to Top of Pump:	<u>—</u>	ft
Water Level After Sample:	<u>24.58</u>	ft
Measurement Method:	Electric Water Level Indicator	

Sampling Information

Purging Method:	<u>Bladder</u>			
Sampling Method:	<u>Bladder</u>			
Dedicated Equip?:	<u>Yes</u> No <u>Yes</u>			
Duplicate Sample?:	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>			
Duplicate Sample ID:				
Purge Date:	<u>2 Oct 18</u>	Time Purging Began: <u>10:25</u> am/pm		
Well Purged Dry?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	Time Purged Dry: <u>—</u> am/pm		
Sample Date:	<u>2 Oct 18</u>	Time of Sampling: <u>11:05</u> am/pm		
Bottle List:	1L Raw	500mL Nitric	500mL Nitric (filtered)	250mL Sulfuric

Control Settings	
Purge:	<u>5</u> sec.
Recover:	<u>55</u> sec.
PSI:	<u>20</u>

Field Measurements

SEQ #	Stabilization (3 consecutive) Time	Temp (°C)	Spec. Cond. ±5%	pH ±0.1	DO (mg/L) ±10%	ORP (mV) ±20 mV	Turbidity (NTU) ±10%	Water Level (ft) 0.25 ft	Pumping Rate ml/min	mL Removed	Description: Clarity, Color, Odor, Ect. Clear, Slightly Turbid, Turbid
2	1050	9.41	3809	6.90	1.80	75.6	0.77	23.30	100.0	2000.0	Clear
3	1055	9.67	3774	6.93	1.89	82.0	0.48	23.74	100.0	500.0	Clear
4	1100	9.84	3717	6.92	1.87	89.0	0.43	23.85	100.0	500.0	Clear
5	1105	9.79	3704	6.91	1.91	90.0	0.44	23.97	100.0	500.0	Clear
6											
7											
8											
9											
10											

Stabilized: Yes No

Total Volume Removed: 4,000.0 mL

Comments:



Field Datasheet

Groundwater Assessment

2616 E. Broadway Ave, Bismarck, ND

Phone: (701) 258-9720

Company: MDU Heskett

Event: Fall 2018

Sample ID: 101

Sampling Personal: Jerry [Signature]

Weather Conditions: Temp: 55 °F Wind: S @ 5-10 Precip: Sunny / ~~Partly Cloudy~~ / Cloudy

Well Information

Well Locked?	Yes	No	
Well Labeled?	Yes	No	
Casing Straight?	Yes	No	
Grout Seal Intact?	Yes	No	Not Visible
Repairs Necessary:			
Casing Diameter:	2"		
Water Level Before Purge:	37.35		ft
Depth to Top of Pump:	_____ ft		
Water Level After Sample:	40.86		ft
Measurement Method:	Electric Water Level Indicator		

Sampling Information

Purging Method:	Bladder		Control Settings	
Sampling Method:	Bladder		Purge:	S sec.
Dedicated Equip?:	Yes	No	Recover:	55 sec.
Duplicate Sample?:	Yes	No	PSI:	30
Duplicate Sample ID:	_____			
Purge Date:	2 Oct 18	Time Purging Began:	1137	am/pm
Well Purged Dry?	Yes	No	Time Purged Dry:	_____ am/pm
Sample Date:	2 Oct 18	Time of Sampling:	1302	am/pm
Bottle List:	1L Raw	500mL Nitric	500mL Nitric (filtered)	250mL Sulfuric

Field Measurements

Stabilization (3 consecutive)	Temp (°C)	Spec. Cond. ±5%	pH ±0.1	DO (mg/L) ±10%	ORP (mV) ±20 mV	Turbidity (NTU) ±10%	Water Level (ft) 0.25 ft	Pumping Rate ml/min	mL Removed	Description: Clarity, Color, Odor, Ect. Clear, Slightly Turbid, Turbid
1	11.42	4719	6.72	4.41	90.9	69.9	38.20	100.0	500.0	clear
2	12.02	4689	6.68	2.51	22.7	27.2	39.18	100.0	2000.0	clear
3	12.22	4683	6.64	2.15	37.8	9.37	39.55	100.0	2000.0	clear
4	12.42	4688	6.64	2.23	38.2	5.79	39.84	100.0	2000.0	clear
5	12.52	4685	6.62	1.90	30.8	4.98	40.12	100.0	1000.0	clear
6	12.57	4702	6.62	1.97	27.2	4.86	40.28	100.0	500.0	clear
7	13.02	4695	6.62	1.94	24.9	4.77	40.32	100.0	500.0	clear
8										
9										
10										

Stabilized: Yes No

Total Volume Removed: 8500.0 mL

Comments:



Field Datasheet

Groundwater Assessment

2616 E. Broadway Ave, Bismarck, ND
Phone: (701) 258-9720

Company: MDU Heskett
Event: Fall 2018
Sample ID: 103
Sampling Personal: Jerry Ph...

Weather Conditions: Temp: 45 °F Wind: S @ 5-10 Precip: Sunny / Partly Cloudy / Cloudy

Well Information

Well Locked?	Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>	
Well Labeled?	<input checked="" type="checkbox"/> Yes No <input type="checkbox"/>	
Casing Straight?	<input checked="" type="checkbox"/> Yes No <input type="checkbox"/>	
Grout Seal Intact?	<input checked="" type="checkbox"/> Yes No <input type="checkbox"/>	Not Visible
Repairs Necessary:		
Casing Diameter:	<u>2"</u>	
Water Level Before Purge:	<u>32.64</u>	ft
Depth to Top of Pump:	<u> </u> ft	
Water Level After Sample:	<u>35.02</u>	ft
Measurement Method:	<u>Electric Water Level Indicator</u>	

Sampling Information

Purging Method:	<u>Bladder</u>		
Sampling Method:	<u>Bladder</u>		
Dedicated Equip?:	<input checked="" type="checkbox"/> Yes	No <input type="checkbox"/>	
Duplicate Sample?:	Yes <input type="checkbox"/>	No <input checked="" type="checkbox"/>	
Duplicate Sample ID:	<u> </u>		
Purge Date:	<u>1 Oct 18</u>	Time Purging Began:	<u>1240</u> am/pm
Well Purged Dry?	Yes <input checked="" type="checkbox"/>	Time Purged Dry:	<u> </u> am/pm
Sample Date:	<u>1 Oct 18</u>	Time of Sampling:	<u>1320</u> am/pm
Bottle List:	1L Raw	500mL Nitric	500mL Nitric (filtered) 250mL Sulfuric

Control Settings	
Purge:	<u>5</u> sec.
Recover:	<u>55</u> sec.
PSI:	

Field Measurements

Stabilization (3 consecutive)	Temp (°C)	Spec. Cond. ±5%	pH ±0.1	DO (mg/L) ±10%	ORP (mV) ±20 mV	Turbidity (NTU) ±10%	Water Level (ft) 0.25 ft	Pumping Rate ml/min	mL Removed	Description: Clarity, Color, Odor, Ect. Clear, Slightly Turbid, Turbid	
SEQ # 1	Time <u>1245</u>	<u>9.29</u>	<u>4980</u>	<u>6.73</u>	<u>1.56</u>	<u>303.0</u>	<u>0.78</u>	<u>33.46</u>	<u>100.0</u>	<u>500.0</u>	<u>clear</u>
2	<u>1305</u>	<u>9.26</u>	<u>5012</u>	<u>6.69</u>	<u>1.78</u>	<u>305.6</u>	<u>1.26</u>	<u>34.41</u>	<u>100.0</u>	<u>2000.0</u>	<u>clear</u>
3	<u>1310</u>	<u>9.20</u>	<u>5010</u>	<u>6.70</u>	<u>1.91</u>	<u>300.6</u>	<u>1.30</u>	<u>34.59</u>	<u>100.0</u>	<u>500.0</u>	<u>clear</u>
4	<u>1315</u>	<u>9.20</u>	<u>5001</u>	<u>6.68</u>	<u>1.86</u>	<u>297.7</u>	<u>1.27</u>	<u>34.63</u>	<u>100.0</u>	<u>500.0</u>	<u>clear</u>
5	<u>1320</u>	<u>9.17</u>	<u>4960</u>	<u>6.67</u>	<u>1.81</u>	<u>291.5</u>	<u>1.23</u>	<u>34.68</u>	<u>100.0</u>	<u>500.0</u>	<u>clear</u>
6											
7											
8											
9											
10											

Stabilized: Yes No
Comments:

Total Volume Removed: 4,000.0 mL



Field Datasheet

Groundwater Assessment

2616 E. Broadway Ave, Bismarck, ND
Phone: (701) 258-9720

Company: MDU Heskett
Event: Fall 2018
Sample ID: 44R
Sampling Personal: *[Signature]*

Weather Conditions: Temp: 45°F Wind: S @ 5-10 Precip: Sunny / Partly Cloudy / Cloudy

Well Information

Well Locked?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	
Well Labeled?	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	
Casing Straight?	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	
Grout Seal Intact?	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	Not Visible
Repairs Necessary:		
Casing Diameter:	2"	
Water Level Before Purge:	27.25	ft
Depth to Top of Pump:	<u> </u> ft	
Water Level After Sample:	27.37	ft
Measurement Method:	Electric Water Level Indicator	

Sampling Information

Purging Method:	Bladder			
Sampling Method:	Bladder			
Dedicated Equip?:	<input checked="" type="checkbox"/> Yes	<input type="checkbox"/> No		
Duplicate Sample?:	<input type="checkbox"/> Yes	<input checked="" type="checkbox"/> No		
Duplicate Sample ID:	<u> </u>			
Purge Date:	10/18	Time Purging Began:	1345	am/pm
Well Purged Dry?:	<input type="checkbox"/> Yes	<input checked="" type="checkbox"/> No	Time Purged Dry:	<u> </u> am/pm
Sample Date:	10/18	Time of Sampling:	1435	am/pm
Bottle List:	1L Raw	500mL Nitric	500mL Nitric (filtered)	250mL Sulfuric

Control Settings	
Purge:	S sec.
Recover:	SS sec.
PSI:	30

Field Measurements

SEQ #	Stabilization (3 consecutive) Time	Temp (°C)	Spec. Cond. ±5%	pH ±0.1	DO (mg/L) ±10%	ORP (mV) ±20 mV	Turbidity (NTU) ±10%	Water Level (ft) 0.25 ft	Pumping Rate ml/min	mL Removed	Description:
											Clarity, Color, Odor, Ect. Clear, Slightly Turbid, Turbid
1	1350	9.41	8952	6.58	2.69	314.3	5.42	27.41	100.0	500.0	Clear
2	1420	9.25	8940	6.54	1.12	308.3	3.10	27.34	100.0	3000.0	Clear
3	1425	9.21	8934	6.52	1.05	312.4	3.23	27.34	100.0	500.0	Clear
4	1430	9.21	8936	6.53	1.09	313.5	3.31	27.34	100.0	500.0	Clear
5	1435	9.21	8937	6.52	1.02	314.5	3.25	27.36	100.0	500.0	Clear
6											
7											
8											
9											
10											


Stabilized: Yes No
Comments:

Total Volume Removed: 5,000.0 mL

**Laboratories, Inc.**

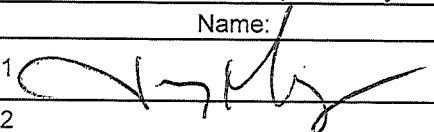
2616 E. Broadway
 Bismarck, ND 58501
 Phone (701) 258-9720

Chain of Custody Record

Project Name: MDU Heskett	Event: Fall 2018	Work Order Number: 82- 2588
Report To: MDU Attn: Samantha Marshall Address: 5181 Southgate Dr. Billings, MT 59102 phone: 406-896-4227 email:	Carbon Copy: Attn: Address:	Name of Sampler(s): 

Lab Number	Sample ID	Date	Time	Sample Type	Bottle Type				Field Parameters			Analysis Required
					1 liter	500mL Nitric	500mL Nitric (filtered)	250 mL Sulfuric	Temp (°C)	Spec. Cond.	pH	
W3236	13	10 Oct 18	0905	GW	X	X	X	X	8.90	9887	6.93	MDU List AA & MDU Appendix 3 List MDU Appendix 4 List minus Red Chem
W3237	Dup1	1 Oct 18	NA	GW	X	X	X	X	NA	NA	NA	
W3238	102	2 Oct 18	0930	GW	X	X	X	X	9.02	9098	6.77	
W3239	70	2 Oct 18	1105	GW	X	X	X	X	9.79	3704	6.91	
W3240	101	2 Oct 18	1302	GW	X	X	X	X	11.87	4695	6.62	
W3241	103	1 Oct 18	1320	GW	X	X	X	X	9.17	4960	6.67	
W3242	44R	1 Oct 18	1435	GW	X	X	X	X	9.21	8937	6.52	
W3243	FB1	2 Oct 18	NA	GW	X	X	X	X	NA	NA	NA	

Comments:

Relinquished By:		Sample Condition:	
Name:	Date/Time	Location:	Temp (°C)
	2 Oct 18 1406	Log In Walk In #2	4.0 psi TM562 / TM588
1			
2			

Received by:	
Name:	Date/Time
N Bachmann	2 Oct 18 1406



CASE NARRATIVE – AMENDED 29 JAN 19 (REPORTING)

MVTL Lab Reference No/SDG: 201882-2619
Client: Montana Dakota Utilities
Location: MDU Heskett
Project Identification: CCR Oct 2018
MVTL Laboratory Identifications: 18-W3261 through 18-W3267
Page 1 of 2

MDU Sample Identification	MVTL Laboratory #
33	18-W3261
3-90	No sample
Dup2	18-W3262
2-90	18-W3263
104	18-W3264
80R	18-W3265
105	18-W3266
FB2	18-W3267

I. RECEIPT

- All samples were received at the laboratory on 4 Oct 18 at 1307.
- Samples were collected and hand delivered by MVTL Field Service personnel to the laboratory.
- Samples were received on ice and evidence of cooling had begun.
 - Temperature of samples upon receipt was 3.1°C.
- All samples were properly preserved unless noted here and/or flagged on the individual analytical laboratory report.
- No other exceptions on sample receipt were encountered on this sample set unless noted here.

II. HOLDING TIMES

- With the exception of pH, all holding times were met for both preparation and analysis unless noted here.

III. METHODS

- Approved methodology was followed for all sample analyses.

IV. ANALYSIS

- All acceptance criteria was met for calibration, method blanks, laboratory control samples, laboratory fortified matrix/matrix duplicates unless noted here and/or flagged on the individual analytical laboratory report.
 - For some analytes, the reported results were elevated due to additional dilutions required to minimize the effects of sample matrix.



MINNESOTA VALLEY TESTING LABORATORIES, INC.

1126 North Front St. ~ New Ulm, MN 56073 ~ 800-782-3557 ~ Fax 507-359-2890
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CASE NARRATIVE – AMENDED 29 JAN 19 (REPORTING)

MVTL Lab Reference No/SDG: **201882-2619**
Client: **Montana Dakota Utilities**
Location: **MDU Heskett**
Project Identification: **CCR Oct 2018**
MVTL Laboratory Identifications: **18-W3261 through 18-W3267**
Page 2 of 2

- For some analytes, the reported results were elevated due to instrument performance at the lower limit of quantitation (LLOQ).

V. REPORTING

- Per email dated 21 Jan 19 from Terri Olson with Barr, the reports were amended to report only Appendix III parameters on one report and only Appendix IV parameters on a separate report.

All laboratory data has been approved by MVTL Laboratories.

SIGNED: Claudette Carroll DATE: 29 Jan 19
Claudette Carroll - MVTL Bismarck Laboratory Manager

Claudette Carroll

From: Terri A. Olson <TOlson@barr.com>
Sent: Monday, January 21, 2019 12:15 PM
To: Claudette Carroll
Cc: 'Marshall, Samantha'; Stephanie A. Theriault
Subject: Re: Reports revisions

Follow Up Flag: Follow up
Flag Status: Flagged

Hi Claudette,

We haven't emailed in a while, hope you're having a good new year.

For the two Heskett CCR reports (201882-2588 and 201882-2619), we will need the Appendix III and Appendix IV CCR analytes split into two reports. The field parameters (pH, temperature, conductivity) can be reported in only the Appendix III report or you can include in both.

- Appendix III – see 201882-0637 for example
 - Chloride
 - TDS
 - Fluoride
 - pH
 - Sulfate
 - Boron
 - Calcium
- Appendix IV
 - Antimony
 - Arsenic
 - Barium
 - Beryllium
 - Cadmium
 - Chromium
 - Cobalt
 - Lead
 - Lithium
 - Molybdenum
 - Selenium
 - Thallium
 - Mercury
 - Fluoride is in both lists so OK to have just in Appendix III since we wouldn't report Appendix IV only

We have discussed the report split with Sam at MDU and she was OK with it. I have copied her on this email. We need ASAP as our report is due at the end of this month.

Let me know if you have any questions.

Thank-you,

Terri A. Olson

Senior Data Quality Specialist
Minneapolis, MN office: 952.842.3578
TOlson@barr.com
www.barr.com



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MEMBER
ACIL

Page: 1 of 1

Quality Control Report – Amended 29 Jan 19

Lab IDs: 18-W3261 to 18-W3267

Project: MDU Heskett

Work Order: 201882-2619

Analyte	LCS Spike Amt	LCS Rec %	LCS % Rec Limits	Matrix Spike Amt	Matrix Spike ID	Matrix Spike Orig Result	Matrix Spike Result	Matrix Spike Rec %	Matrix Spike % Rec Limits	MSD/ Dup Orig Result	MSD/ Dup Result	MSD Rec %	MSD/ Dup RPD	MSD/ Dup RPD Limit (<)	Known Rec (%)	Known % Rec Limits	Method Blank
Boron - Total mg/l	0.40	108	80-120	2.00	18-W3264	0.96	2.82	93	75-125	2.82	2.93	98	3.8	20	-	-	< 0.1
	0.40	108	80-120												-	-	< 0.1
Calcium - Total mg/l	20.0	102	80-120	500	18W3252q	240	705	93	75-125	705	715	95	1.4	20	-	-	< 1
															-	-	< 1
Chloride mg/l	30.0	100	80-120	30.0	18-W3275	9.4	40.5	104	80-120	40.5	43.3	113	6.7	20	-	-	< 1
	30.0	100	80-120												-	-	< 1
Fluoride mg/l	0.50	98	90-110	0.500	18-W3274	< 0.1	0.58	116	80-120	0.58	0.58	116	0.0	20	-	-	< 0.1
	0.50	100	90-110	0.500	18-W3261	0.19	0.65	92	80-120	0.65	0.65	92	0.0	20	-	-	< 0.1
pH units	-	-	-	-	-	-	-	-	-	8.2	8.2	-	0.0	20	-	-	-
	-	-	-	-	-	-	-	-	-	7.8	7.9	-	1.3	20	-	-	-
	-	-	-	-	-	-	-	-	-	7.0	7.1	-	1.4	20	-	-	-
Sulfate mg/l	100	94	80-120	500	18-W3252	735	1250	103	80-120	1250	1210	95	3.3	20	-	-	< 5
	100	101	80-120	100	18-W3267	< 5	97.4	97	80-120	97.4	101	101	3.6	20	-	-	< 5
Total Dissolved Solids mg/l	-	-	-	-	-	-	-	-	-	< 10	< 10	-	0.0	*	-	-	< 10

* Data reported based on acceptance criteria of Absolute Difference of ± 3 mg/L.

Approved by: _____

C. Cant
29 Jan 19



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Page: 1 of 7

Amended 29 Jan 19 (App III/App IV) - CCR

Samantha Marshall
Montana Dakota Utilities
5181 Southgate Dr
Billings MT 59102

Report Date: 30 Oct 18
Lab Number: 18-W3261
Work Order #: 82-2619
Account #: 002800
Date Sampled: 3 Oct 18 11:55
Date Received: 4 Oct 18 13:07
Sampled By: MVTL Field Services

Project Name: MDU Heskett

PO #: 169846 OP

Sample Description: 33

Temp at Receipt: 3.1C ROI

Event and Year: Fall 2018

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
pH - Field	6.48	units	NA	SM 4500 H+ B	3 Oct 18 11:55	JSM
pH	* 6.9	units	0.1	SM4500 H+ B	4 Oct 18 17:00	SVS
Temperature - Field	9.02	Degrees C	NA	SM 2550B	3 Oct 18 11:55	JSM
Conductivity - Field	5136	umhos/cm	1	EPA 120.1	3 Oct 18 11:55	JSM
Fluoride	0.19	mg/l	0.10	SM4500-F-C	4 Oct 18 17:00	SVS
Sulfate	3740	mg/l	5.00	ASTM D516-07	10 Oct 18 12:43	EV
Chloride	11.7	mg/l	1.0	SM4500-Cl-E	17 Oct 18 14:07	EV
Total Dissolved Solids	5290	mg/l	10	I1750-85	5 Oct 18 8:20	SVS
Calcium - Total	438	mg/l	1.0	6010D	12 Oct 18 15:28	BMB
Boron - Total	< 0.5 @	mg/l	0.10	6010D	8 Oct 18 12:49	SZ

* Holding time exceeded

Approved by:

Claudette K. Carroll

CC
29 Jan 19

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

The reporting limit was elevated for any analyte requiring a dilution as coded below:

@ = Due to sample matrix # = Due to concentration of other analytes
! = Due to sample quantity + = Due to internal standard response

CERTIFICATION: ND # ND-00016



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Amended 29 Jan 19 (App III/App IV) - CCR

Samantha Marshall
Montana Dakota Utilities
5181 Southgate Dr
Billings MT 59102

Report Date: 30 Oct 18
Lab Number: 18-W3262
Work Order #: 82-2619
Account #: 002800
Date Sampled: 3 Oct 18
Date Received: 4 Oct 18 13:07
Sampled By: MVTL Field Services

Project Name: MDU Heskett

PO #: 169846 OP

Sample Description: Dup2

Temp at Receipt: 3.1C ROI

Event and Year: Fall 2018

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
pH	* 7.0	units	0.1	SM4500 H+ B	4 Oct 18 17:00	SVS
Fluoride	0.25	mg/l	0.10	SM4500-F-C	4 Oct 18 17:00	SVS
Sulfate	4460	mg/l	5.00	ASTM D516-07	10 Oct 18 12:43	EV
Chloride	374	mg/l	1.0	SM4500-Cl-E	17 Oct 18 14:07	EV
Total Dissolved Solids	7280	mg/l	10	I1750-85	5 Oct 18 8:20	SVS
Calcium - Total	355	mg/l	1.0	6010D	12 Oct 18 15:28	BMB
Boron - Total	< 0.5 @	mg/l	0.10	6010D	8 Oct 18 12:49	SZ

* Holding time exceeded

Approved by:

Claudette K. Carroll

CC
29 Jan 19

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

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CERTIFICATION: ND # ND-00016



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Amended 29 Jan 19 (App III/App IV) - CCR

Samantha Marshall
 Montana Dakota Utilities
 5181 Southgate Dr
 Billings MT 59102

Report Date: 30 Oct 18
 Lab Number: 18-W3263
 Work Order #: 82-2619
 Account #: 002800
 Date Sampled: 3 Oct 18 13:12
 Date Received: 4 Oct 18 13:07
 Sampled By: MVTL Field Services

Project Name: MDU Heskett

PO #: 169846 OP

Sample Description: 2-90

Temp at Receipt: 3.1C ROI

Event and Year: Fall 2018

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
pH - Field	6.87	units	NA	SM 4500 H+ B	3 Oct 18 13:12	JSM
pH	* 7.3	units	0.1	SM4500 H+ B	4 Oct 18 17:00	SVS
Temperature - Field	7.59	Degrees C	NA	SM 2550B	3 Oct 18 13:12	JSM
Conductivity - Field	7292	umhos/cm	1	EPA 120.1	3 Oct 18 13:12	JSM
Fluoride	1.00	mg/l	0.10	SM4500-F-C	4 Oct 18 17:00	SVS
Sulfate	5030	mg/l	5.00	ASTM D516-07	10 Oct 18 12:43	EV
Chloride	70.3	mg/l	1.0	SM4500-Cl-E	17 Oct 18 14:07	EV
Total Dissolved Solids	7970	mg/l	10	I1750-85	5 Oct 18 8:20	SVS
Calcium - Total	452	mg/l	1.0	6010D	12 Oct 18 15:28	BMB
Boron - Total	< 0.5 @	mg/l	0.10	6010D	8 Oct 18 12:49	SZ

* Holding time exceeded

Approved by:

Claudette K. Carroll ^{CC} 29 Jan 19

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

The reporting limit was elevated for any analyte requiring a dilution as coded below:
 @ = Due to sample matrix # = Due to concentration of other analytes
 ! = Due to sample quantity + = Due to internal standard response

CERTIFICATION: ND # ND-00016



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Page: 4 of 7

Amended 29 Jan 19 (App III/App IV) - CCR

Samantha Marshall
Montana Dakota Utilities
5181 Southgate Dr
Billings MT 59102

Report Date: 30 Oct 18
Lab Number: 18-W3264
Work Order #: 82-2619
Account #: 002800
Date Sampled: 4 Oct 18 10:35
Date Received: 4 Oct 18 13:07
Sampled By: MVTL Field Services

Project Name: MDU Heskett

PO #: 169846 OP

Sample Description: 104

Temp at Receipt: 3.1C

Event and Year: Fall 2018

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
pH - Field	6.85	units	NA	SM 4500 H+ B	4 Oct 18 10:35	JSM
pH	* 7.2	units	0.1	SM4500 H+ B	4 Oct 18 17:00	SVS
Temperature - Field	8.44	Degrees C	NA	SM 2550B	4 Oct 18 10:35	JSM
Conductivity - Field	13818	umhos/cm	1	EPA 120.1	4 Oct 18 10:35	JSM
Fluoride	0.51	mg/l	0.10	SM4500-F-C	4 Oct 18 17:00	SVS
Sulfate	11000	mg/l	5.00	ASTM D516-07	10 Oct 18 12:43	EV
Chloride	99.0	mg/l	1.0	SM4500-Cl-E	17 Oct 18 14:07	EV
Total Dissolved Solids	18000	mg/l	10	I1750-85	5 Oct 18 8:20	SVS
Calcium - Total	422	mg/l	1.0	6010D	12 Oct 18 15:28	BMB
Boron - Total	0.96	mg/l	0.10	6010D	8 Oct 18 12:49	SZ

* Holding time exceeded

Approved by:

Claudette K. Carroll

CC
29 Jan 19

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

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@ = Due to sample matrix # = Due to concentration of other analytes
! = Due to sample quantity + = Due to internal standard response

CERTIFICATION: ND # ND-00016



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Amended 29 Jan 19 (App III/App IV) - CCR

Samantha Marshall
Montana Dakota Utilities
5181 Southgate Dr
Billings MT 59102

Report Date: 30 Oct 18
Lab Number: 18-W3266
Work Order #: 82-2619
Account #: 002800
Date Sampled: 3 Oct 18 14:40
Date Received: 4 Oct 18 13:07
Sampled By: MVTL Field Services

Project Name: MDU Heskett

PO #: 169846 OP

Sample Description: 105

Temp at Receipt: 3.1C

Event and Year: Fall 2018

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
pH - Field	6.66	units	NA	SM 4500 H+ B	3 Oct 18 14:40	JSM
pH	* 7.1	units	0.1	SM4500 H+ B	4 Oct 18 17:00	SVS
Temperature - Field	8.51	Degrees C	NA	SM 2550B	3 Oct 18 14:40	JSM
Conductivity - Field	6662	umhos/cm	1	EPA 120.1	3 Oct 18 14:40	JSM
Fluoride	0.25	mg/l	0.10	SM4500-F-C	4 Oct 18 17:00	SVS
Sulfate	4340	mg/l	5.00	ASTM D516-07	10 Oct 18 14:28	EV
Chloride	384	mg/l	1.0	SM4500-Cl-E	17 Oct 18 14:07	EV
Total Dissolved Solids	7320	mg/l	10	I1750-85	5 Oct 18 8:20	SVS
Calcium - Total	350	mg/l	1.0	6010D	12 Oct 18 15:28	BMB
Boron - Total	< 0.5 @	mg/l	0.10	6010D	8 Oct 18 12:49	SZ

* Holding time exceeded

Approved by:

Claudette K. Carroll

29 Jan 19

Claudette K. Carroll, Laboratory Manager, Bismarck, ND

RL = Method Reporting Limit

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@ = Due to sample matrix # = Due to concentration of other analytes
! = Due to sample quantity + = Due to internal standard response

CERTIFICATION: ND # ND-00016



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October 26, 2018

Montana Dakota Utilities
Attn: Samantha Marshall
400 N. 4th St.
Bismarck, ND 58501

RE: Groundwater Sampling Event - MDU Heskett Ash Site

Dear Ms. Marshall:

From October 1-4, 2018, MVTL Laboratories' Field Services division collected groundwater samples at the MDU Heskett site near Mandan, ND for the Heskett CCR and NDDH analysis.

All wells were located and were found to be in generally good condition. All wells were purged and sampled using a dedicated bladder pump and BARR's SOP for low flow purging and sampling. Well 3-90 had an insufficient volume of water so no sample could be collected. Samples collected were, placed on ice and transported back to the MVTL laboratory in Bismarck, ND for analysis. The field data report for the sampling event accompanies this letter.

Thank you for your trust and support of our services. If you have any questions, please call me at (800) 279-6885.

Sincerely,

Jeremy Meyer
MVTL Field Services



MVT L Laboratories Inc.
FIELD DATA REPORT

MDU Heskett
GROUNDWATER SAMPLING

Attn: Samantha Marshall
400 N. 4th St
Bismarck, ND 58501
701-222-7829

WO# 82-2588
82-2619
82-2618

WELL ID	PURGE DATE	START PURGE TIME	SAMPLE DATE	TIME OF SAMPLE	WATER LEVEL START	WATER LEVEL END	VOLUME REMOVED (mL)	SAMPLE METHOD	TEMP (°C)	EC	pH	Turbidity NTU	SAMPLE APPEARANCE OR COMMENT
2-90	3-Oct-18	12:32	3-Oct-18	13:12	22.18	Below Pump	4000.0	Bladder	7.59	7292	6.87	0.56	clear
3-90	NA	NA	3-Oct-18	12:20	Below Pump	NA	NA	Bladder	NA	NA	NA	NA	Insufficient volume
13	1-Oct-18	8:15	1-Oct-18	9:05	30.74	32.76	5000.0	Bladder	8.90	9887	6.93	4.37	clear
33	3-Oct-18	10:45	3-Oct-18	11:55	42.37	43.38	7000.0	Bladder	9.02	5136	6.48	3.02	clear
70	2-Oct-18	10:25	2-Oct-18	11:05	22.07	24.58	4000.0	Bladder	9.79	3704	6.91	0.44	clear
80R	4-Oct-18	8:30	4-Oct-18	9:10	14.76	15.02	4000.0	Bladder	8.27	5610	6.98	0.81	clear
44R	1-Oct-18	13:45	1-Oct-18	14:35	27.25	27.37	5000.0	Bladder	9.21	8937	6.52	3.25	clear
101	2-Oct-18	11:37	2-Oct-18	13:02	37.35	40.86	8500.0	Bladder	11.87	4695	6.62	4.77	clear
102	2-Oct-18	8:50	2-Oct-18	9:30	18.80	20.08	4000.0	Bladder	9.02	9098	6.77	1.46	clear
103	1-Oct-18	12:40	1-Oct-18	13:20	32.64	35.02	4000.0	Bladder	9.17	4960	6.67	1.23	clear
104	4-Oct-18	9:55	4-Oct-18	10:35	14.34	14.63	4000.00	Bladder	8.44	13818	6.85	1.04	clear
105	4-Oct-18	13:40	4-Oct-18	14:40	13.10	13.38	6000.0	Bladder	8.51	6662	6.66	2.91	clear
1-90	4-Oct-18	11:10	4-Oct-18	11:50	12.01	12.15	4000.0	Bladder	9.71	9592	6.74	0.98	clear

NR = Not Recorded on Field Sheet NA = Not Applicable

MVTL Calibration Worksheet

Site: MDU Heskett

Technician: Jerry Gray

Instrument
(Circle One): #1 650 MDS 08E100203

#2 650 MDS 04H14736

#3 556 MPS 12E102056

Pre Site Calibration						
Date:	3 Oct 18		Time:	1020		
	pH	Temp °C	Pre Cal	Post Cal	Post Cal Range	mv Range +/- 50
Buffer 7		14.34	6.97	7.00	6.95-7.05	-22.0 0 +/- 50
Buffer 10		15.57	10.05	10.00	9.95-10.05	-200.8 -180 +/- 50
Buffer 4		15.71	4.06	4.00	4.95-5.05	152.1 180 +/- 50
Conductivity						Check
Buffer 1413		16.07	1386	1413	±10%	Buffer 5000 4951
ORP		11.78	244.0	244.0		
231 mV @ 25C		10.67	98.7%		±10 mV	
DO					Barometric Pressure (mm Hg)	
		10.67	98.7%	10.97	mg/L	750.06

Post Site Check		
Time:	1500	
	pH	Temp °C
Buffer 7		19.16
	Reading	7.03
Conductivity		
Buffer 5000	18.97	4947

Pre Site Calibration						
Date:	4 Oct 18		Time:	0825		
	pH	Temp °C	Pre Cal	Post Cal	Post Cal Range	mv Range +/- 50
Buffer 7		13.53	6.96	7.00	6.95-7.05	-21.2 0 +/- 50
Buffer 10		13.56	10.03	10.00	9.95-10.05	-199.4 -180 +/- 50
Buffer 4		13.73	4.06	4.00	4.95-5.05	151.6 180 +/- 50
Conductivity						Check
Buffer 1413		14.01	1412	1413	±10%	Buffer 5000 4967
ORP		18.93	247.1	244.0		
231 mV @ 25C					±10 mV	
DO					Barometric Pressure (mm Hg)	
		7.55	101.2%	12.12	mg/L	769.11

Post Site Check		
Time:	1200	
	pH	Temp °C
Buffer 7		
	Reading	
Conductivity		
Buffer 5000		



Field Datasheet

Groundwater Assessment

2616 E. Broadway Ave, Bismarck, ND

Phone: (701) 258-9720

Company: MDU Heskett
 Event: Fall 2018
 Sample ID: 33
 Sampling Personal: Jenny May

Weather Conditions: Temp: 45°F Wind: N @ 10-15 Precip: Sunny / Partly Cloudy / ~~Cloudy~~

Well Information

Well Locked?	Yes <input checked="" type="checkbox"/>	No <input type="checkbox"/>	
Well Labeled?	<input checked="" type="checkbox"/>	No <input type="checkbox"/>	
Casing Straight?	<input checked="" type="checkbox"/>	No <input type="checkbox"/>	
Grout Seal Intact?	Yes <input type="checkbox"/>	No <input type="checkbox"/>	<u>Not Visible</u>
Repairs Necessary:			
Casing Diameter:	<u>2"</u>		
Water Level Before Purge:	<u>42.37</u>	ft	
Depth to Top of Pump:	<u>—</u> ft		
Water Level After Sample:	<u>43.38</u>	ft	
Measurement Method:	<u>Electric Water Level Indicator</u>		

Sampling Information

Purging Method:	<u>Bladder</u>			
Sampling Method:	<u>Bladder</u>			
Dedicated Equip?:	<input checked="" type="checkbox"/>	No <input type="checkbox"/>		
Duplicate Sample?:	Yes <input type="checkbox"/>	No <input checked="" type="checkbox"/>		
Duplicate Sample ID:	<u>—</u>			
Purge Date:	<u>3 Oct 18</u>	Time Purging Began:	<u>1045</u>	<u>am/pm</u>
Well Purged Dry?	Yes <input type="checkbox"/>	No <input checked="" type="checkbox"/>	Time Purged Dry:	<u>—</u> am/pm
Sample Date:	<u>3 Oct 18</u>	Time of Sampling:	<u>1155</u>	<u>am/pm</u>
Bottle List:	1L Raw	500mL Nitric	500mL Nitric (filtered)	250mL Sulfuric

Control Settings		
Purge:	<u>5</u>	sec.
Recover:	<u>55</u>	sec.
PSI:	<u>30</u>	

Field Measurements

Stabilization (3 consecutive)		Temp (°C)	Spec. Cond. ±5%	pH ±0.1	DO (mg/L) ±10%	ORP (mV) ±20 mV	Turbidity (NTU) ±10%	Water Level (ft) 0.25 ft	Pumping Rate ml/min	mL Removed	Description: Clarity, Color, Odor, Ect. Clear, Slightly Turbid, Turbid
SEQ #	Time										
1	<u>1050</u>	<u>8.62</u>	<u>5295</u>	<u>6.54</u>	<u>3.50</u>	<u>0.9</u>	<u>72.5</u>	<u>43.06</u>	<u>100.0</u>	<u>500.0</u>	<u>Clear</u>
2	<u>1120</u>	<u>8.70</u>	<u>5190</u>	<u>6.51</u>	<u>2.58</u>	<u>16.5</u>	<u>7.05</u>	<u>43.10</u>	<u>100.0</u>	<u>3000.0</u>	<u>Clear</u>
3	<u>1140</u>	<u>8.80</u>	<u>5136</u>	<u>6.51</u>	<u>2.17</u>	<u>15.8</u>	<u>3.07</u>	<u>43.34</u>	<u>100.0</u>	<u>2000.0</u>	<u>Clear</u>
4	<u>1145</u>	<u>8.72</u>	<u>5131</u>	<u>6.48</u>	<u>1.05</u>	<u>20.3</u>	<u>3.09</u>	<u>43.25</u>	<u>100.0</u>	<u>500.0</u>	<u>Clear</u>
5	<u>1150</u>	<u>8.99</u>	<u>5122</u>	<u>6.48</u>	<u>1.09</u>	<u>20.2</u>	<u>3.15</u>	<u>43.20</u>	<u>100.0</u>	<u>500.0</u>	<u>Clear</u>
6	<u>1155</u>	<u>9.02</u>	<u>5136</u>	<u>6.48</u>	<u>1.14</u>	<u>18.4</u>	<u>3.02</u>	<u>43.29</u>	<u>100.0</u>	<u>500.0</u>	<u>Clear</u>
7											
8											
9											
10											

Stabilized: Yes No

Total Volume Removed: 7,000.0 mL

Comments:



Field Datasheet

Groundwater Assessment

2616 E. Broadway Ave, Bismarck, ND

Phone: (701) 258-9720

Company: MDU Heskett
 Event: Fall 2018
 Sample ID: 290
 Sampling Personal: Jerry [Signature]

Weather Conditions: Temp: 45 °F Wind: N @ 10-15 Precip: Sunny / Partly Cloudy / Cloudy

Well Information

Well Locked?	Yes	<u>No</u>	
Well Labeled?	<u>Yes</u>	No	
Casing Straight?	<u>Yes</u>	No	
Grout Seal Intact?	Yes	No	<u>Not Visible</u>
Repairs Necessary:			
Casing Diameter:	2"		
Water Level Before Purge:	22.18		ft
Depth to Top of Pump:	22.41		ft
Water Level After Sample:	Below Pump		ft
Measurement Method:	Electric Water Level Indicator		

Sampling Information

Purging Method:	Bladder		
Sampling Method:	Bladder		
Dedicated Equip?:	<u>Yes</u>	No	
Duplicate Sample?:	Yes	<u>No</u>	
Duplicate Sample ID:	-		
Control Settings		Purge:	5 sec.
		Recover:	55 sec.
		PSI:	10
Purge Date:	3 Oct 18	Time Purging Began:	1232 am/pm
Well Purged Dry?	Yes <u>No</u>	Time Purged Dry:	- am/pm
Sample Date:	3 Oct 18	Time of Sampling:	1312 am/pm
Bottle List:	1L Raw	500mL Nitric	500mL Nitric (filtered) 250mL Sulfuric

Field Measurements

Stabilization (3 consecutive)	Temp (°C)	Spec. Cond. ±5%	pH ±0.1	DO (mg/L) ±10%	ORP (mV) ±20 mV	Turbidity (NTU) ±10%	Water Level (ft) 0.25 ft	Pumping Rate ml/min	mL Removed	Description: Clarity, Color, Odor, Ect. Clear, Slightly Turbid, Turbid	
1	1237	7.84	7315	6.93	6.24	143.3	3.14	Below Pump	100.0	500.0	Clear
2	1242	7.81	7302	6.90	5.65	152.4	4.57	Below Pump	100.0	500.0	Clear
3	1247	7.83	7302	6.88	5.47	160.0	2.24	BP	100.0	500.0	Clear
4	1252	7.55	7295	6.88	4.49	167.2	1.47	BP	100.0	500.0	Clear
5	1257	7.72	7297	6.87	4.34	175.2	0.78	BP	100.0	500.0	Clear
6	1302	7.62	7291	6.87	3.99	182.5	0.60	BP	100.0	500.0	Clear
7	1307	7.72	7296	6.87	4.10	188.6	0.56	BP	100.0	500.0	Clear
8	1312	7.59	7292	6.87	4.04	194.9	0.56	BP	100.0	500.0	Clear
9											
10											

Stabilized: Yes No
 Comments:

Total Volume Removed: 4000.0 mL
 BP = Below Pump



Field Datasheet

Groundwater Assessment

2616 E. Broadway Ave, Bismarck, ND

Phone: (701) 258-9720

Company: MDU Heskett
 Event: Fall 2018
 Sample ID: 104
 Sampling Personal: Jerry [Signature]

Weather Conditions: Temp: 30F Wind: S @ 5-10 Precip: Sunny / Partly Cloudy / Cloudy

Well Information

Well Locked?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	
Well Labeled?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	
Casing Straight?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	
Grout Seal Intact?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	Not Visible
Repairs Necessary:		
Casing Diameter:	2"	
Water Level Before Purge:	14.34	ft
Depth to Top of Pump:	— ft	
Water Level After Sample:	14.63	ft
Measurement Method:	Electric Water Level Indicator	

Sampling Information

Purging Method:	Bladder		
Sampling Method:	Bladder		
Dedicated Equip?:	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>		
Duplicate Sample?:	Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>		
Duplicate Sample ID:	—		
Purge Date:	4 Oct 18	Time Purging Began:	0955 am/pm
Well Purged Dry?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	Time Purged Dry:	— am/pm
Sample Date:	4 Oct 18	Time of Sampling:	1035 am/pm
Bottle List:	1L Raw	500mL Nitric	500mL Nitric (filtered) 250mL Sulfuric

Control Settings	
Purge:	5 sec.
Recover:	55 sec.
PSI:	20

Field Measurements

Stabilization (3 consecutive)	Temp (°C)	Spec. Cond. ±5%	pH ±0.1	DO (mg/L) ±10%	ORP (mV) ±20 mV	Turbidity (NTU) ±10%	Water Level (ft) 0.25 ft	Pumping Rate ml/min	mL Removed	Description: Clarity, Color, Odor, Ect. Clear, Slightly Turbid, Turbid
SEQ #	Time									
1	1000	8.73	13861	6.93	3.18	274.8	14.58	100.0	500.0	Clear
2	1020	8.72	13771	6.86	1.66	278.7	14.66	100.0	2000.0	Clear
3	1025	8.47	13827	6.87	1.75	277.9	14.65	100.0	500.0	Clear
4	1030	8.82	13778	6.86	1.69	278.9	14.72	100.0	500.0	Clear
5	1035	8.44	13818	6.85	1.67	279.8	14.67	100.0	500.0	Clear
6										
7										
8										
9										
10										

Stabilized: Yes No
 Comments:

Total Volume Removed: 4,000.0 mL



Field Datasheet

Groundwater Assessment

2616 E. Broadway Ave, Bismarck, ND
Phone: (701) 258-9720

Company: MDU Heskett
Event: Fall 2018
Sample ID: 80R
Sampling Personal: Jerry Kly

Weather Conditions: Temp: 25°F Wind: S @ 5-10 Precip: Sunny / Partly Cloudy / Cloudy

Well Information

Well Locked?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	
Well Labeled?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	
Casing Straight?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	
Grout Seal Intact?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	Not Visible
Repairs Necessary:		
Casing Diameter:	2"	
Water Level Before Purge:	14.76 ft	
Depth to Top of Pump:	— ft	
Water Level After Sample:	15.02 ft	
Measurement Method:	Electric Water Level Indicator	

Sampling Information

Purging Method:	Bladder		
Sampling Method:	Bladder		
Dedicated Equip?:	Yes <input checked="" type="checkbox"/>	No <input type="checkbox"/>	
Duplicate Sample?:	Yes <input type="checkbox"/>	No <input checked="" type="checkbox"/>	
Duplicate Sample ID:	—		
Purge Date:	4 Oct 18	Time Purging Began:	0830 am/pm
Well Purged Dry?:	Yes <input checked="" type="checkbox"/>	Time Purged Dry:	— am/pm
Sample Date:	4 Oct 18	Time of Sampling:	0910 am/pm
Bottle List:	1L Raw	500mL Nitric	500mL Nitric (filtered) 250mL Sulfuric

Control Settings		
Purge:	5	sec.
Recover:	55	sec.
PSI:	20	

Field Measurements

Stabilization (3 consecutive)		Temp (°C)	Spec. Cond. ±5%	pH ±0.1	DO (mg/L) ±10%	ORP (mV) ±20 mV	Turbidity (NTU) ±10%	Water Level (ft) 0.25 ft	Pumping Rate ml/min	mL Removed	Description: Clarity, Color, Odor, Ect. Clear, Slightly Turbid, Turbid
SEQ #	Time										
1	0835	7.42	5531	6.92	4.39	226.9	3.16	15.04	100.0	500.0	Clear
2	0855	7.87	5610	6.96	2.29	222.3	0.78	15.00	100.0	2000.0	Clear
3	0900	8.26	5608	6.99	2.13	221.8	0.78	15.00	100.0	500.0	Clear
4	0905	7.72	5618	6.99	2.26	223.4	0.67	15.03	100.0	500.0	Clear
5	0910	8.27	5610	6.98	2.29	224.6	0.81	15.02	100.0	500.0	Clear
6											
7											
8											
9											
10											

Stabilized: Yes No

Total Volume Removed: 4,000.0 mL

Comments:



Field Datasheet

Groundwater Assessment

2616 E. Broadway Ave, Bismarck, ND
Phone: (701) 258-9720

Company: MDU Heskett
Event: Fall 2018
Sample ID: 105
Sampling Personal: Jerry Chy

Weather Conditions: Temp: 45°F Wind: N @ 15-20 Precip: Sunny / Partly Cloudy (Cloudy)

Well Information

Well Locked?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	
Well Labeled?	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	
Casing Straight?	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	
Grout Seal Intact?	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	Not Visible
Repairs Necessary:		
Casing Diameter:	2"	
Water Level Before Purge:	13.10	ft
Depth to Top of Pump:		
Water Level After Sample:	13.38	ft
Measurement Method:	Electric Water Level Indicator	

Sampling Information

Purging Method:	Bladder		
Sampling Method:	Bladder		
Dedicated Equip?:	<input checked="" type="checkbox"/> Yes	<input type="checkbox"/> No	
Duplicate Sample?:	<input checked="" type="checkbox"/> Yes	<input type="checkbox"/> No	
Duplicate Sample ID:	Dup 2		
Control Settings			
Purge:	5	sec.	
Recover:	55	sec.	
PSI:	20		
Purge Date:	3 Oct 18	Time Purging Began:	1340 am/pm
Well Purged Dry?	Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>	Time Purged Dry:	— am/pm
Sample Date:	3 Oct 18	Time of Sampling:	1440 am/pm
Bottle List:	1L Raw	500mL Nitric	500mL Nitric (filtered) 250mL Sulfuric

Field Measurements

SEQ #	Time	Stabilization (3 consecutive)	Temp (°C)	Spec. Cond. ±5%	pH ±0.1	DO (mg/L) ±10%	ORP (mV) ±20 mV	Turbidity (NTU) ±10%	Water Level (ft) 0.25 ft	Pumping Rate ml/min	mL Removed	Description:
												Clarity, Color, Odor, Ect. Clear, Slightly Turbid, Turbid
1	1345		8.32	5773	6.76	2.28	238.3	2.29	13.48	100.0	500.0	Clear
2	1405		8.13	5482	6.75	1.59	212.3	2.56	13.37	100.0	2000.0	Clear
3	1410		7.98	5789	6.71	1.88	213.9	1.98	13.48	100.0	500.0	Clear
4	1415		8.20	6116	6.69	1.60	212.7	2.43	13.42	100.0	500.0	Clear
5	1420		7.98	6204	6.69	1.55	212.3	2.56	13.44	100.0	500.0	Clear
6	1425		8.35	6395	6.68	1.52	212.0	3.01	13.52	100.0	500.0	Clear
7	1430		8.36	6483	6.67	1.38	211.3	2.82	13.48	100.0	500.0	Clear
8	1435		8.61	6633	6.68	1.30	210.0	3.00	13.45	100.0	500.0	Clear
9	1440		8.51	6662	6.66	1.34	210.1	2.91	13.47	100.0	500.0	Clear
10												

Stabilized: Yes No
Comments:

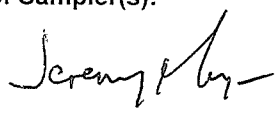
Total Volume Removed: 6,000.0 mL



Laboratories, Inc.

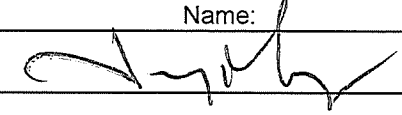
2616 E. Broadway
Bismarck, ND 58501
Phone (701) 258-9720

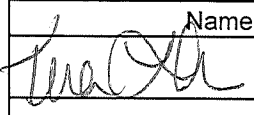
Chain of Custody Record

Project Name: MDU Heskett	Event: Fall 2018	Work Order Number: 82-2619
Report To: MDU Attn: Samantha Marshall Address: 5181 Southgate Dr. Billings, MT 59102 phone: 406-896-4227 email:	Carbon Copy: Attn: Address:	Name of Sampler(s): 

Lab Number	Sample ID	Date	Time	Sample Type	Bottle Type				Field Parameters			Analysis Required
					1 liter	500mL Nitric	500mL Nitric (filtered)	250 mL Sulfuric	Temp (°C)	Spec. Cond.	pH	
W3261	33	30 Oct 18	1155	GW	X	X	X	X	9.02	5136	6.48	MDU List AA & MDU Appendix 3 List MDU App 4 List Minus Pod chem
—	3-90	30 Oct 18	1220	GW	*X	X	X	X	insuff	cont volume		
W3262	Dup2	30 Oct 18	NA	GW	X	X	X	X	NA	NA	NA	
W3263	2-90	30 Oct 18	1312	GW	X	X	X	X	7.59	7292	6.87	
W3264	104	40 Oct 18	1035	GW	X	X	X	X	8.44	13818	6.85	
W3265	80R	40 Oct 18	0910	GW	X	X	X	X	8.27	5610	6.98	
W3266	105	30 Oct 18	1440	GW	X	X	X	X	8.51	6662	6.66	
W3267	FB2	40 Oct 18	NA	GW	X	X	X	X	NA	NA	NA	

Comments: * 1 - 40 Oct 18

Relinquished By:		Sample Condition:	
Name:	Date/Time	Location:	Temp (°C)
	40 Oct 18 1307	Log In Walk In #2	3.1 PC1 TM502 / TM588 40 Oct 18
1			
2			

Received by:	
Name:	Date/Time
	40 Oct 2018 1307

Appendix B

Alternative Source Demonstration Reports

Alternative Source Demonstration: October 2017 Event

R.M. Heskett Station

Prepared for
Montana-Dakota Utilities Co.

April 2018



Alternative Source Demonstration: October 2017 Event

R.M. Heskett Station

Prepared for
Montana-Dakota Utilities Co.

April 2018

Alternative Source Demonstration:
October 2017 Event

April 2018

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Appendix A	YSI Sensor Specifications
Appendix B	SPLP Laboratory Data
Appendix C	Aerial Photograph (1988)
Appendix D	1989 Special Use Disposal Site Permit Application
Appendix E	2014-2016 Boring Logs

Certifications

I hereby certify that I, or my agent, have examined this written demonstration and attest that this Coal Combustion Residuals Facility Alternative Source Demonstration (ASD) is accurate and has been prepared in accordance with good engineering practice, including consideration of applicable industry standards and the requirements of 40 CFR §257.94. I further certify that this report was prepared by me or under my direct supervision and that I am a duly Licensed Professional Engineer under the laws of the state of North Dakota.

Revision	Date	Summary of Revisions
0	April 13, 2018	Initial Alternative Source Demonstration



Thomas J. Radue, P.E.
Barr Engineering Co.
ND Registration Number PE – 3632

1.0 Introduction

Montana-Dakota Utilities Co. (MDU) owns and operates R.M. Heskett Station (Site), a coal-fired generating station and a gas fired turbine located in Mandan, North Dakota (Figure 1). One CCR (coal combustion residual) unit, as defined by 40 CFR 257.53, is located on the property. Wastes contained in the CCR unit primarily consist of coal combustion by-products, asbestos wastes generated from construction activity associated with MDU-owned facilities, and ash derived from burning of tire-derived fuel (TDF) at the facility.

The CCR Rule (US EPA, 2015) §257.94(e)(2) allows for an alternative source demonstration (ASD) in the event of an identified statistically significant increase (SSI) in a downgradient monitoring well over background levels:

The owner or operator may demonstrate that a source other than the CCR unit caused the statistically significant increase over background levels for a constituent or that the statistically significant increase resulted from error in sampling, analysis, statistical evaluation, or natural variation in groundwater quality. The owner or operator must complete the written demonstration within 90 days of detecting a statistically significant increase over background levels to include obtaining a certification from a qualified professional engineer verifying the accuracy of the information in the report.

The purpose of this work is to evaluate the data collected as part of the October 2017 monitoring event, along with historical data, to demonstrate if the identified SSIs are the results of a source other than the CCR unit or due to an error in sampling, analysis, or statistical evaluation, natural variation in groundwater quality.

2.0 October 2017 SSIs

Sampling for the first detection monitoring event was conducted on October 4 and 5, 2017. Four potential SSIs over background were identified: pH at MW-80R, chloride at MW-105, and sulfate and total dissolved solids (TDS) at MW-104 (additional details provided in Table 1). These potential SSIs were verified by additional samples collected on January 22, 2018.

Several characteristics of the CCR unit site geology, groundwater monitoring well locations, and historic groundwater quality data prompted consideration of potential alternative sources for the SSIs, including:

- Elevated water quality parameters in pre-landfill groundwater monitoring data;
- Proximity to nearby roadway surface water runoff ditches; and
- Site-specific geologic conditions.

Several methods of evaluation were subsequently undertaken in an effort to review potential alternative sources for the SSIs. These include the following evaluations:

- Charge balance error calculation;
- Evaluation of statistical methods;
- Comparison with leaching tests of ash materials;
- Comparison with historical (pre-landfill) groundwater data; and
- Analysis of potential spatial trends.

Successful alternative source demonstration is discussed in Section 3.0.

3.0 Alternative Source Demonstration

Methods used to evaluate potential alternative sources for all SSIs (pH at MW-80R, chloride at MW-105; and sulfate and TDS at MW-104) over background were successful for the October 2017 detection monitoring event as discussed in the following sections.

3.1 pH at MW-80R

Quality and accuracy of field sampling and analysis procedures were reviewed as a potential alternative source of elevated pH in groundwater at MW-80R.

3.1.1 Instrument Accuracy

Initially pH was identified as an SSI in MW-80R (7.10 standard units or SU) due to an exceedance of the upper control limit by the cumulative sum. Upon further review of the pH data, it was determined that the values recorded in the field were reported beyond the level of accuracy of the instrument. Accuracy of the field pH meter, as provided by the manufacturer (YSI; Appendix A), is ± 0.2 SU. However, pH was reported in the field down to the hundredth (0.01), over an order of magnitude lower than the level of accuracy achievable by the instrument. If the pH values collected at the Site were rounded to the nearest tenth (0.1), more consistent with the instrument's accuracy, no SSIs were observed (Figure 2). Therefore, based on an error in reporting, a successful demonstration of an alternative source exists for this SSI. It is recommended that pH values are reported to the nearest tenth, consistent with the instrument's level of accuracy, for future monitoring events.

3.2 Chloride at MW-105

Comparisons of CCR ash Synthetic Precipitation Leaching Procedure (SPLP method; EPA Method 1312) results as well as historical (pre-landfill) data were conducted to evaluate potential alternative sources of elevated chloride in groundwater at MW-105.

3.2.1 Comparison with Ash Data

Ash samples collected in 2011 (Appendix B) from various locations across the Site were analyzed using the SPLP method to assess ash as a potential source of water quality changes in downgradient wells. The SPLP method consists of mixing the ash with mildly acidic water in the laboratory to simulate the effect of atmospheric water (i.e., precipitation) infiltrating through the CCR unit and generating leachate.

The hypothesis that we tested is that if the leachate (represented by the SPLP results) was affecting downgradient groundwater quality near MW-105, then both the groundwater and SPLP results should appear to be geochemically similar. If the comparison of the two types of water samples indicate that they are geochemically dissimilar, this indicates that a source "other than the CCR unit" is responsible for the SSI and the alternative source demonstration is successful. The SPLP results along with the October 2017 chloride concentrations for MW-105 are shown on Table 2.

3.2.1.1 Chloride Concentrations

The October 2017 chloride concentration in MW-105 was measured at 346 milligrams per liter (mg/L), which is several times higher than the SPLP results, which ranged from 2 mg/L to 66 mg/L. At the same time, the other major cation and anion concentrations, such as sodium, calcium, potassium, sulfate, and TDS, are lower at MW-105 than in the SPLP results. If there were a release from the CCR unit, the relative concentrations of the major ions in MW-105 should be similar to the proportions of these same ions observed in the SPLP results from the CCR unit. Due to differences in residence times and source waters, actual concentrations differ between groundwater and experimental leachates, but these concentrations should be present in similar proportions if leaching of the ash is a major source of chloride to MW-105. The dissimilar proportion of major ions in MW-105 to the SPLP results support the conclusion that the SSI from MW-105 is due to a “source other than the CCR unit.”

3.2.1.2 Major Ion Comparisons

In order to test the hypothesis that the water quality at MW-105 is different from that expected from the CCR unit, Piper and Stiff diagrams were used to visually compare the SPLP results and the measured groundwater quality at the Site (Figures 3 and 4, respectively). Piper diagrams are plots of major ion chemistry of water samples (calcium, magnesium, potassium, sodium, chloride, sulfate, and alkalinity) that are used to differentiate between water types and to identify potential mixing of water types. Stiff diagrams represent major ion water chemistry as geometric shapes whose vertices are proportional to the geochemical composition of the water. Both of these methods allow a means to identify or “fingerprint” each water sample by their common characteristics to assess which types of water are similar or dissimilar to potential CCR sources or non-source water types (Hensel and Hirsch, 2002).

In the Piper diagram (Figure 3), the downgradient water quality (and of particular interest, at MW-105) is characterized as a Ca/Mg-SO₄ type water, whereas the ash SPLP results are Na-SO₄ type water. The major difference observed between the downgradient water quality (MW-105) and the SPLP results is the dominant cation concentration (calcium and magnesium vs. sodium). Because MW-105 is clustered with the upgradient wells rather than near the SPLP results, it indicates that the water chemistry at MW-105 is more similar to upgradient groundwater than a potential release from the CCR unit.

The Stiff diagrams (Figure 4) also support the hypothesis that the SSI at MW-105 is a “source other than the CCR unit” because of the difference in water chemistry between the SPLP results and MW-105. For example, a major ion in MW-105 is chloride which is generally minor in the SPLP leachate. This finding is consistent with the conclusion of Section 3.2.1.1 above. In addition, the SPLP results are relatively higher in potassium and sulfate, while MW-105 is generally lower with respect to these ions. Due to the high sulfate concentration at each location, relative to the other ions, a modified scale was used for sulfate (10% scale) on Figure 4 for ease of comparison.

While there is some variation among the SPLP sample results that appears related to the type of ash, the variants (e.g., bottom ash) that mostly resemble the major ions from MW-105 are proportionately lower than in MW-105 indicating that the bottom ash variant would be unlikely to cause a significant change in water quality at MW-105. This is because the source ash must be a higher concentration than those found

in downgradient groundwater in order for there to be evidence of a release. These additional lines of evidence also support the conclusion that the SSI from MW-105 is due to a “source other than the CCR unit.”

3.2.2 Comparison to Upgradient Water Quality

The results shown on Figures 3 and 4 indicate that the result at MW-105 appears most similar to the results from the upgradient wells. Samples from these upgradient wells are generally lower in sulfate and potassium while being higher in chloride than the SPLP results suggest are present in the CCR unit.

Therefore, these results suggest that the SSI at MW-105 is due to a “source other than the CCR unit” and may be the result of upgradient conditions.

3.2.3 Comparisons with Historical Data

Groundwater samples collected in 1986 (prior to construction of the CCR unit; an aerial photograph from March 30, 1988 shows the area of the CCR unit, which appears to be undisturbed (Appendix C)) were included in the 1989 Special Use Disposal Site Permit Application (Permit Application, MDU, 1989; Appendix D). Chloride concentrations in these groundwater samples were measured as high as 558 mg/L (Well 44, 11/21/1986), indicating that high chloride concentrations at the Site pre-date construction of the CCR unit. The historical (pre-landfill) chloride concentrations are also reported in the Permit Application included in Appendix D.

Due to the similarly high concentrations of chloride in groundwater prior to the construction of the CCR unit and the lack of similarity with the ash SPLP data, the SSI for chloride at MW-105 is due to a source other than the CCR unit.

3.3 Sulfate and TDS at MW-104

Review of regional geologic information and comparisons to historical (pre-landfill) field and laboratory data were conducted to evaluate a potential alternate source of elevated sulfate and TDS at MW-104.

As previously noted, TDS is a measurement of all parameters dissolved in a water sample. In samples where a particular ion comprises a significant weight percentage of dissolved solids, the concentration of that ion and TDS are often correlated. Data for MW-104 supports this correlation, where sulfate accounts for a large proportion of TDS, and thus the SSIs for these two parameters are likely related.

3.3.1 Comparisons with Historical Data

The groundwater quality data from MW-104 was compared to data collected from historical wells sampled in 1986, prior to construction of the CCR unit (Appendix D).

Analyses of groundwater samples collected prior to construction of the CCR unit included in the Permit Application notes that high TDS was observed at the Site (Appendix D). Maximum TDS and sulfate concentrations reported in 1986 were 14,917mg/L and 11,632 mg/L, respectively, in Well 60 (approximately 700 feet southwest of MW-104), with similar concentrations observed two years later

(Table 3). Sulfate and TDS concentrations reported in October 2017 were 10,200 mg/L and 15,400 mg/L, respectively, in MW-104 which are similar to historic concentrations at Well 60. Figure 5 and 6 show the range of sulfate and TDS concentrations, respectively, across the Site, including recent and historical monitoring well data.

3.3.2 Geologic and Hydrogeologic Variability

The Tertiary (Paleocene) Cannonball Formation underlies the Site and a large portion of eastern Morton County. Based on lithologies and bivalve assemblages, the depositional environment of the Cannonball Formation is a barrier island complex that included lagoonal, beach, and offshore environments (Lindholm, 1983). Lithologic and geophysical logs for the Site indicate that the uppermost 100 feet of the subsurface materials lie within the Cannonball Formation (MDU, 1989).

The dominant lithology observed at the Site is unconsolidated silt in a clay matrix with interspersed fine to medium-grained sand (10% to 30%). Thin sand lenses with limited extent have also been observed. Small gypsum crystals are documented discontinuously throughout the upper 30 feet of the surface materials, which have been presumed to be the result of diagenetic processes which occur above the water table during alternating wetting and drying cycles (Groenewold et al, 1983).

Gypsum is a hydrated calcium sulfate mineral that can be a source of high sulfate concentrations in groundwater. Dissolution of gypsum will occur until equilibrium concentrations are attained in the groundwater or until all the minerals are consumed. The Permit Application noted that “small gypsum crystals occur throughout the upper 30 feet of the site. These gypsum crystals are presumed to be the result of diagenetic processes which occur above the water table during alternate wetting and drying cycles” (MDU, 1989; Appendix D).

The boring log for MW-104 (Appendix E) notes gypsum present throughout the upper layer of the screened interval. Boring logs for other CCR wells and pre-landfill wells note gypsum occurrences across the Site (Appendix D (Exhibit 5-E) and Appendix E). The water level and screened interval in MW-104 are within the gypsum-bearing unit. In some other wells with lower sulfate and TDS concentrations, the water levels and/or screened units are below the documented gypsum occurrences.

Based on presence of gypsum in native subsurface deposits, we conclude that a “source other than the CCR unit” is the cause of elevated TDS and sulfate at MW-104, therefore, a successful demonstration of an alternative source exists for SSIs of sulfate and TDS at MW-104.

4.0 Conclusions

Four SSIs were identified from the October 2017 detection monitoring event. This report demonstrates that a “source other than the CCR unit” caused the SSIs, that the SSIs resulted from analytical error, or natural variation in groundwater quality, as allowed by §257.94(e)(2). The results of this alternative source demonstration are summarized in the table below.

Summary of SSIs and Alternative Sources

Well	Parameter	Report Section	Evidence for Alternative Source
MW-80R	pH	3.1	Analytical error (instrument accuracy)
MW-105	Chloride	3.2	Source other than CCR unit (water quality not consistent with samples from CCR unit, spatial trend inconsistent with hydraulic gradient), natural variability (pre-landfill values higher than current groundwater concentrations)
MW-104	Sulfate	3.3	Natural variability (pre-landfill values and geologic background)
MW-104	Total Dissolved Solids	3.3	Natural variability (pre-landfill values and geologic background)

On the basis of the alternative source demonstration presented herein and per the requirements of CCR Rule §257.94(e)(2), detection monitoring will continue for the CCR unit. Further, this alternative source demonstration will be included with the next annual groundwater monitoring and corrective action report required by CCR Rule §257.90(e).

5.0 References

Groenewold, G.H., Koob, G.J., McCarthy, B.W., and Peterson, W.M., 1983, Geologic and Geochemical Controls on the Chemical Evolution of Subsurface Water in Undisturbed and Surface-Mined Landscapes on Western North Dakota, North Dakota Geological Survey Report of Investigation 79, 151 p.

Hensel, D.R. and R. M. Hirsch, 2002. Statistical Methods in Water Resources Techniques of Water Resources Investigations, Book 4, chapter A3. U.S. Geological Survey. 522 pages.

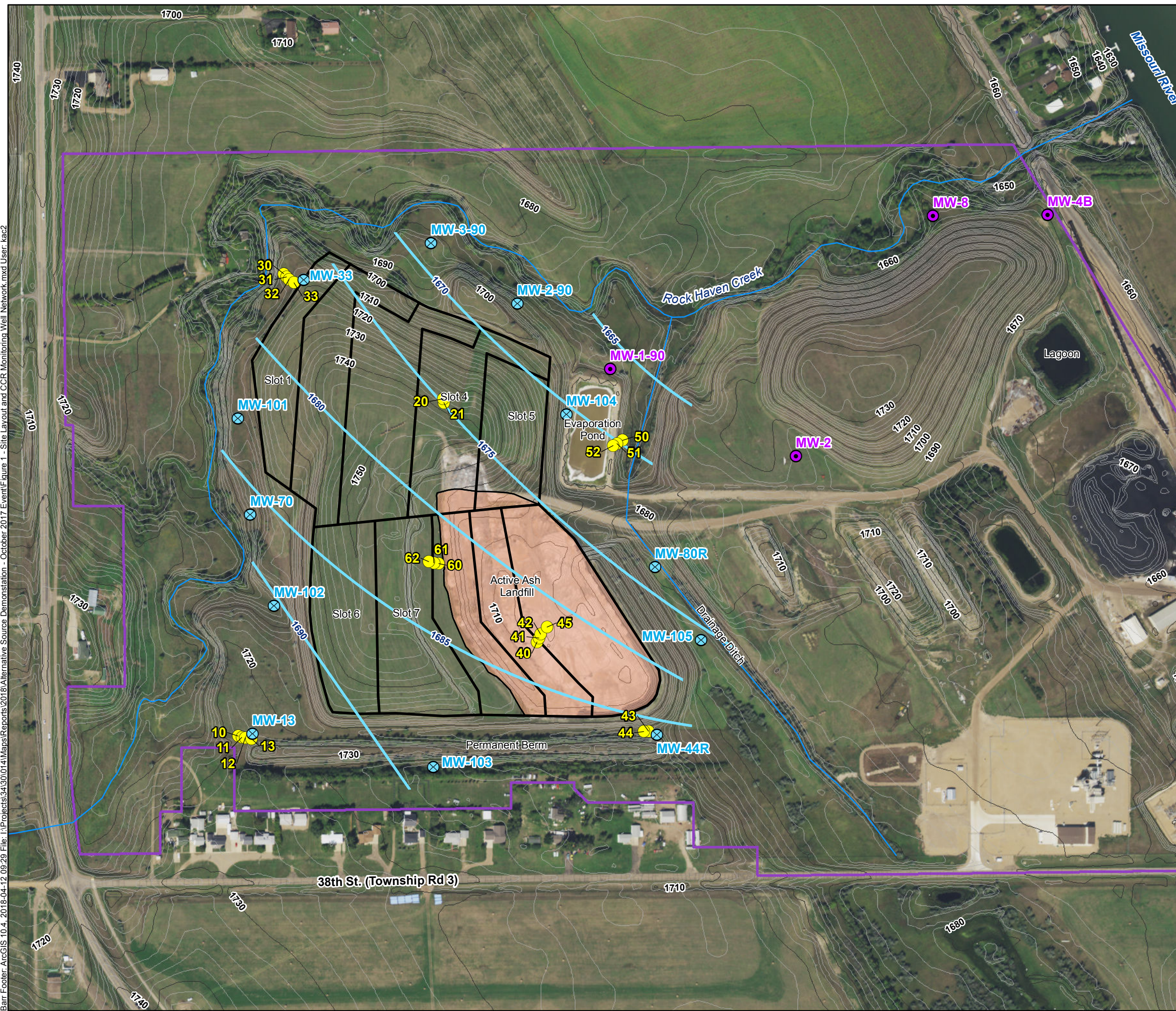
Lindholm, R., 1983. Bivalve Associations of Cannonball Formation (Paleocene, Danian) of North Dakota. AAPG Bulletin, Volume 67, Issue 8, P1347. Meeting abstract available at:
<http://archives.datapages.com/data/bulletns/1982-83/data/pg/0067/0008/1300/1347a.htm>

Montana-Dakota Utilities Co. (MDU), 1989, R.M. Heskett Station Special Use Disposal Site Permit Application. Submitted to North Dakota State Department of Health, March 1, 1989.

US EPA, 2015, Hazardous and Solid Waste Management Systems; Management of Coal Combustion Residuals From Electric Utility, CFR Parts 257 and 261 , Federal Register, Vol. 80, No. 74, April 17, 2015.

Figures

Barr Footer: ArcGIS 10.4, 2018-04-12 09:29 File: I:\Projects\3430\014\Maps\Reports\2018\Alternative Source Demonstration - October 2017 Event\Figure 1 - Site Layout and CCR Monitoring Well Network.mxd User: kac2













-  Monitoring Well Location
-  Monitoring Well Location - Water Level Only
-  Pre-Landfill Wells (Approximate)
-  June 2017 Groundwater Contours (dashed were inferred)
-  Existing Slot Boundaries
-  Streams
-  Property Line
-  10ft Contours
-  2ft Contours
-  Active Portion of Landfill

Image Source: 2017 Statewide Imagery (ND GIS Hub)

CAD Data Source: Slot Linework.dwg

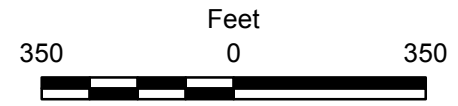
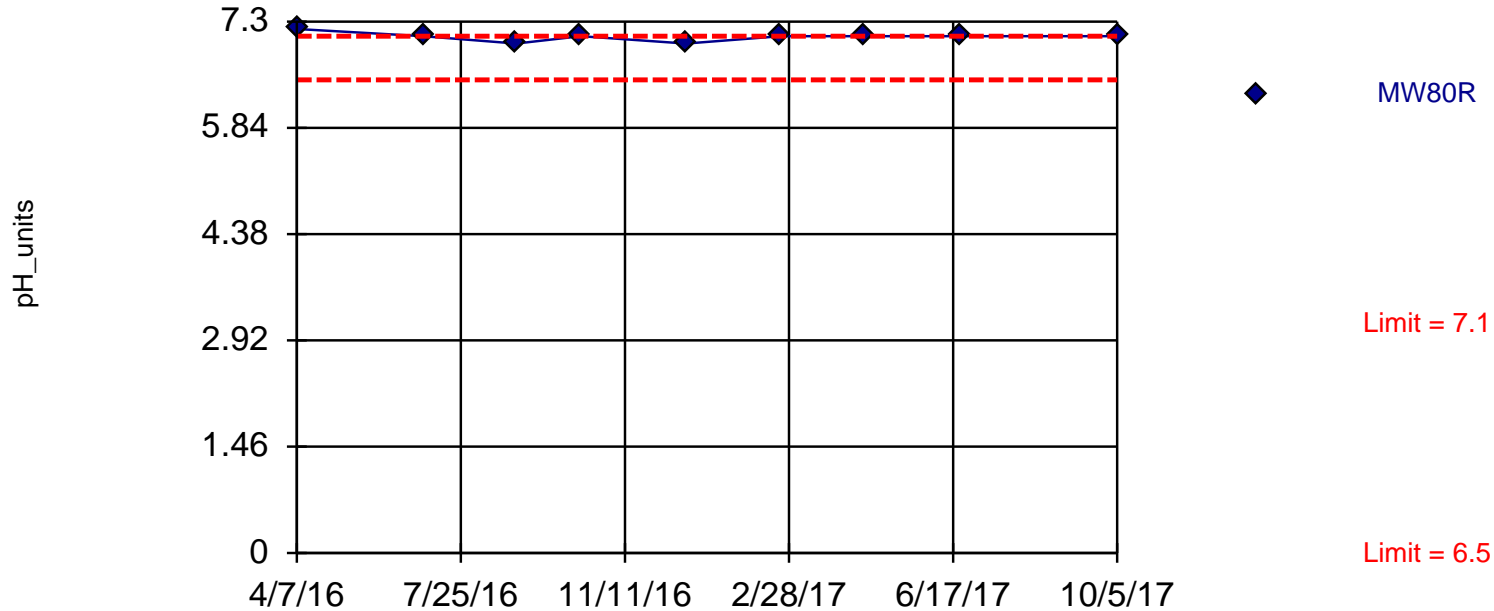


Figure 1

**SITE LAYOUT AND CCR
MONITORING WELL NETWORK**
R. M. Heskett Station
Alternative Source Demonstration:
October 2017 Event
Montana Dakota Utilities
Mandan, North Dakota

Within Limits

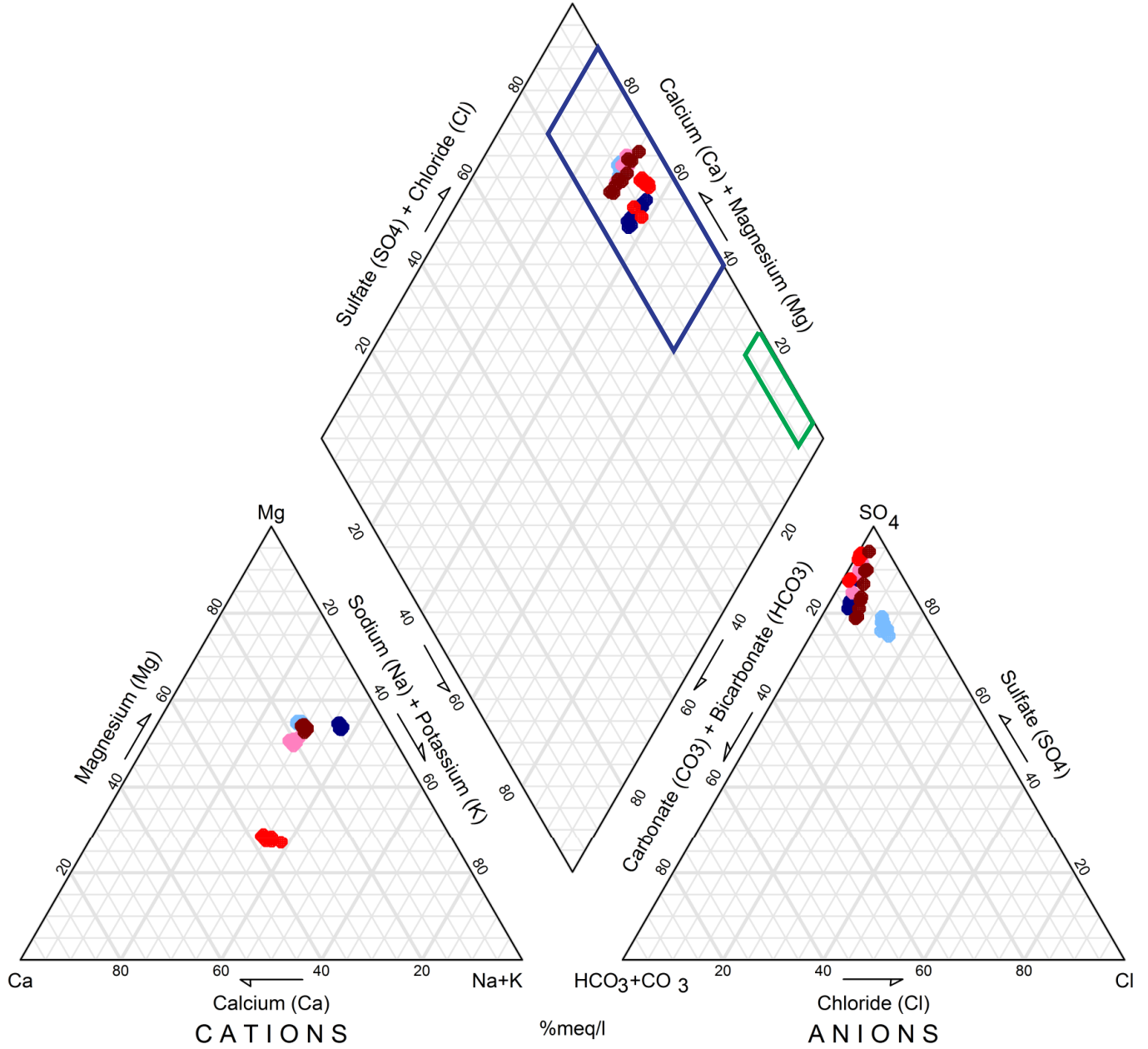
Prediction Limit
Interwell Non-parametric



Non-parametric test used in lieu of interwell control chart because the Shapiro Francia normality test showed the data to be non-normal at the 0.05 alpha level. Limits are highest and lowest of 68 background values. Annual per-constituent alpha = 0.008286. Individual comparison alpha = 0.0008301 (1 of 2). Most recent point compared to limit. Assumes 4 future values.

Constituent: pH, Field Analysis Run 4/6/2018 12:38 PM
Heskett Station Client: Barr Engineering Company Data: pH

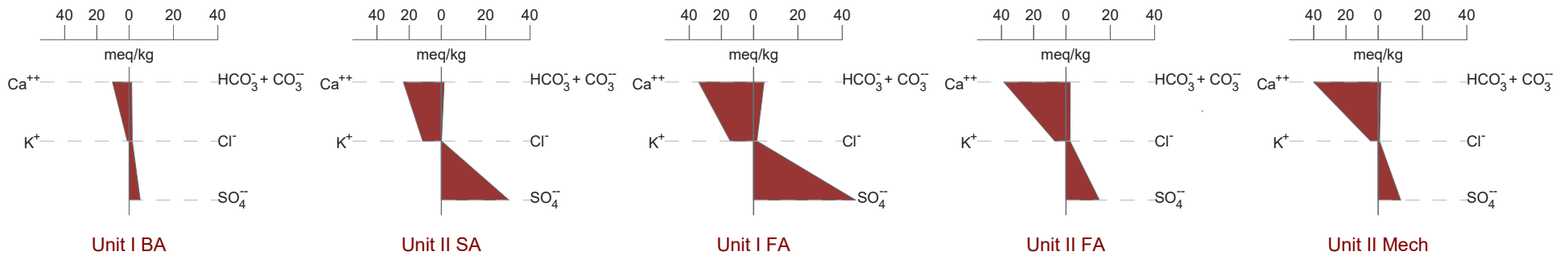
Piper Diagram



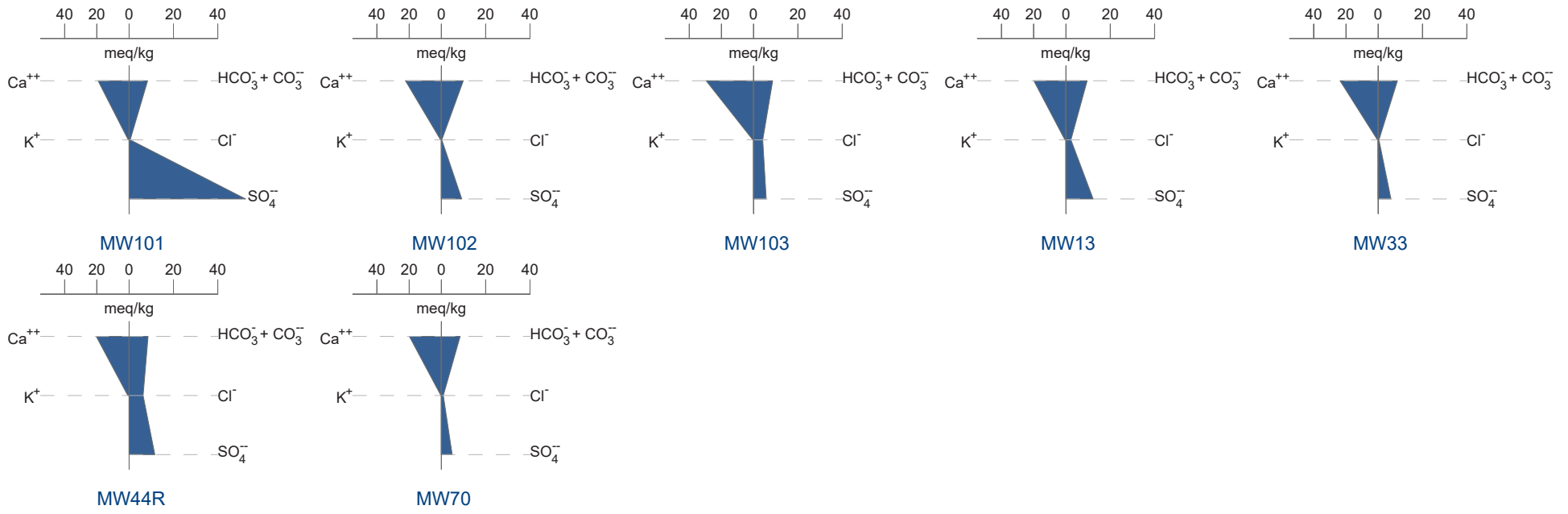
- MW104
- MW105
- MW2-90
- MW3-90
- MW-80R
- Upgradient
- Ash SPLP

Figure 3
 PIPER PLOT
 R.M. Heskett Station
 Alternative Source Demonstration
 October 2017 Event
 Montana Dakota Utilities
 Mandan, North Dakota

Ash SPLP Results



Upgradient



Downgradient

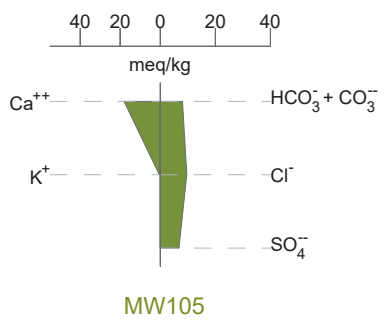
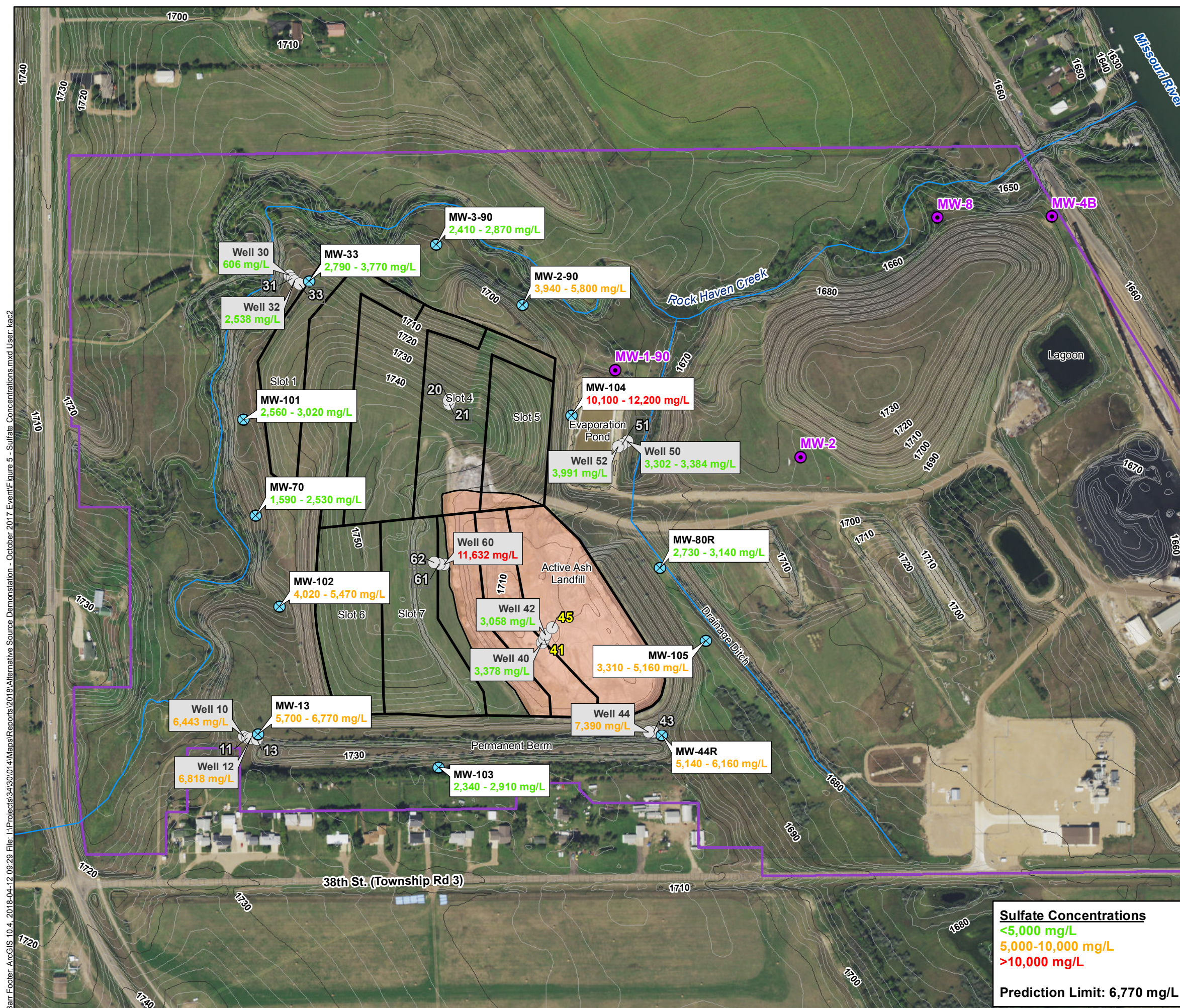


Figure 4

STIFF PLOTS
 R. M. Heskett Station
 Alternative Source Demonstration
 October 2017 Event
 Montana Dakota Utilities
 Mandan, North Dakota

Notes: Stiff plots show concentrations of selected cations and anions in milliequivalents per kilogram of water. Sulfate concentrations are plotted as 10% of actual values for scaling.



- Monitoring Well Location
- Monitoring Well Location - Water Level Only
- Pre-Landfill Wells (Approximate)
- Existing Slot Boundaries
- Streams
- Property Line
- 10ft Contours
- 2ft Contours
- Active Portion of Landfill

Image Source: 2017 Statewide Imagery (ND GIS Hub)
 CAD Data Source: Slot Linework.dwg
 Pre-Landfill well concentrations are from 9/11/1986, 11/21/1986 (MDU, 1989), and CCR Rule monitoring well concentrations are from 2016 and 2017.

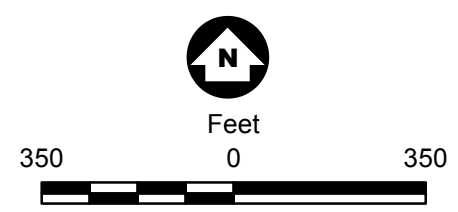


Figure 5
 SULFATE CONCENTRATIONS
 R. M. Heskett Station
 Alternative Source Demonstration:
 October 2017 Event
 Montana Dakota Utilities
 Mandan, North Dakota

Barr Footer: ArcGIS 10.4, 2018-04-12 09:29 File: I:\Projects\3430\014\Maps\Reports\2018\Alternative Source Demonstration - October 2017 Event\Figure 5 - Sulfate Concentrations.mxd User: kac2

Tables

Table 1
 October 2017 SSIs
 R.M. Heskett Station
 Montana-Dakota Utilities Co.

Well	Parameter (unit)	Concentration		
		Prediction Limit ¹	Detection Monitoring (10/5/17) ²	Verification Resample (1/22/18)
MW-80R	pH (SU)	7.07	7.1	7.12
MW-105	Chloride (mg/L)	271	346	339
MW-104	Sulfate (mg/L)	6,770	10,200	11,300
MW-104	Total Dissolved Solids (TDS; mg/L)	9,970	15,400	16,200

¹ SSIs determined by prediction limits (parametric for pH; non-parametric for chloride, sulfate, and TDS).

² TDS sample at MW-104 taken November 6, 2017.

Table 2
 Select Parameter Concentrations: Ash SPLP, MW-104, and MW-105
 R.M. Heskett Station
 Montana-Dakota Utilities Co.

Location	Date	Parameter (mg/L) ¹						
		B	Ca	Cl	F	pH	SO ₄	TDS
Unit 1 Bottom Ash SPLP	7/22/2011	<0.5	210	50.5	0.1	12.2	2,440	4,860
Unit 2 Sand Ash SPLP	7/22/2011	5.96	481	2	0.1	11.1	14,900	22,500
Unit 1 Fly Ash SPLP	7/22/2011	2	700	54	5.6	12.9	22,600	42,200
Unit II Fly Ash SPLP	7/22/2011	<1	785	66	3.6	12.8	7,400	16,000
Unit II Mechanicals SPLP	7/22/2011	<1	818	20.8	0.6	12.7	4,960	11,400
Fly Ash Unit 1&2 SPLP	11/30/2011	0.51	710	50.6	3.35	12.8	8,380	17,900
MW-104 (Fall 2017)	10/5/2017 ²	0.81	430	99.6	0.5	6.82	10,200	15,400
MW-105 (Fall 2017)	10/5/2017 ²	<0.5	367	346	0.24	6.6	3,310	6,650

¹ pH is in standard units (SU)

² TDS from samples collected 11/6/2017

Table 3
Select Parameter Concentrations: Historical Well 60 and MW-104
R.M. Heskett Station
Montana-Dakota Utilities Co.

Location	Date	B	Ca	Cl	F	pH	SO4	TDS
Well 60	11/21/1986	n.m.	417	208	0.5	6.83	11,632	14,917
	12/20/1988	1.8	415	273	0.64	7	10,780	17,634
MW-104	10/5/2017	1	430	100	0.5	6.82	10,200	15,400

Units are mg/L or pH standard units.

n.m.: Not measured

Appendices

Appendix A YSI Sensor Specifications



YSI 600XL and 600XLM Sondes

Measure multiple parameters simultaneously

The YSI 600XL and YSI 600XLM compact sondes measure eleven parameters simultaneously:

Temperature	TDS
Conductivity	pH
Specific Conductance	ORP
Salinity	Depth or Level
Resistivity	Rapid Pulse™ DO (% and mg/L)



The YSI 600XL and 600XLM

Connect with Data Collection Platforms

Either sonde can easily connect to the YSI 6200 DAS (Data Acquisition System), YSI EcoNet™ or your own data collection platform, via SDI-12 for remote and real-time data acquisition applications.

Economical Logging System

The YSI 600XLM is an economical logging system for long-term, *in situ* monitoring and profiling. It will log all parameters at programmable intervals and store 150,000 readings. At one-hour intervals, the instrument will log data for about 75 days utilizing its own power source. The 600XL can also be utilized in the same manner with user-supplied external power.

- Either sonde fits down 2-inch wells
- Horizontal measurements in very shallow waters
- Stirring-independent Rapid Pulse® dissolved oxygen sensor
- Field-replaceable sensors
- Easily connects to data collection platforms
- Available with detachable cables to measure depth up to 200 feet
- Compatible with YSI 650 Multiparameter Display System
- Use with the YSI 5083 flow cell for groundwater applications

Pure
Data for a
Healthy
Planet.®
Economical, multiparameter
sampling or logging in a
compact sonde

Sensor performance verified*

The 6820 VZ and 6920 VZ sondes use sensor technology that was verified through the US EPA's Environmental Technology Verification Program (ETV). For information on which sensors were performance-verified, turn this sheet over and look for the ETV logo.





To order, or for more info,
contact YSI Environmental.

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www.ysi.com

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ISO 9001
ISO 14001

Yellow Springs, Ohio Facility

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*Sensors with listed with the ETV logo were submitted to the ETV program on the YSI 6000EIS. Information on the performance characteristics of YSI water quality sensors can be found at www.epa.gov/etv, or call YSI at 800.897.4151 for the ETV verification report. Use of the ETV name or logo does not imply approval or certification of this product nor does it make any explicit or implied warranties or guarantees as to product performance.

YSI incorporated
Who's Minding
the Planet?[®]

YSI 600XL & 600XLM Sensor Specifications

	Range	Resolution	Accuracy
Dissolved Oxygen % Saturation 6562 Rapid Pulse™ Sensor* ET ✓	0 to 500%	0.1%	0 to 200%: ±2% of reading or 2% air saturation, whichever is greater; 200 to 500%: ±6% of reading
Dissolved Oxygen mg/L 6562 Rapid Pulse™ Sensor* ET ✓	0 to 50 mg/L	0.01 mg/L	0 to 20 mg/L: ±0.2 mg/L or 2% of reading, whichever is greater; 20 to 50 mg/L: ±6% of reading
Conductivity* 6560 Sensor* ET ✓	0 to 100 mS/cm	0.001 to 0.1 mS/cm (range dependent)	±0.5% of reading + 0.001 mS/cm
Salinity	0 to 70 ppt	0.01 ppt	±1% of reading or 0.1 ppt, whichever is greater
Temperature 6560 Sensor* ET ✓	-5 to +50°C	0.01°C	±0.15°C
pH 6561 Sensor* ET ✓	0 to 14 units	0.01 unit	±0.2 unit
ORP	-999 to +999 mV	0.1 mV	±20 mV
Depth & Level Medium Shallow Vented Level	0 to 200 ft, 61 m 0 to 30 ft, 9.1 m 0 to 30 ft, 9.1 m	0.001 ft, 0.001 m 0.001 ft, 0.001 m 0.001 ft, 0.001 m	±0.4 ft, ±0.12 m ±0.06 ft, ±0.02 m ±0.01 ft, 0.003 m

* Report outputs of specific conductance (conductivity corrected to 25° C), resistivity, and total dissolved solids are also provided. These values are automatically calculated from conductivity according to algorithms found in *Standard Methods for the Examination of Water and Wastewater* (ed 1989).

YSI 600XL & 600XLM Sonde Specifications

Medium		Fresh, sea or polluted water
Temperature	Operating Storage	-5 to +50°C -10 to +60°C
Communications		RS-232, SDI-12
Software		EcoWatch®
Dimensions	Diameter Length Weight	1.65 in, 4.19 cm 1.65 in, 4.9 cm 16 in, 40.6 cm 21.3 in, 54.1 cm 1.3 lbs, 0.59 kg 1.5 lbs, 0.69 kg
Power	External Internal (600XLM only)	12 V DC 4 AA-size alkaline batteries

YSI model 5083
flow cell and
600XL. This is an
ideal combination
for groundwater
applications.



Appendix B SPLP Laboratory Data

EXHIBIT 2-A

WASTE LEACHATE EXTRACTION ANALYSES



MINNESOTA VALLEY TESTING LABORATORIES, Inc.



PHONE (507) 354-8517

P.O. BOX 249, CENTER & GERMAN STREETS, NEW ULM, MINNESOTA 56073-0249

Report To: Montana Dakota Utilities
400 North 4th Street
Bismarck, ND 58501

Date: November 11, 1986

Work Order # CS-2251

Attn: John Verwey

Date Received: 9-25-86

Sample Identification: Coarse Ash Hopper, Precipitation Hopper Comp.

Analyses	Unit #1	
	Coarse Ash Hopper (Bottom Ash)	Precipitation Hopper Comp. (Fly Ash)
Total Alkalinity as CaCO ₃ ...mg/l..	414	1.472
Bicarbonate as CaCO ₃ ...mg/l.....	161	150
Calcium.....mg/l.....	77.5	95.0
Carbonate as CaCO ₃ ...mg/l.....	253	1,323
Chloride.....mg/l.....	19.0	23.0
Fluoride.....mg/l.....	0.11	0.22
Hardness as CaCO ₃ ...mg/l.....	194	238
Iron.....mg/l.....	0.2	0.2
Manganese.....mg/l.....	< 0.01	0.01
Magnesium.....mg/l.....	0.1	0.1
Nitrate.....mg/l.....	< 1.0	< 1.0
pH.....	11.5	12.6
Potassium.....mg/l.....	15.0	100
Sodium.....mg/l.....	380	2,200
Specific Conductance micromhos/cm	2,544	15,001
Sulfate.....mg/l.....	900	6,550
Total Dissolved Solids...mg/l....	1,357	10,389
Boron.....mg/l.....	0.91	1.18

EP TOX Extraction
no acid added.

BY Jerome Kolesky



MINNESOTA VALLEY TESTING LABORATORIES, Inc.



PHONE (507) 354-8517

P.O. BOX 249, CENTER & GERMAN STREETS, NEW ULM, MINNESOTA 56073-0249

Report To: Montana Dakota Utilities
400 North 4th Street
Bismarck, ND 58501

Attn: John Verwey

Date: November 11, 1986
Work Order # CS-2251
Date Received: 9-25-86

Sample Identification: Coarse Ash Hopper, Precipitation Hopper Comp.

Analyses	Unit #1 Bottom Ash	Unit #1 Fly Ash
	Coarse Ash Hopper	Precipitation Hopper Comp.
Arsenic.....mg/l.....	< 0.002	0.070
Barium.....mg/l.....	< 0.5	< 0.5
Cadmium.....mg/l.....	< 0.01	0.02
Chromium.....mg/l.....	< 0.05	< 0.05
Lead.....mg/l.....	< 0.10	0.40
Mercury.....mg/l.....	< 0.002	< 0.002
Selenium.....mg/l.....	< 0.003	0.003
Silver.....mg/l.....	< 0.05	< 0.05
Molybdenum....mg/l.....	< 0.50	< 0.50

EP-TOX Extraction
no acid added

BY Jerome Kotecky



MINNESOTA VALLEY TESTING LABORATORIES, Inc.



PHONE (507) 354-8517

P.O. BOX 249, CENTER & GERMAN STREETS, NEW ULM, MINNESOTA 56073-0249

Report To: Montana Dakota Utilities
400 North 4th Street
Bismarck, ND 58501

Date: November 11, 1986

Work Order # CS-2251

Attn: John Verwey

Date Received: 9-25-86

Sample Identification: Bed Ash, Bag House

*Unit #2
Bottom Ash*

*Unit #2
Fly Ash*

Analyses	Bed Ash	Bag House
Total Alkalinity as CaCO ₃ ...mg/l..	173	598
Bicarbonate as CaCO ₃ ...mg/l.....	69.0	80.5
Calcium.....mg/l.....	570	105
Carbonate as CaCO ₃ ...mg/l.....	103.5	517.5
Chloride.....mg/l.....	5.0	21.0
Fluoride.....mg/l.....	< 0.10	0.27
Hardness as CaCO ₃ ...mg/l.....	1,429	263
Iron.....mg/l.....	0.2	0.1
Manganese.....mg/l.....	< 0.01	< 0.01
Magnesium.....mg/l.....	1.4	0.1
Nitrate.....mg/l.....	< 1.0	< 1.0
pH.....	10.7	11.9
Potassium.....mg/l.....	40.0	100
Sodium.....mg/l.....	1,200	2,350
Specific Conductance micromhos/cm	7,066	10,870
Sulfate.....mg/l.....	4,300	6,160
Total Dissolved Solids...mg/l....	5,774	8,324
Boron.....mg/l.....	1.20	1.70

*EP TOX Extraction
no acid added*

BY *Jerome Kotecky*



MINNESOTA VALLEY TESTING LABORATORIES, Inc.



PHONE (507) 354-8517

P.O. BOX 249, CENTER & GERMAN STREETS, NEW ULM, MINNESOTA 56073-0249

Report To: Montana Dakota Utilities
400 North 4th Street
Bismarck, ND 58501

Attn: John Verwey

Date: November 11, 1986

Work Order # CS-2251

Date Received: 9-25-86

Sample Identification: Bed Ash, Bag House

*Unit #2
Bottom Ash*

*Unit #2
Fly Ash*

Analyses	Bed Ash	Bag House
Arsenic.....mg/l.....	0.155	0.045
Barium.....mg/l.....	< 0.5	< 0.5
Cadmium.....mg/l.....	0.02	0.03
Chromium.....mg/l.....	< 0.05	< 0.05
Lead.....mg/l.....	0.35	0.25
Mercury.....mg/l.....	< 0.002	< 0.002
Selenium.....mg/l.....	< 0.003	0.004
Silver.....mg/l.....	< 0.05	< 0.05
Molybdenum....mg/l.....	< 0.50	< 0.50

*EP TOX Extraction
no acid added.*

BY _____

Jerome Kotecky



*Sewer
ad - Utilization*

**MINNESOTA VALLEY
TESTING LABORATORIES, Inc.**



PHONE (507) 354-8517

P.O. BOX 249, CENTER & GERMAN STREETS, NEW ULM, MINNESOTA 56073-0249

*BIOB method
No X detection
1-20?*

**Report To: Montana Dakato Utilities Co.
Attn: Gene Brown
P.O. Box 40
Mandan, ND 58554**

Date: November 18, 1987

Work Order # 12-2237

Date Received: 9-29-87

Sample Identification: EPA Toxicity

Unit #2 bottom ad

<u>Analysis</u>	<u>4638</u>
Arsenic.....mg/L.....	0.004
Barium.....mg/L.....	< 0.1
Cadmium.....mg/L.....	< 0.05
Chromium.....mg/L.....	0.14
Lead.....mg/L.....	< 0.100
Mercury.....mg/L.....	0.0003
Selenium.....mg/L.....	< 0.003
Silver.....mg/L.....	0.04

A FULL SERVICE LABORATORY

BY David A. Diamond

MVTL guarantees the accuracy of the analysis done on the sample submitted for testing. It is not possible for MVTL to guarantee that a test result obtained on a particular sample will be the same on any other sample unless all conditions affecting the sample are the same, including sampling by MVTL. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

LABORATORY REPORT

To: Mineral Specialities (1)
Address: P.O. Box 1563
Billings, Montana 59103
ATTN: Jerry Vollmer

Lab No.: 87-7859
Date: 7/24/87 pjf

EP TOXICITY ANALYSIS - Fly Ash - Unit 2

Heskett Plant, North Dakota
Submitted 6/26/87

Extraction and analysis performed according to SW-846,
Test Methods for Evaluating Solid Waste.

<u>CONSTITUENT</u>	<u>mg/l in extract</u>
Arsenic	<0.5
Barium	<10
Cadmium	<0.1
Chromium	<0.5
Lead	<0.5
Mercury	<0.02
Selenium	0.2
Silver	<0.5

Post-it® Fax Note	7671	Date	4/3	# of pages	1
To	Alan Wette	From	Andrea		
Co./Dept.		Co.			
Phone #		Phone #			
Fax #		Fax #			

Appendix C Aerial Photograph (1988)

SINGLE
FAMILY
RESIDENTIAL

SINGLE
FAMILY
RESIDENTIAL

INDUSTRIAL

PROPOSED

ASH

DISPOSAL

SITE

INDUSTRIAL

R.M. HESKETT STATION

AGRICULTURAL

MULTIPLE
FAMILY
RESIDENTIAL

INDUSTRIAL

EXHIBIT 3-C
HESKETT SITE
AERIAL PHOTO & ZONING

Scale: 1" = 200'
3-30-88

**Appendix D 1989 Special Use Disposal Site
Permit Application**

R. M. HESKETT STATION

SPECIAL USE DISPOSAL SITE

PERMIT APPLICATION

Montana-Dakota Utilities Co.
400 North 4th Street
Bismarck, ND 58501

March 1, 1989

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1.0 INTRODUCTION

This application describes hydrogeologic, constructional, and operational details relevant to the procurement of a Solid Waste Disposal Permit from the State of North Dakota. The characterization data and design specifications contained within this application are based upon results obtained from a 1986 investigation which focused upon selecting a waste disposal site that would be suitable for long-term disposal of coal combustion ash generated at the R.M. Heskett Station. The specific objective was to locate a site that would require minimal engineering design and allow the use of in-situ materials for leachate containment and chemical attenuation. Several localities were considered with one site being selected for a highly detailed geohydrologic evaluation. The proposed ash disposal site is located approximately one-quarter mile west of Heskett Station and 2 miles north of Mandan, ND.

A total of 27 monitoring wells were installed in and around the site. The monitoring of well water levels over a two year period has indicated the presence of a static water table (generally 30-40 feet below the ground surface) which flows in a north-northeasterly direction. Potentiometric levels indicated a substantial downward component of groundwater flow over the entire proposed disposal site.

During the operational phase of ash disposal primary objectives will include the minimization of fugitive dust production and preservation of the area landscape by continual reclamation of ash-filled "trenches". Frequent coverage of the trenches with low permeability earthen materials, in conjunction with in-pit water collection devices and an evaporative liquids treatment system, is expected to reduce highly mineralized leachate generation and its degradation potential to the poor-quality groundwater resource beneath

the facility. The suitability of the disposal setting is further assured by the placement of waste above the historic water table and the construction of a surface water drainage system adjacent to the site. Contingencies have also been identified which would hinder unanticipated increases in water table elevation.

2.0 WASTE INFORMATION

2.1 Sources of Waste

Montana-Dakota Utilities Co. currently operates two lignite-fired electrical generation units at its R. M. Heskett Station. Unit #1, operational since 1954, utilizes a spreader stoker-type steam generator in the production of up to 20,000 Kw/hr of electrical energy. Unit #2 became functional in 1963 with a boiler similar in design to Unit #1. In early 1987, Unit #2 was converted to an atmospheric fluidized bed combustor capable of supporting a turbine capacity of 73,000 Kw/hr. Units #1 and #2 have an anticipated remaining operational life of 20 years and 30 years, respectively. Both units produce fly ash and bottom ash as the mineral residue of lignite combustion.

2.2 Amounts of Waste Produced

Annual ash generation rates from Heskett Station are estimated in Table 2.1. The proposed disposal facility is designed to accommodate the combustion wastes that will be generated throughout the remaining operational life of Unit #1 (175,000 tons or 1.5×10^5 cy) and Unit #2 (1,569,000 tons or 1.4×10^6 cy).

TABLE 2-1

Annual Ash Generation from Units 1 and 2
at R. M. Heskett Station

	FLY ASH		BOTTOM ASH		SAND ¹	
	Tons	Cubic Yards	Tons	Cubic Yards	Tons	Cubic Yards
Unit 1	4035	4000	4737	3500	-----	-----
Unit 2	25877	25500	10569	7800	15854	11800
Total	29912	29500	15306	11300	15854	11800
Percent (by weight)	49	-----	25	-----	26	-----
Estimated total weight of ash (with sand) 61,070 tons						
Estimated total volume of ash (with sand) 52,600 cubic yards						

¹ Sand is only used within the fluidized bed of Unit #2.

2.3 Description of Waste

All lignite combustion waste produced at Heskett Station will be deposited within the disposal facility in a nonsegregated manner. The combined ash-types differ in color from a light brown to gray-black. Waste texture can vary from a fine, flour-like powder to a distinctly granular consistency. The fluidized bed combustor for Unit #2 utilizes significant amounts of inert sand as a bed matrix. During combustion this sand becomes coated and interspersed with bottom ash slag. Bed sand will be disposed of with the fly ash/bottom ash mixture. The fluidized bed material is visually obvious in the ash mixture due to its uniform granular appearance.

An analysis was performed on the leachate of representative samples of each type of ash waste intended for disposal at the proposed facility. Fly ash and bottom ash samples were collected from Unit #1 ash hoppers during normal operations. Unit #2 fly ash and bottom ash samples were obtained during a "test burn" of Beulah lignite in a scale model fluidized bed steam generation system.

Leachate was extracted from each ash sample using EPA Extraction Procedure Method 1310 (EP Toxicity Test) without pH adjustments (no acetic acid additions). Exhibit 2-A present results of the analytical analysis for both fly ash and bottom ash types. (Because Unit #2 fly ash and bottom ash were collected from a test burn, an EP Toxicity Test was later performed to characterize operational ash samples - these results also appear in Exhibit 2-A.)

The pH of all ash leachates appeared quite alkaline in nature. Fly ashes from Units #1 and #2 contained more alkali than their respective bottom

ashes. Leachate pH was considered an important factor in judging site suitability in that it controls the release of trace elements which are locked in the lattice structures of various mineral phases of lignite combustion residue (Groenewold et al., 1980). Sulfate and sodium concentrations were also higher in the fly ashes when compared to those of the bottom ashes.

Leachate from all ash samples, except Unit #1 bottom ash, contained detectable levels of arsenic, cadmium and lead. Selenium was detected only in the fly ash of both units. Fluoride, iron, magnesium, chloride and boron occurred in both the fly and bottom ash leachate at very low concentrations. Nitrates and other analyzed trace elements were near or below laboratory detection limits.

EXHIBIT 2-A

WASTE LEACHATE EXTRACTION ANALYSES



MINNESOTA VALLEY TESTING LABORATORIES, Inc.



PHONE (507) 354-8517

P.O. BOX 249, CENTER & GERMAN STREETS, NEW ULM, MINNESOTA 56073-0249

Report To: Montana Dakota Utilities
400 North 4th Street
Bismarck, ND 58501

Date: November 11, 1986

Work Order # CS-2251

Attn: John Verwey

Date Received: 9-25-86

Sample Identification: Coarse Ash Hopper, Precipitation Hopper Comp.

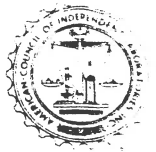
Analyses	Unit #1	
	Coarse Ash Hopper (Bottom Ash)	Precipitation Hopper Comp. (Fly Ash)
Total Alkalinity as CaCO ₃ ...mg/l..	414	1.472
Bicarbonate as CaCO ₃ ...mg/l.....	161	150
Calcium.....mg/l.....	77.5	95.0
Carbonate as CaCO ₃ ...mg/l.....	253	1,323
Chloride.....mg/l.....	19.0	23.0
Fluoride.....mg/l.....	0.11	0.22
Hardness as CaCO ₃ ...mg/l.....	194	238
Iron.....mg/l.....	0.2	0.2
Manganese.....mg/l.....	< 0.01	0.01
Magnesium.....mg/l.....	0.1	0.1
Nitrate.....mg/l.....	< 1.0	< 1.0
pH.....	11.5	12.6
Potassium.....mg/l.....	15.0	100
Sodium.....mg/l.....	380	2,200
Specific Conductance micromhos/cm	2,544	15,001
Sulfate.....mg/l.....	900	6,550
Total Dissolved Solids...mg/l....	1,357	10,389
Boron.....mg/l.....	0.91	1.18

EP TOX Extraction
no acid added.

BY Jerome Kolesky



MINNESOTA VALLEY TESTING LABORATORIES, Inc.



PHONE (507) 354-8517

P.O. BOX 249, CENTER & GERMAN STREETS, NEW ULM, MINNESOTA 56073-0249

Report To: Montana Dakota Utilities
400 North 4th Street
Bismarck, ND 58501

Attn: John Verwey

Date: November 11, 1986
Work Order # CS-2251
Date Received: 9-25-86

Sample Identification: Coarse Ash Hopper, Precipitation Hopper Comp.

Analyses	Unit #1 Coarse Ash Hopper	Unit #1 Precipitation Hopper Comp.
	Bottom Ash	Fly Ash
Arsenic.....mg/l.....	< 0.002	0.070
Barium.....mg/l.....	< 0.5	< 0.5
Cadmium.....mg/l.....	< 0.01	0.02
Chromium.....mg/l.....	< 0.05	< 0.05
Lead.....mg/l.....	< 0.10	0.40
Mercury.....mg/l.....	< 0.002	< 0.002
Selenium.....mg/l.....	< 0.003	0.003
Silver.....mg/l.....	< 0.05	< 0.05
Molybdenum....mg/l.....	< 0.50	< 0.50

EP-TOX Extraction
no acid added

BY Jerome Kotecky



MINNESOTA VALLEY TESTING LABORATORIES, Inc.



PHONE (507) 354-8517

P.O. BOX 249, CENTER & GERMAN STREETS, NEW ULM, MINNESOTA 56073-0249

Report To: Montana Dakota Utilities
400 North 4th Street
Bismarck, ND 58501

Date: November 11, 1986

Work Order # CS-2251

Attn: John Verwey

Date Received: 9-25-86

Sample Identification: Bed Ash, Bag House

*Unit #2
Bottom Ash*

*Unit #2
Fly Ash*

Analyses	Bed Ash	Bag House
Total Alkalinity as CaCO ₃ ...mg/l..	173	598
Bicarbonate as CaCO ₃ ...mg/l.....	69.0	80.5
Calcium.....mg/l.....	570	105
Carbonate as CaCO ₃ ...mg/l.....	103.5	517.5
Chloride.....mg/l.....	5.0	21.0
Fluoride.....mg/l.....	< 0.10	0.27
Hardness as CaCO ₃ ...mg/l.....	1,429	263
Iron.....mg/l.....	0.2	0.1
Manganese.....mg/l.....	< 0.01	< 0.01
Magnesium.....mg/l.....	1.4	0.1
Nitrate.....mg/l.....	< 1.0	< 1.0
pH.....	10.7	11.9
Potassium.....mg/l.....	40.0	100
Sodium.....mg/l.....	1,200	2,350
Specific Conductance micromhos/cm	7,066	10,870
Sulfate.....mg/l.....	4,300	6,160
Total Dissolved Solids...mg/l....	5,774	8,324
Boron.....mg/l.....	1.20	1.70

*EP TOX Extraction
no acid added*

BY *Jerome Kotecky*



MINNESOTA VALLEY TESTING LABORATORIES, Inc.



PHONE (507) 354-8517

P.O. BOX 249, CENTER & GERMAN STREETS, NEW ULM, MINNESOTA 56073-0249

Report To: Montana Dakota Utilities
400 North 4th Street
Bismarck, ND 58501

Attn: John Verwey

Date: November 11, 1986

Work Order # CS-2251

Date Received: 9-25-86

Sample Identification: Bed Ash, Bag House

*Unit #2
Bottom Ash*

*Unit #2
Fly Ash*

Analyses	Bed Ash	Bag House
Arsenic.....mg/l.....	0.155	0.045
Barium.....mg/l.....	< 0.5	< 0.5
Cadmium.....mg/l.....	0.02	0.03
Chromium.....mg/l.....	< 0.05	< 0.05
Lead.....mg/l.....	0.35	0.25
Mercury.....mg/l.....	< 0.002	< 0.002
Selenium.....mg/l.....	< 0.003	0.004
Silver.....mg/l.....	< 0.05	< 0.05
Molybdenum....mg/l.....	< 0.50	< 0.50

*EP TOX Extraction
no acid added.*

BY _____ *Jerome Kotecky*



MINNESOTA VALLEY TESTING LABORATORIES, Inc.

*Sewer
cell - Utilization*



PHONE (507) 354-8517

P.O. BOX 249, CENTER & GERMAN STREETS, NEW ULM, MINNESOTA 56073-0249

*BIOB method
No X detection
1-20?*

Report To: Montana Dakato Utilities Co.
Attn: Gene Brown
P.O. Box 40
Mandan, ND 58554

Date: November 18, 1987

Work Order # 12-2237

Date Received: 9-29-87

Sample Identification: EPA Toxicity

Unit #2 bottom cell

Analysis	4638
Arsenic.....mg/L.....	0.004
Barium.....mg/L.....	< 0.1
Cadmium.....mg/L.....	< 0.05
Chromium.....mg/L.....	0.14
Lead.....mg/L.....	< 0.100
Mercury.....mg/L.....	0.0003
Selenium.....mg/L.....	< 0.003
Silver.....mg/L.....	0.04

A FULL SERVICE LABORATORY

BY David A. Diamond

MVTL guarantees the accuracy of the analysis done on the sample submitted for testing. It is not possible for MVTL to guarantee that a test result obtained on a particular sample will be the same on any other sample unless all conditions affecting the sample are the same, including sampling by MVTL. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

LABORATORY REPORT

To: Mineral Specialities (1)
Address: P.O. Box 1563
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ATTN: Jerry Vollmer

Lab No.: 87-7859
Date: 7/24/87 pjf

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Submitted 6/26/87

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<u>CONSTITUENT</u>	<u>mg/l in extract</u>
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Mercury	<0.02
Selenium	0.2
Silver	<0.5

Post-it® Fax Note	7671	Date	4/3	# of pages	1
To	Alan Wette	From	Andrea		
Co./Dept.		Co.			
Phone #		Phone #			
Fax #		Fax #			

3.0 PROPOSED SPECIAL USE DISPOSAL SITE

3.1 Site Location

The R. M. Heskett Station is located in Morton County approximately two miles north of Mandan, ND. Disposal facility siting began by reviewing existing published geologic and hydrologic data to preliminarily identify potential sites within a 20 mile radius of Heskett Station. Five candidate sites were chosen and field evaluated. Two sites were determined as meriting further characterization and were comparatively examined in detail (Exhibit 3-A). Hydrologic, lithologic, aesthetic, economic, land use, and safety considerations indicated that the Heskett Site would prove best suited for the proposed disposal facility.

The Heskett Site is located east of Highway No. 1806 and approximately one-half mile west of Heskett Station. The site covers 47 acres of the SW1/4 of Section 10, Range 81 West, Township 139 North and is bound on the west and north by Rock Haven Creek, east by Heskett Station and the existing ash storage pile, and on the south by 43rd Street Northeast. Industrial property belonging to the Amoco Oil Refinery lies directly to the south of 43rd Street Northeast. Scattered residential housing lies adjacent to the north, west, and south of Heskett Site.

3.2 Land Use and Zoning

Heskett Site is currently owned by Montana-Dakota Utilities Co. and holds an industrial zoning designation. A plat of the site appears in Exhibit 3-B along with monitoring well location/elevation information. An examination

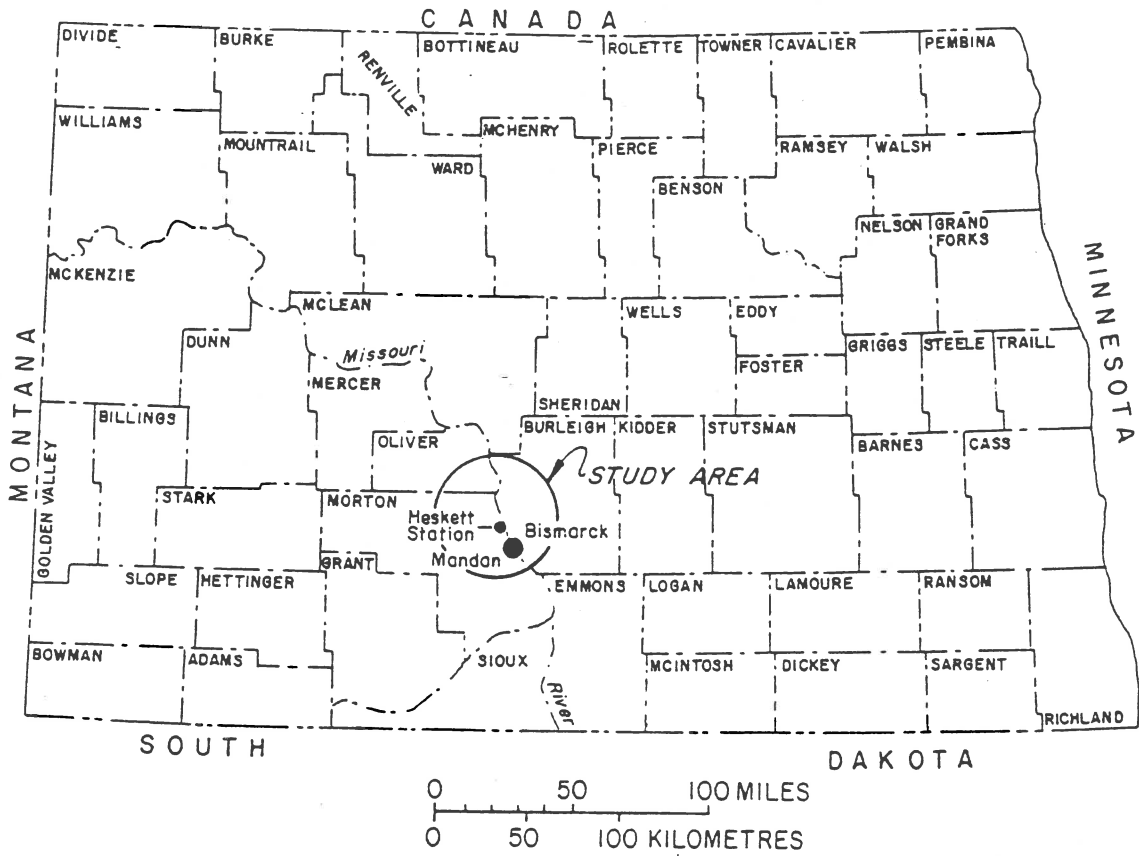
of Exhibits 3-B and 3-C indicates area land use to be primarily of an industrial and agricultural nature. The site itself is native grassland previously used for grazing livestock. Flat farmlands extend to the north while hilly pasture predominates to the west of Highway No. 1806. Level cropland and wildlife sanctuary exists on Amoco Refinery property south of 43rd Street Northeast.

Several family dwellings exist to the south and west of the Heskett Site. Other dwellings are scattered singly and in groups throughout the surrounding area. Because of the close proximity of some residences to the proposed facility, certain features will be incorporated into the design which will preserve the landscape by presenting line-of-site obstructions from the south and, if needed, west and north.

EXHIBIT 3-A

STUDY REVIEW AREA AND FINAL SITES

Study Review Area



Study Area - Final Sites

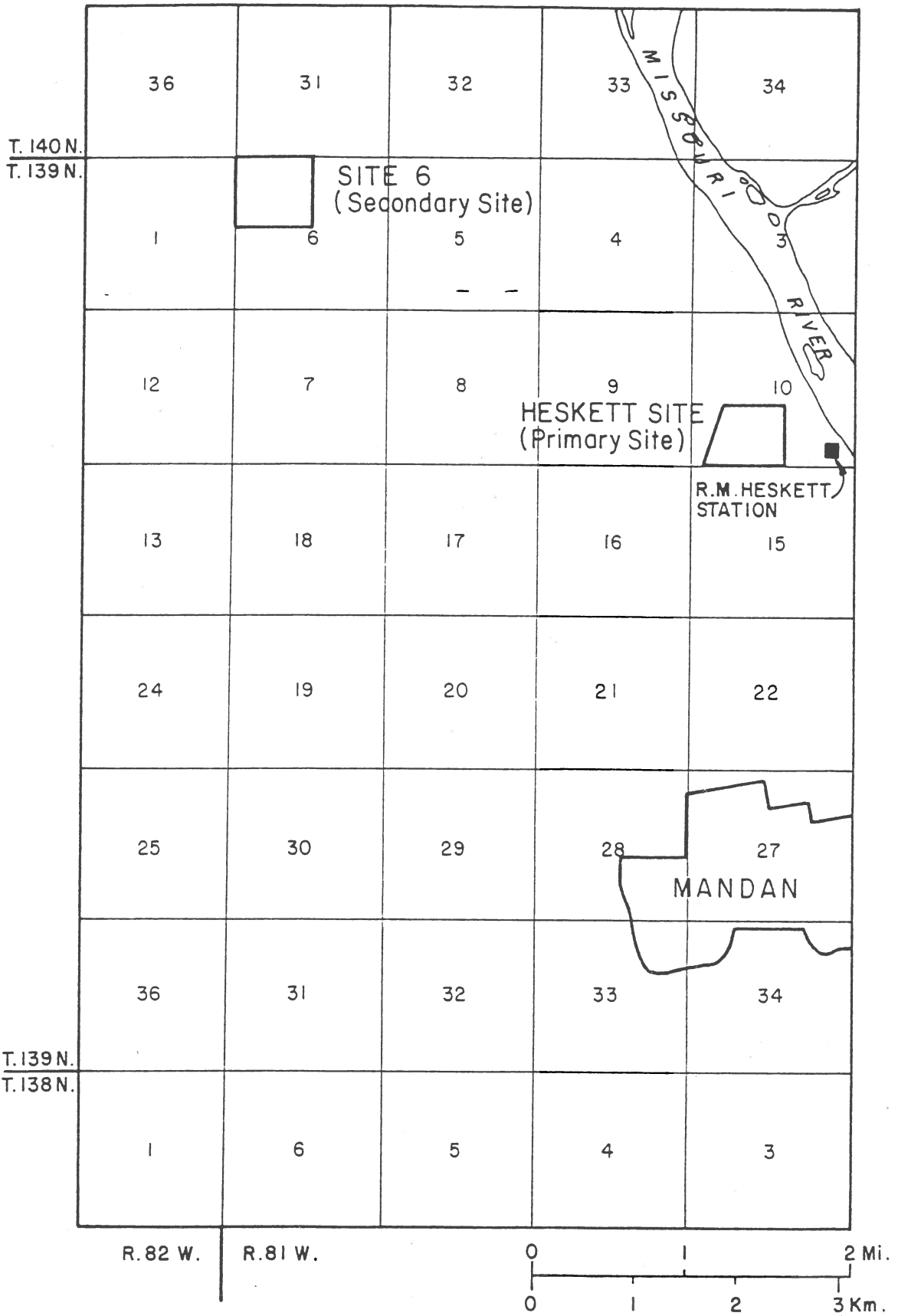


EXHIBIT 3-B

SITE PLAT/WELL SITINGS

EXHIBIT 3-C

AERIAL PHOTO AND ZONING

4.0 AREA DESCRIPTION

4.1 Geographical Setting

The disposal area is located entirely within the Missouri Plateau of the Great Plains Physiographic Province. Characterized by plains and gently sloping hills, the landscape is interrupted by isolated tablelands and river valleys entrenched 200 to 400 feet (Ackerman, 1980). Surface altitudes generally increase towards the west.

The Heskett site is a relatively flat area bounded on the west and north by an ephemeral stream (Rock Haven Creek) which supports a small shrub/woodlands community. Rock Haven Creek drains a small hilly area of approximately 2.4 square miles to the west of the site. Discharge is made directly into the Missouri River. No surface water flow gauging has ever been done at Rock Haven Creek. The North Dakota State Water Commission estimated annual flow of at least 50 acre-feet for every 80 years out of 100. One hundred acre feet of flow can be expected for 50 years out of 100.

4.2 Regional Geology

The Tertiary Cannonball Formation underlies the entire Heskett site and lies stratigraphically under several other regional formations (Exhibit 4-A). The Cannonball Formation crops out over a large portion of eastern Morton County. The bluffs along the Missouri River north of Mandan near Heskett Station are resultant from these outcrops.

The Cannonball Formation is characterized by deposits of sand, silt and clay. The beds within this formation are generally unconsolidated and tend to weather rapidly. Some of the sand units are partially cemented and are resistant to erosion. The resistant units often form benches along eroded

drainages (Carlson, 1983). Cvancara (1976) points out another characteristic of the Cannonball Formation; lack of persistent lithostratigraphic units or beds. The units are often truncated because most bedding within this formation is lenticular.

The Cretaceous and Tertiary rocks in this portion of North Dakota generally dip toward the center of the Williston Basin. Reported dips of the Cannonball Formation in the Bismarck-Mandan area are generally less than 1° and trend toward the northwest. Local irregularities in dip direction and magnitude are common in the Cannonball Formation. These minor variations are caused by small synclines and anticlines which are superimposed on the larger structure of the basin (Kume and Hansen, 1965). These small anomalies may often be responsible for local irregularities in groundwater flow direction and magnitude.

4.3 Regional Groundwater

The Cannonball Formation interfingers with its continental equivalent, the Ludlow Formation. The two formations are contemporary with deposition of the Cannonball occurring in a marine environment and deposition of the Ludlow occurring in a fresh water environment.

Aquifers within these formations are generally found in fine grained sandstones. Such units range from 5 to 129 feet thick and contain from 5 to 40 percent silt and clay. Lateral extensiveness is typically lacking. Core samples from these aquifers possess hydraulic conductivities ranging 2.9×10^{-3} cm sec⁻¹ to 1.5×10^{-5} cm sec⁻¹ (Ackerman, 1980). General groundwater movement is to the east or northeast with major discharge areas occurring in the valleys of the Missouri River, Heart River, and Big Muddy Creek.

Ackerman (1980) further states that the Cannonball and Ludlow Formation aquifers maybe in hydraulic connection with adjacent glacial drift aquifers. Area groundwater is generally of a sodium bicarbonate or sodium bicarbonate-sulfate type. Such waters are usually of poor quality for domestic usage because of high sulfate concentrations and excessive levels of total dissolved solids.

4.4 Climate

The climate of the Heskett site is semiarid with widely ranging seasonal temperatures. Summer temperatures may exceed 100°F (38°C) while winter temperatures may drop below -40°F (-40°C). The mean average annual temperature at Mandan, ND is 41.4°F (5.2°C) with average annual precipitation being 16.8 inches (42.6 cm). Approximately 60 percent of the annual precipitation (10 inches) occurs as rain during a four month period beginning in April and extending through July (U.S. Department of Commerce, 1973).

There are on the average about 125 frost-free days in this region of North Dakota. The mean depth of frost penetration is 4.5 feet (1.4 m). Extremely cold winters may occasionally allow frost to penetrate up to a depth of 7.0 feet (2.1 m) (Jensen, 1984).

The prevailing wind in the Bismarck-Mandan area is from the west-northwest with a mean velocity of 10 mph (16.1 km/hr). Winds are generally stronger in the spring and early summer as opposed to the fall and winter (Jensen, 1984).

4.5 Regional Soils

Regional near-surface materials are soils which have developed from climatic and biotic interactions with poorly consolidated sand, silt, and clay

of the Upper Cretaceous and Tertiary Formations. Glacial till appears preserved on some upland surfaces and lowland alluviums (Carlson, 1983).

Area hills have moderately steep slopes and typically have well entrenched dendritic drainageways. Patterson, et al. (1968) stated that the Bainville and Morton soil series dominate the smoothly rounded hills west of the proposed site. These soils appear on slopes of 2 to 30 percent and are well to excessively drained. Both soils, being derived from weathered medium-textured beds of the Tertiary period, tend to be loamy with high water holding capacities and somewhat limited permeabilities. Morton soils comprise 35 to 50 percent of the immediate area and are often used for cropland. Bainville soils cover 40 to 55 percent of area acreage and, being susceptible to water erosion hazards, are commonly used for pasturage.

Adjacent to the Heskett site lies the floodplain of the Missouri River. Alluvial Havre soils overlay medium-textured sediments and dominate 60 to 85 percent of the nearly level floodplain. Havre soils, with their moderate permeability and high water-holding capacities, are extensively utilized for croplands and pasturage. Well-drained Banks and Lohmiller soils each comprise 5 to 15 percent of the slightly elevated ridges and flats associated with the Missouri River floodplain (Patterson, et al., 1968).

4.6 Vegetation

The principle natural vegetative community in the study area is the mixed-grass prairie dominated by short grasses. Edwards and Ableiter (1936) stated that the smooth heavy soils of the uplands support substantial growths of western wheatgrass (Agropyron smithii) and needlegrass (Stipa comata). Little bluestem (Andropogon scoparius) commonly grows on exposed knobs and

steep slopes. Sedges, weeds, and cattails are typical of the poorly drained areas.

Natural forests are confined to bottomlands and along large streams and drainageways. Steep-sided gullies, especially those with northern exposures, contain ash (Fraxinus lanceolata), elm (Ulmus americana), aspen (Populus tremuloides), and oak (Quercus macrocarpa). The Missouri River floodplain contains significant natural stands of cottonwood trees (Populus deltoides). Also present are occasional occurrences of thicket-type woody vegetative communities dominated by buffaloberry (Shepherdia argentea). Such thickets are common in or near "woody draws" and bottomlands but seldom cover large surface expanses.

EXHIBIT 4-A

REGIONAL GEOLOGIC FORMATIONS

Regional Geologic Formations

ERA	SYSTEM	FORMATION OR GROUP	THICKNESS (FEET)	LITHOLOGY	
CENOZOIC	QUATERNARY	ALLUVIUM	0-30	SILT, SAND AND GRAVEL	
		COLEHARBOR	0-300	TILL, GRAVEL AND SAND	
	TERTIARY	FORT UNION GROUP	GOLDEN VALLEY	0-60	SILT, CLAY AND SANDSTONE
			SENTINEL BUTTE	0-700	SILT, CLAY, SAND AND LIGNITE
			BULLION CREEK	0-500	SILT, CLAY, SAND AND LIGNITE
			SLOPE	0-60	SILT, CLAY, SAND AND LIGNITE
			CANNONBALL	0-300	SILT, CLAY AND SAND
			LUDLOW	0-200	SILT, CLAY, SAND AND LIGNITE

5.0 SITE SPECIFIC CHARACTERISTICS

5.1 Site Investigation Methods

5.1.1 Site Selection Criteria

A primary concern involved the location and development of a site which would have near-surface (upper 30 feet) in-situ materials possessing characteristics similar to those of clay liner material. Relatively level near-surface sediments characterized by high clay and silt content were considered desirable. Because such materials typically transmit groundwater at slow rates, the migration of leachate into usable subsurface water supplies would be severely hindered. Another consideration was the chemical attenuation capabilities of the subsurface geologic materials. Clay and silt have been reported to generally have higher chemical attenuation capabilities than do other sediments, thereby making their presence desirable for many waste disposal settings. (Drever, 1982).

Selection of potential site areas larger than 1 square mile were based solely upon existing available data. A database was constructed which included published information from county geologic and groundwater investigative reports, soil survey reports, and water well drilling reports submitted to the North Dakota State Water Commission (NDSWC) by private contractors. Topographic maps and county zoning maps were also reviewed.

Five candidate sites were selected based upon geologic, geomorphic, and hydrologic data evaluations. Limited surficial investigations (including soil borings) were then conducted at each of the five sites. The position of the water table was very important in defining an acceptable site. Only those

sites with water tables more than 25 feet below a relatively level ground surface were considered.

Selection of two final sites were based on lithology, transport distance, road limitations, topography, and apparent depth to groundwater. Boreholes were drilled at each of the sites (maximum drilled depth was 120 feet) and lithologic/hydrologic/geophysical information recorded. Review of this information indicated that the final candidate sites had very similar geologic and hydrologic characteristics. Economics of site development, local zoning conditions, land use, transportation safety, facility access, and operational monitoring factors strongly suggested that the Heskett site was the most suitable disposal facility location.

5.1.2 Subsurface Borings

Boreholes were drilled by either a Portadrill 524 or a Denver-Gardner Heavy Duty 1000. All borings were air drilled (without the addition of drilling fluids) to reduce contaminations to groundwater. Drilling conditions for each bore hole are presented in Exhibit 5-C. Samples were collected at 5-foot intervals or at occurrences of lithologic change.

A total of 27 observation wells were installed at the Heskett site with twelve of the boreholes developed into water table monitoring wells and 15 developed as piezometers. The location of the various observation wells are shown in Exhibit 5-A. Additional information on area hydrogeochemistry was obtained from 9 wells (identified in this report as monitoring wells WS1, WS1A, WS1B, WS2, WS3, WS3A, WS4, WS4A, and WS4B) that were installed during a previous groundwater investigation which was conducted around the ash waste pile immediately east of the proposed facility (Armstrong and Schmid, 1986).

The observation wells were installed in nests of 2 to 4 single wells screened at differing elevations. Nine separate piezometer nests were installed over the Heskett study area. The deepest well in each nest was geophysically and lithologically logged (Exhibits 5-D and 5-E, respectively). A typical nest contained one water table monitoring well and two piezometers screened at different elevations.

5.1.3 Monitoring Well Construction

Monitoring wells were constructed of two-inch schedule 40 PVC pipe with screened lengths of either 4 or 20 feet. The 20-foot screened sections were installed to monitor the elevation of the water table and for water quality sampling. The 4-foot screened sections were primarily installed to monitor hydraulic head. A factory slotted size of 1 X .020 inches was used for all well screens.

A filter sand pack was placed around the screened portion of each well after the pipe was lowered into the bore hole. Washed quartz sand was packed with the use of packing poles to a height of two feet above the top of the screened interval. Before sampling was conducted each well was developed twice by backwash and mechanical surge methods.

After the sand pack was complete, sealing grout was slurried down the annulus between the bore hole and the PVC pipe. The grout seal was continued to the land surface where a two-foot diameter grout pad was constructed around each monitoring well. The monitoring wells were capped with threaded male PVC cap adapters and assigned unique well numbers.

The water level measuring reference point for the wells was the top of the PVC well pipe. Well locations and elevations can be seen on Exhibits 3-B and 5-A. Well construction data are presented in Exhibit 5-C.

5.1.4 Groundwater Monitoring

Water levels were monitored periodically during and after the course of the formal characterization study. Water level information, as determined with an electric-contact gauge tape, appears in Exhibit 5-G.

Each well was purged prior to sampling by removing at least 3 well volumes of standing water or until dry, whichever occurred first. The wells were purged with either a stainless steel and teflon mechanical two-inch submersible pump or a 1.25 inch hand bailer. All well groundwater samples were collected with a hand bailer in accordance with the Environmental Protection Agency's publication 600/4-82-029, "Handbook for Sampling and Sample Preservation of Water and Waste Water" (US EPA, 1982). Immediately after the samples were collected field pH, specific conductance and temperature were measured and recorded.

Samples were collected and preserved for major ion analysis and for trace element determinations. Other samples were collected from select wells for oil, grease, and phenol analyses. Site characterization study samples (collected in 1986) were transported to the University of North Dakota's Mining and Mineral Resources Research Institute's Fuels Analysis Laboratory for chemical analysis. Additional follow-up sampling and chemical analysis was performed in 1988 by Minnesota Valley Testing Labs of Bismarck, ND.

5.2 Site Investigation Results

5.2.1 Geology

Lithologic and geophysical logs of the wells drilled at this site indicated that at least the upper most 100 feet of subsurface material lies

within the Cannonball Formation. Consequently, the proposed Heskett waste disposal facility would be constructed completely within the Cannonball Formation. The Ludlow Formation may appear subsurface of the Heskett site study area below an elevation of 1605 feet above mean sea level (MSL). However, only the deepest bore holes penetrated to this elevation and geophysical logs from these wells do not provide any indication of contact between the two formations.

An existing topographic reference map (with well locations and cross-section locations) is provided in Exhibit 5-A. A series of eight geohydrologic cross-sections of the proposed Heskett disposal site are provided in Exhibit 5-B. Each cross-section includes topography (exaggerated 10 times), dominant lithologies, observation well locations, potentiometric levels and water table position as of October, 1986.

The Heskett Site consists of unconsolidated silt and clay with lesser amounts of very fine to medium-grained sand (lithologic log, Exhibit 5-E). The sand is generally found interspersed in a matrix of silt and clay; however, it sometimes occurs as distinct lenses which range in depth from 0.5 inches to 1 foot. The thin sand lenses are not horizontally persistent. Small gypsum crystals occur throughout the upper 30 feet of the site. These gypsum crystals are presumed to be the result of diagenetic processes which occur above the water table during alternate wetting and drying cycles (Groenewold et al., 1983).

The dominant lithology of the site is silt which commonly occurs in a clay-rich matrix. Above an elevation of 1695 feet MSL the clayey-silt is generally brownish-tan in color with grain coatings and mottling of iron-oxides. Below this elevation the color changes to steel-gray with the iron

compounds existing in the reduced state. The reduced/oxidized boundary is well defined over the site by the color change described above and corresponds with the elevation of the water table.

The uppermost indurated unit encountered beneath the proposed disposal area is a siltstone bed occurring between the elevations of 1625 feet and 1635 feet MSL. This is the most laterally continuous and persistent unit found at the Heskett site.

A thin veneer of till is present in small patches throughout the Heskett study area. This till, along with all glacial material in North Dakota, has been grouped within the Coleharbor Formation (Bluemle, 1971). The till of the Heskett study area is less than 2 feet thick and is of a pebble-loam nature. Other evidence of glaciation includes the presence of several large boulders, less than 3 feet in diameter, which were derived from the Canadian Shield.

The glacial sediments indicate that glacial ice covered the study area during the Pleistocene Epoch. Horizontal sheet fracturing may have developed within the surficial bedrock formations, including the Cannonball Formation, as this glacial ice ablated. The fracturing of these sediments might promote secondary porosity and be responsible for the relatively large groundwater flow volumes encountered within the silts and clays beneath the Heskett site study area.

The soils across the proposed Heskett ash disposal area (Exhibit 5-F) are generally well developed. Edwards and Ableiter (1936) classified upland soils of the site as Hall series silt-loam. The soil is very silty with abundant clay and minor amounts of fine-grained sand. Internal drainage is generally good and surface drainage is sufficient. Most site soils are

approximately 1 foot thick with the upper 6 to 8 inches appearing very dark due to abundant organic matter. The soil becomes lighter in color 8 inches below the soil surface. All soils at the Heskett site are calcareous and freely effervesces with dilute hydrochloric acid.

5.2.2 Geohydrology

Exhibit 5-H illustrates the water table elevation contour of the Heskett site as of October 16, 1986. Because periodic well measurements over two years indicated relatively static potentiometric levels, the described elevation of the water table is considered representative. Water levels of all of the Heskett Site wells are given in Exhibit 5-G. Hydrographs of select piezometer nests appear in Exhibit 5-I.

The shallow groundwater beneath the proposed facility is flowing generally towards the northeast. Local variations do exist and can be attributed to the heterogeneous nature of the lithologies of the Cannonball Formation along with the undulating surface topography of the site. Surface topography appears to exert the most profound effect on groundwater flow with water table elevation mimicking the surface topography. As the groundwater approaches Rock Haven Creek it begins to take a more easterly path following the down-cut gradient of this creek into the Missouri River.

The groundwater flow beneath the base of a small draw, which extends to the north and slightly west from the south-central border of Section 10 to its intersection with the Rock Haven Creek, is nearly directly north. This groundwater flow is strongly influenced by the surficial topography which also dips toward the north. Industrial surface water holding ponds located on Amoco

refinery property south of the proposed site occasionally provides surface discharge into this draw. Running and ponded water resultant from these discharges as well as area ground surface runoff are frequently evident on MDU property just north of 43rd Street Northeast.

Morton County often experiences a drop in the elevation of the water table during the winter months due to a lack of recharge (Groenewold, et al., 1979 and 1983). Hydrographs (Exhibit 5-I) developed from two years of accumulated site potentiometric data indicate little apparent seasonal effect. An overall potentiometric level drop can be noted during the drought year of 1988. The data also indicated that the groundwater is flowing strongly downward. Thus, it can be expected that water will not be entering the proposed disposal pit from beneath the site.

Six subsurface lithologic intervals were sampled from in and near the proposed ash disposal site and laboratory tested to determine certain physical/chemical properties. Table 5-1 summarizes the results of cation exchange capacity and hydraulic conductivity testing for these samples (See Exhibit 5-K for greater detail). Data obtained from such lab permeability testing should be considered representative only of the point of sampling. Samples are often modified, in terms of hydraulic conductivity, during well drilling and sample collection. Minor subsurface fracturing might not be preserved in the laboratory. However, these data are useful in estimating flow rates through interstices in the subsurface geologic media and in situations where in-situ sediments will be modified by compaction to reduce secondary permeability.

Single-well response tests performed on select Heskett site wells (wells 11, 20, 31, 41 and 43) show greater in-situ permeabilities than the falling-head lab permeabilities of wells screened in the same sediments.

TABLE 5-1

Hydraulic Conductivities and Cation Exchange Capacities

Well Number	60	WS2	WS2
Sample Depth (ft)	20-40	29-30	61-62
Type of Sample	Bag	Core	Core
Permeability			
K @ 20°C (cm/sec)	2.0×10^{-7}	2.7×10^{-9}	3.6×10^{-8}
K @ 20°C (ft/min)	4.0×10^{-7}	5.4×10^{-9}	7.1×10^{-8}
Cation Exchange Cap. (meq/100 grams)	-----	92.2	12.0
Well Number	WS1	WS1	WS1
Sample Depth (ft)	20-21	25-26	30-31
Type of Sample	Core	Core	Core
Permeability			
K @ 20°C (cm/sec)	2.6×10^{-8}	1.5×10^{-8}	1.7×10^{-8}
K @ 20°C (ft/min)	5.2×10^{-8}	2.9×10^{-8}	3.4×10^{-8}
Cation Exchange Cap. (meq/100 grams)	71.8	12.3	74.2

WS - Refers to wells installed and sampled during a previous groundwater investigation around the coal ash waste pile at Heskett Station. This study was conducted by Water Supply, Incorporated.

These slug tests provide estimates of permeability over the screened 4-foot interval. Results, which appear in Table 5-2, show that wells 11 and 31 have the lowest permeabilities of the wells tested with values on the order of $K = 10^{-5}$ cm sec⁻¹. Higher conductivities were encountered in wells 20, 41 and 43 with values approximating $K = 10^{-4}$ cm sec⁻¹.

TABLE 5-2

Single Well Response Tests

<u>Well</u>	<u>Permeability</u>	<u>Screen Depth (MSL)</u>
11	3.78×10^{-5} cm sec ⁻¹	1642.81 - 1646.81
20	6.57×10^{-4} cm sec ⁻¹	1627.48 - 1631.48
31	2.84×10^{-5} cm sec ⁻¹	1635.58 - 1639.58
41	4.12×10^{-4} cm sec ⁻¹	1626.77 - 1630.77
43	5.07×10^{-4} cm sec ⁻¹	1650.14 - 1654.14

Reference: Freeze, R. A., and Cherry, J. A., 1979., Groundwater: Chapter 8.5, pgs. 339-342, Prentice-Hall Inc., Englewood Cliffs, NJ.

5.2.3 Hydrogeochemistry

Results of the site groundwater characterizations are shown in Exhibit 5-J. Analysis of samples collected in 1986 from wells 10-70 were conducted by the Mining and Mineral Resources Research Institute's Fuels Analysis Laboratory at the University of North Dakota. Supplemental sampling was conducted in 1988 by Minnesota Valley Testing Labs of Bismarck, ND. All samples were analyzed in accordance with EPA publication 600/4-79-020, "Methods for Chemical Analysis of Water and Wastes" (U.S. EPA, 1979).

The quality of the shallow (less than 120 feet below the land surface) groundwater at the proposed Heskett disposal site was found to be quite poor. Similar groundwater quality has been reported in other shallow wells within the Cannonball Formation (Ackerman, 1977 and 1980). Large quantities of salts and soluble mineral phases were deposited along with the sediments of the Cannonball. These materials dissociate as undersaturated interstitial groundwater flows through the formation. The ultimate quality of the water depends on the solubility of the geologic media and saturation condition of the groundwater which flows through it. Soluble constituents of the shallow groundwater at the Heskett site, as is characteristic of other Cannonball Formation wells, are high or very high relative to water in other aquifers in the area. Without pretreatment such groundwater is generally considered to be unfit for consumption by humans and livestock. Most of the local domestic wells tap either the underlying Hell Creek or the Fox Hills aquifers which possess waters with qualities far superior to that of the Cannonball.

An examination of the 1986 data appearing in Exhibit 5-J shows that the specific conductance and pH of wells sampled at the Heskett site are within the range of what has been reported as characteristic of the Cannonball Formation. Well 70 is located upgradient from known industrial influences and

can be considered representative of background groundwater quality at the site. Chemical analyses indicate that water within wells 60 and 70 have the highest specific conductance of all monitored wells.

Total dissolved solids (TDS) concentrations show the shallow groundwater at the Heskett site to be highly mineralized, ranging from 1,286 mg/L in well 30 to 14,917 mg/L in well 60. Wells screened within the Cannonball Formation commonly have TDS concentrations ranging from 1,000 to 3,000 mg/L (Ackerman, 1980).

Wells finished within the Cannonball Formation typically have sodium concentrations ranging from 500 mg/L to 1000 mg/L (Ackerman, 1977 and 1980). Sodium levels of wells 10, 12, 55 and 70 were well above these levels. Sulfate concentrations were highest in wells 44, 55, 60 and 70 with observed maximum occurring in well 60 (11,632 mg/L). Sodium, TDS and sulfate concentrations indicated that extremely saline pockets of groundwater exist at the southwestern (near wells 70, 10-13, and 60-62) and east-central (near wells 55 and 56) borders of the Heskett study area.

Both magnesium and calcium concentrations were relatively high and variable over the Heskett site study area. Well 44 contained the highest levels of these two constituents with 648 mg/L of calcium and 1,322 mg/L of magnesium. Heskett site water would be considered quite hard with actual values (expressed as CaCO_3) ranging from 222 mg/L in well 30 to 7,040 mg/L in well 60.

Chloride, potassium, iron, and fluoride concentrations were generally within the expected range of concentrations for wells finished within the Cannonball Formation. However, potassium was slightly elevated in wells 44 and 60 where it reached concentrations of 51 mg/L and 41 mg/L, respectively.

Nitrate concentrations were found to be erratic over the Heskett site. Wells 55 and 60 contain the highest nitrate levels with 154 mg/L and 170 mg/L, respectively. The drinking water standard (provided in Exhibit 5-J for reference purposes) for nitrate (NO_3^-) is currently set at 45 mg/L. The elevated nitrate concentrations in wells 50, 52, 55 and 60 would tend to indicate contamination from biological sources. Domestic sewage drainfields are known to exist near the center of the south border of the proposed disposal site in the vicinity of wells 43 and 44. It is believed that these sources contribute at least a portion of the observed elevated nitrate concentrations.

Selenium is a common naturally-occurring element in sediments, especially in shale and clay (Freeze and Cherry, 1979). Wells 55 and 60 had the highest concentrations with 0.368 mg/L and 0.195 mg/L, respectively. The levels observed in these two wells are above levels common to groundwater systems which contain shale and dissolved selenium. Indeed, these levels approach 100 times the concentration observed in groundwater taken elsewhere from the Cannonball Formation (Ackerman, 1977).

Molybdenum was detected at reduced concentrations in wells 10, 32, 54 and 70. Water Supply Incorporated (WS), in their previous groundwater investigation concerning the currently operational Heskett ash pile, noted concentrations of molybdenum in well WS4 similar to those observed in this study in wells 10, 54 and 70. Well WS4 was at the time noted for increasing molybdenum levels with the greatest concentration reaching 0.11 mg/L on September 11, 1985 (Armstrong and Schmid, 1986). Further groundwater monitoring has shown that after this finding molybdenum levels then dropped below analytical detection limits. Minimum detection levels have only occasionally been exceeded in the ensuing years. With this study's addition

of background monitoring wells upgradient from the current ash pile it can be determined that concentrations of molybdenum in well WS4 were within the background range of groundwater at the Heskett site. The elevated molybdenum concentrations as noted by W.S. are therefore not believed caused by the migration of leachate from the existing ash pile.

The 1988 groundwater data characterized only the uppermost zone of saturation near the proposed site. Its review indicated that the same general relationship between water quality and heavy metal parameters still exists after two years. A general diminishing of nitrate concentrations can be noted. Boron, an untested analyte in 1986, appeared in concentrations ranging from 1.0 ppm to 2.8 ppm (wells 45 and 70, respectively). Molybdenum was not detected. Wells 60 and 70 continued to exhibit extremely poor overall quality.

5.2.4 Chemical Attenuation of Leachate in Soil

A major concern in developing a waste disposal landfill is the potential generation and migration of toxic leachate. If highly mineralized subsurface leachate moves beyond the disposal site degradation of valuable groundwater supplies might occur. The leachate from the fly ash and bottom ash samples were generally comparable, in terms of overall quality, to the chemical composition of naturally-occurring groundwater at the Heskett site. An examination of Exhibits 2-A and 5-J shows that several of the major ions actually occurred at lower concentrations in the leachate than in the groundwater. Unit 1 bottom ash leachate appeared to be of much better quality than any groundwater sampled. Fly ash samples produced more highly mineralized (higher TDS) leachate than did bottom ash samples.

The overall quality of the existing groundwater at the proposed Heskett ash disposal site is brackish to saline with an average TDS concentration of 8,000 mg/L. The ash leachate produced using the modified EP toxicity test had an average TDS concentration of 6,500 mg/L. Consequently it may be expected that Heskett ash leachate will not significantly affect the TDS content of contaminated underlying groundwater even if soil buffer and attenuation mechanisms would be discounted.

The heavy metal analytes of primary concern in the leachate appear to be arsenic, cadmium, and lead. Sorptive, precipitation and co-precipitation processes are the major attenuation mechanisms that effect the concentration of these dissolved elements. Hassett and Groenewold (1986) studied trace element attenuation capabilities of coal-bearing Tertiary overburden deposits of central and western North Dakota. They found that the pH of a given leachate and the alkaline buffering capacity of the geologic media were the most critical variables in trace element attenuation. Western fly ash leachates are typically very alkaline with pH values approaching 13. In order to buffer such a solution either protons (H^+) must be added or hydroxyls (OH^-) must be removed. Oxides tend to ~~lose~~ lose protons in strongly alkaline solutions. This H^+ source, along with other acid producing reactions such as pyrite oxidation and organic decomposition, are the main alkaline buffering reactions. The protons that are liberated during these reactions will tend to neutralize the hydroxyl ions, thereby lowering the pH of the solution. The pH of the leachate will be buffered until it reaches equilibrium with the groundwater. In central and western North Dakota this equilibrium is generally attained at a pH value of between 7 and 9 (Groenewold et al., 1983; Koob and Groenewold, 1984).

Direct precipitation of cadmium and lead occur at pH values above 6.5. The solubility product of lead carbonate ($PbCO_3$) at 18°C is 3.3×10^{-14} . In groundwater systems which contain abundant carbonate lead will be precipitated as lead carbonate, thereby maintaining dissolved lead at low concentrations (Beaver, 1986 and 1987). The same type of reaction maintains cadmium at very low concentrations. Hassett and Groenewold (1986) found that cadmium was removed in excess of 99 percent during laboratory experiments with reduced and oxidized silts. Beaver (1986) confirmed the attenuation capabilities of similar geologic media during a coal ash field monitoring program near Center, North Dakota. He noted that several ions, including arsenic, cadmium and lead, were highly mobile under alkaline conditions within the ash itself. However, the alkaline leachate was buffered as soon as it came into contact with the surrounding clay and silt deposits. As the pH became lower the concentrations of cadmium and lead were greatly reduced (Beaver, 1986).

Arsenic attenuation is also controlled by solution pH. Laboratory experiments performed by Hassett and Groenewold (1986) have shown that arsenic, as As^{5+} , is significantly attenuated by the Tertiary sediments of western North Dakota. Arsenic appears to be most strongly attenuated in the pH range of 7-9. The mobility of selenium is similar to that of arsenic and the same attenuation processes control its concentration in groundwater systems. Sorptive processes appear responsible for arsenic attenuation in geologic media but the mechanisms of attenuation have not yet been well defined (Hassett and Groenewold, 1986). It does appear that cation and anion adsorption on clay particles and hydroxide coatings are important mechanisms in attenuating arsenic and other trace elements.

Hassett and Groenewold (1986) have shown that the clay, silt and sand sediments of central and western North Dakota have a strong capacity to buffer

highly alkaline leachates and attenuate trace elements such as arsenic and selenium. The ash pile at Heskett station has been subjected to continuous leaching for the past 30 years. When the quality of the shallow groundwater in the vicinity of the ash pile (data currently on file with the Health Department) was compared to the proposed disposal site it was apparent that upgradient groundwater quality was similar to or of poorer quality than the water near the ash pile. Consequently, groundwater sampling data around the existing ash pile may support the Hasset and Groenewold conclusions if buffered and attenuated leachate from the ash pile is infiltrating underlying groundwater.

EXHIBIT 5-A

TOPOGRAPHY AND BOREHOLE/CROSS-SECTION LOCATIONS

EXHIBIT 5-B

GEOHYDROLOGIC CROSS-SECTIONS

(PLATES A THROUGH H)

EXHIBIT 5-C

WELL COMPLETION REPORTS

Well Number: 10

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CCD

Elevation: Ground; 1722.06 ft. Casing top; 1725.01 ft.
Well Bottom; 1604.01 ft.

Completion: Date drilled; 8-12-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 120 ft.
Encountered water (below surface); 65 ft.
Geophysical log recorded

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.90-115.30 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 115.30-119.30 ft.
Elevation of interval; 1604.01-1608.01 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 114-120 ft.

Grout Seal: Depths (from ground); 0-114 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 51.97 ft. below top of casing
Elevation; 1673.04 ft.

Chemistry: Date; 8-21-86
pH; 7.75 Sp. cond; 11050 micromhos/cm
Temp; 8.9 oC

Well Number: 11

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CCD

Elevation: Ground; 1722.10 ft. Casing top; 1725.01 ft.
Well Bottom; 1642.81 ft.

Completion: Date drilled; 8-12-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 80 ft.
Encountered water (below surface); 65 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.90-78.20 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 78.20-82.20 ft.
Elevation of interval; 1642.81-1646.81 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 77-79 ft.

Grout Seal: Depths (from ground); 0-77 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 43.83 ft. below top of casing
Elevation; 1681.18 ft.

Chemistry: Date; 8-21-86
pH; 7.75 Sp. cond; 9840 micromhos/cm
Temp; 8.6 oC

Well Number: 12

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CCD

Elevation: Ground; 1721.88 ft. Casing top; 1724.90 ft.
Well Bottom; 1643.51 ft.

Completion: Date drilled; 8-12-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 80 ft.
Encountered water (below surface); 65 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +3.02-58.37 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 58.37-78.37 ft.
Elevation of interval; 1643.51-1663.51 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 57-79 ft.

Grout Seal: Depths (from ground); 0-57 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 43.60 ft. below top of casing
Elevation; 1681.30 ft.

Chemistry: Date; 8-21-86
pH; 7.60 Sp. cond; 11440 micromhos/cm
Temp; 8.5 oC

Well Number: 13

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CCD

Elevation: Ground; 1721.88 ft. Casing top; 1724.90 ft.
Well Bottom; 1681.88 ft.

Completion: Date drilled; 11-13-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry

Boring: Diameter; 5 5/8 in. Depth drilled; 40 ft.
Encountered water (below surface); ? ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +3.02-20.37 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC Depths (from
ground); 20.37-40.37 ft.
Elevation of interval; 1681.51-1701.51 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 19-41 ft.

Grout Seal: Depths (from ground); 0-19 ft.
Date sealed; 1-27-87

Additional Data:

Static Water Level: Date; 12-15-86
Depth; 30.09 ft. below top of casing
Elevation; 1694.81 ft.

Chemistry: Date; NA
pH; NA Sp. cond; NA
Temp; NA

Well Number: 20

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CAC

Elevation: Ground; 1707.04 ft. Casing top; 1709.48 ft.
Well Bottom; 1627.48 ft.

Completion: Date drilled; 8-12-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry

Boring: Diameter; 5 5/8 in. Depth drilled; 80 ft.
Encountered water (below surface); 45 ft.
Geophysical log recorded

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.44-75.56 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 75.56-79.56 ft.
Elevation of interval; 1627.48-1631.48 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 74-80 ft.

Grout Seal: Depths (from ground); 0-74 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 37.96 ft. below top of casing
Elevation; 1671.52 ft.

Chemistry: Date; 8-21-86
pH; 7.98 Sp. cond; 4970 micromhos/cm
Temp; 8.7 oC

Well Number: 21

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CAC

Elevation: Ground; 1707.22 ft. Casing top; 1709.40 ft.
Well Bottom; 1661.90 ft.

Completion: Date drilled; 8-12-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;

Boring: Diameter; 5 5/8 in. Depth drilled; 50 ft.
Encountered water (below surface); 45 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.66-21.32 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 21.32-45.32 ft.
Elevation of interval; 1661.90-1685.90 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 20-46 ft.

Grout Seal: Depths (from ground); 0-20 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 29.33 ft. below top of casing
Elevation; 1680.07 ft.

Chemistry: Date; 8-21-86
pH; 6.95 Sp. cond; 13920 micromhos/cm
Temp; 8.5 oC

Well Number: 30

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CBA

Elevation: Ground; 1715.55 ft. Casing top; 1717.64 ft.
Well Bottom; 1595.64 ft.

Completion: Date drilled; 8-12-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 120 ft.
Encountered water (below surface); 60 ft.
Geophysical log recorded

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.90-115.91 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 115.91-119.91 ft.
Elevation of interval; 1595.64-1599.64 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 114-120 ft.

Grout Seal: Depths (from ground); 0-114 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 49.41 ft. below top of casing
Elevation; 1668.23 ft.

Chemistry: Date; 8-21-86
pH; 7.95 Sp. cond; 1993 micromhos/cm
Temp; 8.6 oC

Well Number: 31

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CBA

Elevation: Ground; 1715.24 ft. Casing top; 1717.58 ft.
Well Bottom; 1635.58 ft.

Completion: Date drilled; 8-12-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 80 ft.
Encountered water (below surface); 60 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.34-75.66 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 75.66-79.66 ft.
Elevation of interval; 1635.58-1639.58 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 74-80 ft.

Grout Seal: Depths (from ground); 0-74 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 43.54 ft. below top of casing
Elevation; 1674.04 ft.

Chemistry: Date; 8-21-86
pH; 7.96 Sp. cond; 1993 micromhos/cm
Temp; 7.8 oC

Well Number: 32

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CBA

Elevation: Ground; 1715.34 ft. Casing top; 1717.79 ft.
Well Bottom; 1641.69 ft.

Completion: Date drilled; 8-12-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 80 ft.
Encountered water (below surface); 60 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.45-53.65 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 53.65-73.65 ft.
Elevation of interval; 1641.69-1661.69 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 52-75 ft.

Grout Seal: Depths (from ground); 0-52 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 42.03 ft. below top of casing
Elevation; 1675.76 ft.

Chemistry: Date; 8-21-86
pH; 7.22 Sp. cond; 3000 micromhos/cm
Temp; 8.0 oC

Well Number: 33

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CBA

Elevation: Ground; 1715.34 ft. Casing top; 1717.79 ft.
Well Bottom; 1672.79 ft.

Completion: Date drilled; 11-13-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry

Boring: Diameter; 5 5/8 in. Depth drilled; 45 ft.
Encountered water (below surface); ? ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.45-25.65 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 25.65-45.65 ft.
Elevation of interval; 1669.69-1689.69 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 24-45 ft.

Grout Seal: Depths (from ground); 0-24 ft.
Date sealed; 1-27-87

Additional Data:

Static Water Level: Date; 12-15-86
Depth; 40.68 ft. below top of casing
Elevation; 1677.11 ft.

Chemistry: Date; NA
pH; NA Sp. cond; NA
Temp; NA

Well Number: 40

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CDB

Elevation: Ground; 1708.02 ft. Casing top; 1710.15 ft.
Well Bottom; 1592.25 ft.

Completion: Date drilled; 8-13-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 120 ft.
Encountered water (below surface); 50 ft.
Geophysical log recorded

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.13-111.77 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 111.77-115.77 ft.
Elevation of interval; 1592.25-1596.25 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 110-117 ft.

Grout Seal: Depths (from ground); 0-117 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 63.72 ft. below top of casing
Elevation; 1646.43 ft.

Chemistry: Date; 8-21-86
pH; 7.58 Sp. cond; 6260 micromhos/cm
Temp; 8.2 oC

Well Number: 41

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CDB

Elevation: Ground; 1708.03 ft. Casing top; 1710.07 ft.
Well Bottom; 1626.77 ft.

Completion: Date drilled; 8-13-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 82 ft.
Encountered water (below surface); 50 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.04-77.26 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 77.26-81.26 ft.
Elevation of interval; 1626.77-1630.77 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 76-82 ft.

Grout Seal: Depths (from ground); 0-76 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 36.58 ft. below top of casing
Elevation; 1673.49 ft.

Chemistry: Date; 8-21-86
pH; 7.57 Sp. cond; 5480 micromhos/cm
Temp; 8.4 oC

Well Number: 42

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CDB

Elevation: Ground; 1708.12 ft. Casing top; 1710.31 ft.
Well Bottom; 1652.61 ft.

Completion: Date drilled; 8-13-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 60 ft.
Encountered water (below surface); 50 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.19-35.51 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 35.51-55.51 ft.
Elevation of interval; 1652.61-1672.61 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 34-56 ft.

Grout Seal: Depths (from ground); 0-34 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 32.88 ft. below top of casing
Elevation; 1677.43 ft.

Chemistry: Date; 8-21-86
pH; 7.22 Sp. cond; 5060 micromhos/cm
Temp; 8.6 oC

Well Number: 43

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CDD

Elevation: Ground; 1708.92 ft. Casing top; 1711.03 ft.
Well Bottom; 1650.14 ft.

Completion: Date drilled; 9-18-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry

Boring: Diameter; 5 5/8 in. Depth drilled; 60 ft.
Encountered water (below surface); 25 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.11-54.78 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 54.78-58.78 ft.
Elevation of interval; 1650.14-1654.14 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 53-59 ft.

Grout Seal: Depths (from ground); 0-53 ft.
Date sealed; 9-18-86

Additional Data:

Static Water Level: Date; 10-4-86
Depth; 25.85 ft. below top of casing
Elevation; 1685.18 ft.

Chemistry: Date; 10-4-86
pH; 6.70 Sp. cond; 6950 micromhos/cm
Temp; 8.5 oC

Well Number: 44

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CDD

Elevation: Ground; 1709.09 ft. Casing top; 1711.40 ft.
Well Bottom; 1685.88 ft.

Completion: Date drilled; 9-18-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry

Boring: Diameter; 5 5/8 in. Depth drilled; 25 ft.
Encountered water (below surface); 25 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.31-3.21 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 3.21-23.54 ft.
Elevation of interval; 1685.88-1705.88 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 2.5-24.0 ft.

Grout Seal: Depths (from ground); 0-2.5 ft.
Date sealed; 9-18-86

Additional Data:

Static Water Level: Date; 10-4-86
Depth; 21.92 ft. below top of casing
Elevation; 1689.48 ft.

Chemistry: Date; 10-4-86
pH; 6.72 Sp. cond; 10270 micromhos/cm
Temp; 9.1 oC

Well Number: 45

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CDB

Elevation: Ground; 1708.12 ft. Casing top; 1710.31 ft.
Well Bottom; 1668.12 ft.

Completion: Date drilled; 11-13-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;

Boring: Diameter; 5 5/8 in. Depth drilled; 40 ft.
Encountered water (below surface); ? ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.19-20.51 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 20.51-40.51 ft.
Elevation of interval; 1667.61-1687.61 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 19-41 ft.

Grout Seal: Depths (from ground); 0-19 ft.
Date sealed; 1-27-86

Additional Data:

Static Water Level: Date; 12-15-86
Depth; 28,71 ft. below top of casing
Elevation; 1681.60 ft.

Chemistry: Date; NA
pH; NA Sp. cond; NA
Temp; NA

Well Number: 50

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CAD

Elevation: Ground; 1674.58 ft. Casing top; 1677.01 ft.
Well Bottom; 1647.51 ft.

Completion: Date drilled; 8-13-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 30 ft.
Encountered water (below surface); 17 ft.
Geophysical log recorded

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.43-7.07 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 7.07-27.07 ft.
Elevation of interval; 1647.51-1667.51 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 6-29 ft.

Grout Seal: Depths (from ground); 0-6 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 5.45 ft. below top of casing
Elevation; 1671.56 ft.

Chemistry: Date; 8-21-86
pH; 7.56 Sp. cond; 6480 micromhos/cm
Temp; 10.8 oC

Well Number: 51

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CAD

Elevation: Ground; 1674.47 ft. Casing top; 1676.70 ft.
Well Bottom; 1637.33 ft.

Completion: Date drilled; 9-18-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 40 ft.
Encountered water (below surface); 18 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.23-32.14 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 32.14-37.14 ft.
Elevation of interval; 1637.33-1642.33 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 31-38 ft.

Grout Seal: Depths (from ground); 0-31 ft.
Date sealed; 9-18-86

Additional Data:

Static Water Level: Date; 10-4-86
Depth; 5.77 ft. below top of casing
Elevation; 1670.93 ft.

Chemistry: Date; 10-4-86
pH; 7.46 Sp. cond; 3700 micromhos/cm
Temp; 8.2 oC

Well Number: 52

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CAD

Elevation: Ground; 1674.45 ft. Casing top; 1676.71 ft.
Well Bottom; 1658.01 ft.

Completion: Date drilled; 9-18-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 20 ft.
Encountered water (below surface); 18 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.26-6.44 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 6.44-16.44 ft.
Elevation of interval; 1658.01-1668.01 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 5-18 ft.

Grout Seal: Depths (from ground); 0-5 ft.
Date sealed; 9-18-86

Additional Data:

Static Water Level: Date; 10-4-86
Depth; 4.13 ft. below top of casing
Elevation; 1672.58 ft.

Chemistry: Date; 10-4-86
pH; 7.29 Sp. cond; 6300 micromhos/cm
Temp; 9.4 oC

Well Number: 53

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10DCC

Elevation: Ground; 1685.71 ft. Casing top; 1688.17 ft.
Well Bottom; 1665.70 ft.

Completion: Date drilled; 9-18-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry

Boring: Diameter; 5 5/8 in. Depth drilled; 21 ft.
Encountered water (below surface); 15 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.46-5.01 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 5.01-20.01 ft.
Elevation of interval; 1665.70-1680.70 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 4-21 ft.

Grout Seal: Depths (from ground); 0-4 ft.
Date sealed; 9-18-86

Additional Data:

Static Water Level: Date; 10-4-86
Depth; 6.30 ft. below top of casing
Elevation; 1681.87 ft.

Chemistry: Date; 10-4-86
pH; NA Sp. cond; NA micromhos/cm
Temp; NA oC

Well Number: 54

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10DCC

Elevation: Ground; 1685.71 ft. Casing top; 1688.10 ft.
Well Bottom; 1633.11 ft.

Completion: Date drilled; 9-18-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry

Boring: Diameter; 5 5/8 in. Depth drilled; 60 ft.
Encountered water (below surface); 15 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.39-47.60 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 47.60-52.60 ft.
Elevation of interval; 1633.11-1638.11 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 46-54 ft.

Grout Seal: Depths (from ground); 0-46 ft.
Date sealed; 9-18-86

Additional Data:

Static Water Level: Date; 10-4-86
Depth; 15.16 ft. below top of casing
Elevation; 1672.94 ft.

Chemistry: Date; 10-4-86
pH; 9.55 Sp. cond; 1100 micromhos/cm
Temp; 9.8 oC

Well Number: 55

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10DCA

Elevation: Ground; 1693.86 ft. Casing top; 1696.10 ft.
Well Bottom; 1636.95 ft.

Completion: Date drilled; 9-18-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry

Boring: Diameter; 5 5/8 in. Depth drilled; 60 ft.
Encountered water (below surface); 45 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.24-31.91 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 31.91-56.91 ft.
Elevation of interval; 1636.95-1661.95 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 30-58 ft.

Grout Seal: Depths (from ground); 0-30 ft.
Date sealed; 9-18-86

Additional Data:

Static Water Level: Date; 10-4-86
Depth; 29.46 ft. below top of casing
Elevation; 1666.64 ft.

Chemistry: Date; 10-4-86
pH; 6.81 Sp. cond; 10840 micromhos/cm
Temp; 8.5 oC

Well Number: 56

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-80-10DCA

Elevation: Ground; 1693.86 ft. Casing top; 1696.42 ft.
Well Bottom; 1597.99 ft.

Completion: Date drilled; 9-18-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry

Boring: Diameter; 5 5/8 in. Depth drilled; 100 ft.
Encountered water (below surface); 45 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.56-91.87 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 91.87-96.87 ft.
Elevation of interval; 1597.99-1601.99 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 90-98 ft.

Grout Seal: Depths (from ground); 0-90 ft.
Date sealed; 9-18-86

Additional Data:

Static Water Level: Date; 10-4-86
Depth; 42.03 ft. below top of casing
Elevation; 1654.39 ft.

Chemistry: Date; 10-4-86
pH; 8.44 Sp. cond; 4160 micromhos/cm
Temp; 8.3 oC

Well Number: 60

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-18-10CDB

Elevation: Ground; 1714.23 ft. Casing top; 1716.42 ft.
Well Bottom; 1662.02 ft.

Completion: Date drilled; 8-13-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 60 ft.
Encountered water (below surface); 45 ft.
Geophysical log recorded

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.19-22.21 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 22.21-52.21 ft.
Elevation of interval; 1662.02-1692.02 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 21-54 ft.

Grout Seal: Depths (from ground); 0-21 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 31.01 ft. below top of casing
Elevation; 1685.41 ft.

Chemistry: Date; 8-21-86
pH; 6.94 Sp. cond; 15760 micromhos/cm
Temp; 8.5 oC

Well Number: 61

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CDA

Elevation: Ground; 1714.23 ft. Casing top; 1716.53 ft.
Well Bottom; 1670.89 ft.

Completion: Date drilled; 9-18-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry

Boring: Diameter; 5 5/8 in. Depth drilled; 46 ft.
Encountered water (below surface); 37 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.30-13.34 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 13.34-43.34 ft.
Elevation of interval; 1670.89-1700.89 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 12-45 ft.

Grout Seal: Depths (from ground); 0-12 ft.
Date sealed; 9-18-86

Additional Data:

Static Water Level: Date; 10-4-86
Depth; 32.58 ft. below top of casing
Elevation; 1683.95 ft.

Chemistry: Date; 10-4-86
pH; 6.83 Sp. cond; 12750 micromhos/cm
Temp; 8.4 oC

Well Number: 62

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CDB

Elevation: Ground; 1714.32 ft. Casing top; 1716.67 ft.
Well Bottom; 1681.40 ft.

Completion: Date drilled; 9-18-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry

Boring: Diameter; 5 5/8 in. Depth drilled; 35 ft.
Encountered water (below surface); 35 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.35-12.92 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 12.92-32.91 ft.
Elevation of interval; 1681.40-1701.40 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 11-34 ft.

Grout Seal: Depths (from ground); 0-11 ft.
Date sealed; 9-18-86

Additional Data:

Static Water Level: Date; 10-4-86
Depth; 32.74 ft. below top of casing
Elevation; 1683.93 ft.

Chemistry: Date; 10-4-86
pH; 6.71 Sp. cond; 13170 micromhos/cm
Temp; 9.3 oC

Well Number: 70

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-16ABA

Elevation: Ground; 1733.18 ft. Casing top; 1735.67 ft.
Well Bottom; 1634.57 ft.

Completion: Date drilled; 8-13-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 102 ft.
Encountered water (below surface); 45 ft.
Geophysical log recorded

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.49-94.61 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 94.61-98.61 ft.
Elevation of interval; 1634.57-1638.57 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 93-99 ft.

Grout Seal: Depths (from ground); 0-93 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 54.20 ft. below top of casing
Elevation; 1681.47 ft.

Chemistry: Date; 8-21-86
pH; 7.85 Sp. cond; 13000 micromhos/cm
Temp; 10.1 oC

Well Number: (WS1)

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-DBB

Elevation: Ground; 1679.61 ft. Casing top; 1681.71 ft.
Well Bottom; 1606.73 ft.
Repaired casing top (1-13-86); 1683.67 ft.

Completion: Date drilled; 9-22-81
Driller; Water Supply, Inc.
Method of drilling; NA

Boring: Diameter; NA in. Depth drilled; 73 ft.
Encountered water (below surface); NA ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.7-40, 45-73 ft.
(as of 1-13-87); +4.7-40, 45-73 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 40-45 ft.
Elevation of interval; 1634.61-1639.61 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 37-47 ft.

Grout Seal: Depths (from ground); 0-37 ft.
Date sealed; NA

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 24.61 ft. below top of casing
Elevation; 1657.10 ft.

Chemistry: Date; 8-21-86
pH; 7.47 Sp. cond; 1899 micromhos/cm
Temp 7.0 oC

Well Number: (WS1A)

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-DBB

Elevation: Ground; 1679.10 ft. Casing top; 1682.23 ft.
Well Bottom; 1657.10 ft.

Completion: Date drilled; 8-5-85
Driller; Water Supply, Inc.
Method of drilling; NA

Boring: Diameter; NA in. Depth drilled; 23 ft.
Encountered water (below surface); NA ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +3.2-17 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 17-22 ft.
Elevation of interval; 1657.10-1662.10 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 15-23 ft.

Grout Seal: Depths (from ground); 0-15 ft.
Date sealed; NA

Additional Data:

Static Water Level: Date; 8-21-86
Depth; DRY ft. below top of casing
Elevation; ft.

Chemistry: Date: 8-21-86
pH; NA Sp. cond; NA micromhos/cm
Temp; NA oC

Well Number: (WS1B)

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10DBB

Elevation: Ground; 1678.80 ft. Casing top; 1682.07 ft.
Well Bottom; 1648.80 ft.

Completion: Date drilled; 8-6-85
Driller; Water Supply, Inc.
Method of drilling; NA

Boring: Diameter; NA in. Depth drilled; 30 ft.
Encountered water (below surface); NA ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +3.3-25 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 25-30 ft.
Elevation of interval; 1648.80-1653.80 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 23-30 ft.

Grout Seal: Depths (from ground); 0-22 ft.
Date sealed; NA

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 24.48 ft. below top of casing
Elevation; 1657.59 ft.

Chemistry: Date; 8-21-86
pH; 7.07 Sp. cond; 3940 micromhos/cm
Temp; 8.5 oC

Well Number: (WS2)

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10DCC

Elevation: Ground; 1696.00 ft. Casing top; 1698.64 ft.
Well Bottom; 1607.00 ft.

Completion: Date drilled; 9-23-81
Driller; Water Supply, Inc.
Method of drilling; NA

Boring: Diameter; NA in. Depth drilled; 90 ft.
Encountered water (below surface); NA ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +3-56, 61-89 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 56-61 ft.
Elevation of interval; 1635.00-1640.00 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 53-62 ft.

Grout Seal: Depths (from ground); 0-52 ft.
Date sealed; NA

Additional Data:

Static Water Level: Date; 10-4-86
Depth; 33.86 ft. below top of casing
Elevation; 1664.78 ft.

Chemistry: Date; 8-21-86
pH; 7.04 Sp. cond; 3760 micromhos/cm
Temp; 8.6 oC

Well Number: (WS3)

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10DBA

Elevation: Ground; 1658.00 ft. Casing top; 1661.00 ft.
Well Bottom; 1608.00 ft.

Completion: Date drilled; 9-21-81
Driller; Water Supply, Inc.
Method of drilling; NA

Boring: Diameter; NA in. Depth drilled; 50 ft.
Encountered water (below surface); NA ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +3-25, 30-50 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 25-30 ft.
Elevation of interval; 1628.00-1633.00 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 24-32 ft.

Grout Seal: Depths (from ground); 0-23 ft.
Date sealed; NA

Additional Data:

Static Water Level: Date; 9-4-86
Depth; 14.67 ft. below top of casing
Elevation; 1646.33 ft.

Chemistry: Date; NA
pH; NA Sp. cond; NA micromhos/cm
Temp; NA oC

Well Number: (WS3A)

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10DBA

Elevation: Ground; 1657.70 ft. Casing top; 1660.81 ft.
Well Bottom; 1645.31 ft.

Completion: Date drilled; 8-5-85
Driller; Water Supply, Inc.
Method of drilling; NA

Boring: Diameter; NA in. Depth drilled; 13 ft.
Encountered water (below surface); NA ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +3.1-7.5 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 7.5-12.5 ft.
Elevation of interval; 1645.31-1650.31 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 6-13 ft.

Grout Seal: Depths (from ground); 0-6 ft.
Date sealed; NA

Additional Data:

Static Water Level: Date; 10-4-86
Depth; 8.37 ft. below top of casing
Elevation; 1652.44 ft.

Chemistry: Date; NA
pH; NA Sp. cond; NA micromhos/cm
Temp; NA oC

Well Number: (WS4)

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10DBA

Elevation: Ground; 1659.61 ft. Casing top; 1662.61 ft.
Well Bottom; 1607.60 ft.

Completion: Date drilled; 9-24-81
Driller; Water Supply, Inc.
Method of drilling; NA

Boring: Diameter; NA in. Depth drilled; 52 ft.
Encountered water (below surface); NA ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +3-30, 35-52 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 30-35 ft.
Elevation of interval; 1624.60-1629.60 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 27-36 ft.

Grout Seal: Depths (from ground); 0-26 ft.
Date sealed; NA

Additional Data:

Static Water Level: Date; 9-4-86
Depth; 19.62 ft. below top of casing
Elevation; 1642.99 ft.

Chemistry: Date; NA
pH; NA Sp. cond; NA micromhos/cm
Temp; NA oC

Well Number: (WS4A)

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10DBA

Elevation: Ground; 1659.49 ft. Casing top; 1662.49 ft.
Well Bottom; 1641.50 ft.

Completion: Date drilled; 9-24-81
Driller; Water Supply, Inc.
Method of drilling; NA

Boring: Diameter; NA in. Depth drilled; 18 ft.
Encountered water (below surface); NA ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +3-13 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 13-18 ft.
Elevation of interval; 1641.50-1646.50 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 11-18 ft.

Grout Seal: Depths (from ground); 0-11 ft.
Date sealed; NA

Additional Data:

Static Water Level: Date; 9-4-86
Depth; 17.29 ft. below top of casing
Elevation; 1645.20 ft.

Chemistry: Date; NA
pH; NA Sp. cond; NA micromhos/cm
Temp; NA oC

Well Number: (WS4B)

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10DBA

Elevation: Ground; 1659.75 ft. Casing top; 1662.75 ft.
Well Bottom; 1635.80 ft.

Completion: Date drilled; 8-5-85
Driller; Water Supply, Inc.
Method of drilling; NA

Boring: Diameter; NA in. Depth drilled; 25 ft.
Encountered water (below surface); NA ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +3.1-19.0 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 19-24 ft.
Elevation of interval; 1635.80-1640.80 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 18-25 ft.

Grout Seal: Depths (from ground); 0-18 ft.
Date sealed; NA

Additional Data:

Static Water Level: Date; 9-4-86
Depth; 17.39 ft. below top of casing
Elevation; 1645.36 ft.

Chemistry: Date; NA
pH; NA Sp. cond; NA micromhos/cm
Temp; NA oC

EXHIBIT 5-D

GEOPHYSICAL LOGS

EXHIBIT 5-E

LITHOLOGIC LOGS

Wells 10, 11, 12 and 13

- 0-1 Top soil, silty, clayey, sandy, brown, calcareous; with some limestone pebbles.
- 1-11 Silt, clayey, brownish-tan, slightly indurated, very dry, calcareous; with thin coarse-grained, clean silt lenses and a few small (less than .5 in.) iron oxide concretions. Abundant small gypsum crystals (less than .13 in. long). Some small, black flakes of organic plant material. Cannonball-Ludlow Formations.
- 11-14 Silt, as above, with some (less than 20%) very fine- to fine-grained sand interspersed.
- 14-30 Silt, as above, clayey, less sand than above interval, oxidized; with very fine-grained silty sand lenses and very few gypsum crystals.
- 30-41 Silt, very clayey, with some (less than 20%) very fine-grained sand interspersed, steel-gray (color change), moderately indurated; with fewer small gypsum crystals than above intervals.
- 41-59 Silt, as above, very clayey, with some (less than 20%) fine- to medium-grained sand interspersed in a silt and clay matrix.
- 59-65 Silt, as above, with abundant (more than 20%) fine- to medium-grained sand interspersed.
- 65-81 Silt, clayey, steel-gray to bluish, moderately indurated; with thin coarse-grained silt to very fine-grained sand lenses in an otherwise fine silt to clay matrix.
- 81-84 Clay, silty, steel-gray to bluish, moderately indurated, dense.
- 84-91 Siltstone, sandy, clayey, steel-gray to bluish, slightly indurated; with small fine-grained sand lenses and abundant (more than 20%) sand interspersed in the matrix.
- 91-110 Silt, clayey, bluish-gray, moderately indurated; with thin (less than 1 foot) mudstone lenses.
- 110-120 Silt, very clayey, steel-gray to bluish, moderately indurated, very dense. Cannonball-Ludlow Formations.

Wells 20 and 21

- 0-1 Top soil, silty, sandy, clayey, dark-brown, calcareous; with some limestone and granite pebbles.
- 1-21 Silt, clayey, with minor amounts (less than 10%) of very fine-grained sand interspersed, brownish-tan, slightly indurated, calcareous, oxidized; with small iron oxide concretions and abundant small gypsum crystals.
Cannonball-Ludlow Formations.
- 21-26 Silt, as above, steel-gray (color change).
- 26-49 Silt, clayey, with some (less than 20%) very fine- to medium-grained sand interspersed, steel-gray to bluish, slightly indurated; with very few small gypsum crystals and some thin (less than 1 foot) siltstone lenses.
- 49-53 Silt, as above, with abundant (more than 20%) fine- to medium-grained sand interspersed.
- 53-63 Silt, as above, clayey, less sand, with thin (less than 1 foot) siltstone to mudstone lenses.
- 63-80 Silt, very clayey, steel-gray to bluish, moderately indurated, very dense.
Cannonball-Ludlow Formations.

Wells 30, 31, 32 and 33

- 0-1 Top soil, silty, sandy, brownish, calcareous; with some granite and limestone pebbles.
- 1-2 Pebble-loam (glacial till), silty, sandy, clayey, yellowish-brown, dry, calcareous.
- 2-31 Silt, clayey, with minor amounts (less than 10%) of very fine-grained sand interspersed, brownish-tan, slightly indurated, calcareous, oxidized; with small iron oxide concretions. Some small, black flakes organic plant material.
Cannonball-Ludlow Formations.
- 31-44 Silt, clayey, steel-gray (color change), slightly indurated, calcareous; with small iron oxide concretions, thin coarse silt lenses, small gypsum crystals and gray to reddish-brown mottling.

- 44-61 Silt, as above, with some (less than 20%) fine- to medium-grained sand interspersed.
- 61-65 Silt, as above, with abundant (more than 20%) fine- to medium-grained sand interspersed, dense.
- 65-76 Silt, as above, clayey, less sand, some thin (less than 1 foot) lenses of siltstone to mudstone.
- 76-80 Siltstone, sandy, clayey, steel-gray to bluish, slightly indurated; with small fine-grained sand lenses and abundant (more than 20%) fine-grained sand interspersed in the matrix.
- 80-92 Silt, clayey, steel-gray to bluish, moderately indurated, with some (less than 20%) very fine- to fine grained sand interspersed.
- 92-120 Silt, very clayey, steel-gray to bluish, moderately indurated, very dense.
Cannonball-Ludlow Formations.

Well 40

- 0-1 Top soil, sandy, silty, brownish-tan, calcareous; with some granite and limestone pebbles.
- 1-5 Pebble-loam (glacial till), sandy, silty, with detrital lignite and organic matter, yellowish-brown, very dry, calcareous.
- 5-22 Sand, very fine- to medium-grained, unconsolidated, with thin lenses of clay and detrital lignite, brownish-yellow, calcareous.
- 22-40 Silt, clayey, with minor amounts (less than 10%) very fine-grained sand interspersed, brownish-tan, slightly indurated, calcareous, oxidized; with small iron oxide concretions and small gypsum crystals; Cannonball-Ludlow Formations.
- 40-51 Silt, clayey, with minor amounts (less than 10%) of very fine-grained sand interspersed, steel-gray (color change), moderately indurated; with some reddish-brown mottling and some very thin (less than 6 inches) mudstone lenses.
- 51-58 Silt, as above, with abundant (more than 20%) fine-grained sand and thin silty-clay lenses.

- 58-62 Siltstone, sandy, clayey, steel-gray to bluish, moderately indurated; with small fine-grained sand lenses and abundant (more than 20%) sand interspersed in the matrix.
- 62-70 Silt, clayey, with some (less than 20%) fine- to medium-grained sand interspersed, steel-gray to bluish, moderately indurated; with thin (less than 2 feet) sandy lenses.
- 70-80 Silt, as above, very clayey, some (less than 10%) fine-grained sand interspersed; less sand than above interval.
- 80-120 Silt, as above, dark-steel-gray.
Cannonball-Ludlow Formations.

Wells 41, 42 and 43

- 0-1 Top soil, sandy, silty, dark-brown, calcareous; with some granite and limestone pebbles.
- 1-4 Pebble-loam (glacial till), sandy, silty, clayey, yellowish-brown, very dry, calcareous.
- 4-40 Silt, clayey, with some (less than 20%) very fine-grained sand interspersed, brownish-tan, unconsolidated, noncompacted, calcareous to 25 feet, oxidized; with small iron oxide concretions and abundant small gypsum crystals.
Cannonball-Ludlow Formations.
- 40-51 Silt, clayey, with minor amounts (less than 10%) of very fine-grained sand interspersed, steel-gray (color change), moderately indurated; with some reddish-brown mottling and some very thin (less than 6 inches) mudstone lenses.
- 51-58 Silt, as above, with abundant (more than 20%) fine-grained sand and thin silty-clay lenses.
- 58-62 Siltstone, sandy, clayey, steel-gray to bluish, moderately indurated; with small fine-grained sand lenses and abundant (more than 20%) sand interspersed in the matrix.
- 62-70 Silt, clayey, with some (less than 20%) fine- to medium-grained sand interspersed, steel-gray to bluish, moderately indurated; with thin (less than 2 feet) sandy lenses.

30-40 Silt, as above, very clayey, less sand than above interval, dark-steel-gray.
Cannonball-Ludlow Formations.

Wells 53 and 54

- 0-4 Top soil, clayey, silty, very dark-brown, wet, sticky.
- 4-15 Clay, silty, with some (less than 20%) fine- to medium-grained sand interspersed, brownish-tan, slightly indurated, dry, calcareous; with small iron oxide concretions, small gypsum crystals and occasional reddish-brown mottling;
Cannonball-Ludlow Formations.
- 15-20 Sand, very fine-grained to medium-grained, silty, clayey, unconsolidated, yellowish-brown, oxidized.
- 20-30 Silt, clayey, with some (less than 20%) fine-grained sand interspersed, steel-gray (color change), slightly indurated; with clay and sand lenses, some small concretions and some small gypsum crystals.
- 30-45 Silt, as above, very clayey.
- 45-60 Silt, as above, clayey, brownish-gray, moderately indurated, some reddish-brown mottling.
Cannonball-Ludlow Formations.

Wells 55 and 56

- 0-5 Sandy-loam (glacial), with fine- to medium-grained sand, silty, calcareous; with small granite and limestone pebbles.
- 5-26 Clay, silty, with minor amounts (less than 10%) of very fine-grained sand, dark-brownish-tan, moderately indurated, brittle, very dry, calcareous; with small iron oxide concretions, small gypsum crystals and occasional thin sandstone laminae. Some small, black flakes of organic plant material.
Cannonball-Ludlow Formations.
- 26-35 Clay, as above, very silty, sandy, brownish-tan, oxidized.

- 35-40 Silt, clayey, with some (less than 20%) very fine- to fine-grained sand interspersed, steel-gray (color change) moderately indurated; with small gypsum crystals and occasional clay lenses.
- 40-60 Silt, as above, with minor amounts (less than 10%) of fine-grained sand interspersed.
- 60-85 Silt, as above, clayey, less sand than above interval.
- 85-100 Silt, as above, very clayey, with minor amounts (less than 10%) of sand interspersed, light-gray. Cannonball-Ludlow Formations.

Wells 60, 61 and 62

- 0-2 Top soil, silty, clayey, dark-brown to tanish-brown, calcareous.
- 2-25 Silt, very clayey, with some minor amounts (less than 10%) of very fine- to fine-grained sand interspersed, brownish-tan, slightly indurated, dry, calcareous; with abundant small gypsum crystals and thin silt and sand lenses; Cannonball-Ludlow Formations.
- 25-29 Silt, as above, with abundant (more than 20%) fine- to medium-grained sand interspersed.
- 29-36 Silt, as above, clayey, less sand than above interval, dark-brownish-tan, oxidized.
- 36-60 Silt, very clayey, with some (less than 20%) very fine-grained sand interspersed, steel-gray (color change), moderately indurated; with thin (less than 1 foot) sandy-silt lenses. Cannonball-Ludlow Formations.

Well 70 0-2 Pebble-loam (glacial till), clayey, sandy, yellowish-brown, unconsolidated, damp, calcareous.

- 2-21 Silty, clayey, with some (less than 20%) fine-grained sand interspersed, brownish-tan, moderately indurated, very dry, calcareous, oxidized; with small iron oxide concretions and abundant small gypsum crystals. Cannonball-Ludlow Formations.

- 21-24 Shale, silty, steel- to dark-gray (color change), indurated, fissile, very dry; with occasional thin silt and sand lenses.
- 24-31 Silt, clayey, with abundant (more than 30%) sand, steel-gray, moderately indurated.
- 31-62 Silt, clayey, with some (less than 20%) very fine- to fine- grained sand interspersed, steel-gray, moderately indurated; with some small gypsum crystals and small iron oxide concretions.
- 62-76 Silt, as above, with some (less than 20%) fine-grained sand interspersed.
- 76-82 Silt, as above, with abundant (more than 20%) fine- to medium-grained sand.
- 82-100 Silt, as above, clayey, with some (less than 20%) fine-grained sand interspersed, dark-gray.
Cannonball-Ludlow Formations.

EXHIBIT 5-F

SITE SOILS CLASSIFICATION MAP

EXHIBIT 5-G

WATER LEVEL DATA

HESKETT SWL INFORMATION

WELL DATA

WELL NO.	TOP OF CASE	GROUND SURFACE	SCREENED	INTERVAL	CASING HEIGHT
10	1725.01	1722.06	1604.01	to 1608.01	2.95
11	1725.01	1722.10	1642.81	to 1646.81	2.91
12	1724.90	1721.88	1643.51	to 1663.51	3.02
13	1724.98	1721.80	1681.51	to 1701.51	3.18
20	1709.48	1707.04	1627.48	to 1631.48	2.44
21	1709.40	1707.22	1661.90	to 1685.90	2.18
30	1717.64	1715.55	1595.64	to 1599.64	2.09
31	1717.58	1715.24	1635.58	to 1639.58	2.34
32	1717.79	1715.34	1641.69	to 1661.69	2.45
33	1717.91	1715.48	1669.69	to 1689.69	2.43
40	1710.15	1708.02	1592.25	to 1596.25	2.13
41	1710.07	1708.03	1626.77	to 1630.77	2.04
42	1710.31	1708.12	1652.61	to 1672.61	2.19
43	1711.03	1708.92	1650.14	to 1654.14	2.11
44	1711.40	1709.09	1685.88	to 1705.88	2.31
45	1710.17	1708.34	1667.61	to 1687.61	1.83
50	1677.01	1674.58	1647.51	to 1667.51	2.43
51	1676.70	1674.47	1637.33	to 1642.33	2.23
52	1676.71	1674.45	1658.01	to 1668.01	2.26
53	1688.17	1685.71	1665.70	to 1680.70	2.46
54	1688.10	1685.71	1633.11	to 1638.11	2.39
55	1696.10	1693.86	1636.95	to 1661.95	2.24
56	1696.42	1693.86	1597.99	to 1601.99	2.56
60	1716.42	1714.23	1662.02	to 1692.02	2.19
61	1716.53	1714.23	1670.89	to 1700.89	2.30
62	1716.67	1714.32	1681.40	to 1701.40	2.35
70	1735.67	1733.18	1634.57	to 1638.57	2.49
WS2	1698.64	1696.00	1635.00	to 1640.00	2.64
WS1	1681.71	1679.61	1634.61	to 1639.61	2.10
WS1	1683.67	as of 1-3-87			4.06
WS1A	1682.23	1679.10	1657.10	to 1662.10	3.13
WS1B	1682.07	1678.80	1648.80	to 1653.80	3.27
WS4	1662.61	1659.61	1624.60	to 1629.60	3.00
WS4A	1662.49	1659.49	1641.50	to 1646.50	3.00
WS4B	1662.75	1659.75	1635.80	to 1640.80	3.00
WS3	1661.00	1658.00	1628.00	to 1633.00	3.00
WS3A	1660.81	1657.70	1645.31	to 1650.31	3.11

CASING ON WELL WS1 WAS REPAIRED IN JANUARY, 1987

ALL VALUES ARE IN FEET ABOVE MEAN SEA LEVEL

SWL-TOP = STATIC WATER LEVEL (in feet) FROM TOP OF CASING
 SWL-MSL = STATIC WATER LEVEL (in feet) AT MEAN SEA LEVEL
 SWL-BLS = STATIC WATER LEVEL (in feet) BELOW LAND SURFACE

HESKETT SWL INFORMATION

WELL NO.	DATE	SWL-TOP	SWL-MSL	SWL-BLS
10	9-11-86	51.64	1673.37	48.69
	10-16-86	53.32	1671.69	50.37
	11-21-86	53.58	1671.43	50.63
	1-13-87	53.71	1671.30	50.76
	3-6-87	53.61	1671.40	50.66
	4-21-87	53.45	1671.56	50.50
	6-3-87	53.48	1671.53	50.53
	5-11-88	54.79	1670.22	51.84
	9-12-88	55.05	1669.96	52.10
1-4-89	56.33	1668.68	53.38	
11	9-11-86	42.42	1682.59	39.51
	10-16-86	41.47	1683.54	38.56
	11-21-86	40.88	1684.13	37.97
	1-13-87	40.72	1684.29	37.81
	3-6-87	40.59	1684.42	37.68
	4-21-87	40.72	1684.29	37.81
	6-3-87	40.65	1684.36	37.74
	5-11-88	42.62	1682.39	39.71
	9-12-88	43.67	1681.34	40.76
1-4-89	44.10	1680.91	41.19	
12	9-11-86	42.42	1682.48	39.40
	10-16-86	40.55	1684.35	37.53
	11-21-86	40.00	1684.90	36.98
	1-13-87	39.86	1685.04	36.84
	3-6-87	39.77	1685.13	36.75
	4-21-87	39.83	1685.07	36.81
	6-3-87	39.90	1685.00	36.88
	5-11-88	41.90	1683.00	38.88
	9-12-88	43.21	1681.69	40.19
1-4-89	43.37	1681.53	40.35	
13	12-15-86	30.09	1694.89	26.91
	1-13-87	29.99	1694.99	26.81
	3-6-87	30.15	1694.83	26.97
	4-21-87	29.92	1695.06	26.74
	6-3-87	29.86	1695.12	26.68
	5-11-88	31.27	1693.71	28.09
	9-12-88	31.53	1693.45	28.35
	1-4-89	31.69	1693.29	28.51

HESKETT SWL INFORMATION

WELL NO.	DATE	SWL-TOP	SWL-MSL	SWL-BLS
20	9-11-86	37.17	1672.31	34.73
	10-16-86	36.85	1672.63	34.41
	11-21-86	36.75	1672.73	34.31
	1-13-87	36.68	1672.80	34.24
	3-6-87	35.09	1674.39	32.65
	4-21-87	35.73	1673.75	33.29
	6-3-87	35.93	1673.55	33.49
	5-11-88	37.93	1671.55	35.49
	9-12-88	39.80	1669.68	37.36
	1-4-89	40.16	1669.32	37.72
21	9-11-86	29.17	1680.23	26.99
	10-16-86	28.94	1680.46	26.76
	11-21-86	28.61	1680.79	26.43
	1-13-87	28.51	1680.89	26.33
	3-6-87	28.41	1680.99	26.23
	4-21-87	27.95	1681.45	25.77
	6-3-87	28.12	1681.28	25.94
	5-11-88	30.77	1678.63	28.59
	9-12-88	32.22	1677.18	30.04
	1-4-89	33.07	1676.33	30.89

HESKETT SWL INFORMATION

WELL NO.	DATE	SWL-TOP	SWL-MSL	SWL-BLS
30	9-11-86	49.38	1668.26	47.29
	10-16-86	49.35	1668.29	47.26
	11-21-86	49.28	1668.36	47.19
	1-13-87	49.15	1668.49	47.06
	3-6-87	48.53	1669.11	46.44
	4-21-87	48.10	1669.54	46.01
	6-3-87	48.36	1669.28	46.27
	5-11-88	50.36	1667.28	48.27
	9-12-88	51.97	1665.67	49.88
	1-4-89	52.40	1665.24	50.31
31	9-11-86	43.21	1674.37	40.87
	10-16-86	43.74	1673.84	41.40
	11-21-86	43.74	1673.84	41.40
	1-13-87	43.41	1674.17	41.07
	3-6-87	42.59	1674.99	40.25
	4-21-87	42.26	1675.32	39.92
	6-3-87	42.59	1674.99	40.25
	5-11-88	45.01	1672.57	42.67
	9-12-88	46.88	1670.70	44.54
	1-4-89	47.31	1670.27	44.97
32	9-11-86	42.52	1675.27	40.07
	10-16-86	42.03	1675.76	39.58
	11-21-86	41.87	1675.92	39.42
	1-13-87	41.18	1676.61	38.73
	3-6-87	40.29	1677.50	37.84
	4-21-87	40.00	1677.79	37.55
	6-3-87	40.39	1677.40	37.94
	5-11-88	43.18	1674.61	40.73
	9-12-88	45.18	1672.61	42.73
	1-4-89	45.65	1672.14	43.20
33	12-15-86	40.68	1677.23	38.25
	1-13-87	40.72	1677.19	38.29
	3-6-87	39.73	1678.18	37.30
	4-21-87	39.01	1678.90	36.58
	6-3-87	39.54	1678.37	37.11
	5-11-88	42.06	1675.85	39.63
	9-12-88	43.57	1674.34	41.14
	1-4-89	44.03	1673.88	41.60

HESKETT SWL INFORMATION

WELL NO.	DATE	SWL-TOP	SWL-MSL	SWL-BLS
40	9-11-86	63.82	1646.33	61.69
	10-16-86	63.68	1646.47	61.55
	11-21-86	63.29	1646.86	61.16
	1-13-87	63.39	1646.76	61.26
	3-6-87	63.06	1647.09	60.93
	4-21-87	63.16	1646.99	61.03
	6-3-87	63.26	1646.89	61.13
	5-11-88	63.36	1646.79	61.23
	9-12-88	63.72	1646.43	61.59
	1-4-89	63.89	1646.26	61.76
41	9-11-86	36.29	1673.78	34.25
	10-16-86	36.09	1673.98	34.05
	11-21-86	35.93	1674.14	33.89
	1-13-87	36.16	1673.91	34.12
	3-6-87	35.83	1674.24	33.79
	4-21-87	35.43	1674.64	33.39
	6-3-87	35.63	1674.44	33.59
	5-11-88	37.40	1672.67	35.36
	9-12-88	39.21	1670.86	37.17
	1-4-89	39.70	1670.37	37.66
42	9-11-86	33.30	1677.01	31.11
	10-16-86	32.74	1677.57	30.55
	11-21-86	31.43	1678.88	29.24
	1-13-87	31.46	1678.85	29.27
	3-6-87	31.27	1679.04	29.08
	4-21-87	31.20	1679.11	29.01
	6-3-87	31.30	1679.01	29.11
	5-11-88	32.61	1677.70	30.42
	9-12-88	33.96	1676.35	31.77
	1-4-89	34.12	1676.19	31.93
45	12-15-86	28.71	1681.46	26.88
	1-13-87	28.58	1681.59	26.75
	3-6-87	28.48	1681.69	26.65
	4-21-87	28.58	1681.59	26.75
	6-3-87	28.71	1681.46	26.88
	5-11-88	29.89	1680.28	28.06
	9-12-88	30.84	1679.33	29.01
	1-4-89	30.97	1679.20	29.14

HESKETT SWL INFORMATION

WELL NO	DATE	SWL-TOP	SWL-MSL	SWL-BLS
43	10-16-86	26.02	1685.01	23.91
	11-21-86	25.82	1685.21	23.71
	1-13-87	26.08	1684.95	23.97
	3-6-87	25.89	1685.14	23.78
	4-21-87	26.12	1684.91	24.01
	6-3-87	26.58	1684.45	24.47
	5-11-88	27.56	1683.47	25.45
	9-12-88	29.92	1681.11	27.81
	1-4-89	29.20	1681.83	27.09
44	10-16-86	21.98	1689.42	19.67
	11-21-86	21.85	1689.55	19.54
	1-13-87	22.15	1689.25	19.84
	3-6-87	22.05	1689.35	19.74
	4-21-87	21.72	1689.68	19.41
	6-3-87	22.21	1689.19	19.90
	5-11-88	23.46	1687.94	21.15
	9-12-88	dry		
	1-4-89	24.87	1686.53	22.56

HESKETT SWL INFORMATION

WELL NO.	DATE	SWL-TOP	SWL-MSL	SWL-BLS
50	9-11-86	5.45	1671.56	3.02
	10-16-86	4.53	1672.48	2.10
	11-21-86	4.17	1672.84	1.74
	1-13-87	4.76	1672.25	2.33
	3-6-87	not taken		
	4-21-87	3.74	1673.27	1.31
	6-3-87	4.33	1672.68	1.90
	5-11-88	5.41	1671.60	2.98
	9-12-88	7.87	1669.14	5.44
	1-4-89	7.97	1669.04	5.54
	51	10-16-86	6.43	1670.27
11-21-86		6.07	1670.63	3.84
1-13-87		6.30	1670.40	4.07
3-6-87		5.94	1670.76	3.71
4-21-87		5.45	1671.25	3.22
6-3-87		5.74	1670.96	3.51
5-11-88		7.35	1669.35	5.12
9-12-88		9.61	1667.09	7.38
1-4-89		9.81	1666.89	7.58
52		10-16-86	4.43	1672.28
	11-21-86	4.07	1672.64	1.81
	1-13-87	4.56	1672.15	2.30
	3-6-87	3.81	1672.90	1.55
	4-21-87	3.61	1673.10	1.35
	6-3-87	4.20	1672.51	1.94
	5-11-88	4.99	1671.72	2.73
	9-12-88	7.81	1668.90	5.55
	1-4-89	7.89	1668.82	5.63

HESKETT SWL INFORMATION

WELL NO.	DATE	SWL-TOP	SWL-MSL	SWL-BLS
53	10-16-86	6.66	1681.51	4.20
	11-21-86	6.46	1681.71	4.00
	1-13-87	6.92	1681.25	4.46
	3-6-87	7.55	1680.62	5.09
	4-21-87	6.17	1682.00	3.71
	6-3-87	7.32	1680.85	4.86
	5-11-88	7.51	1680.66	5.05
	9-12-88	11.25	1676.92	8.79
	1-4-89	10.93	1677.24	8.47
54	10-16-86	21.36	1666.74	18.97
	11-21-86	20.97	1667.13	18.58
	1-13-87	20.87	1667.23	18.48
	3-6-87	21.00	1667.10	18.61
	4-21-87	20.70	1667.40	18.31
	6-3-87	20.54	1667.56	18.15
	5-11-88	22.28	1665.82	19.89
	9-12-88	23.13	1664.97	20.74
	1-4-89	23.62	1664.48	21.23
55	10-16-86	29.46	1666.64	27.22
	11-21-86	29.50	1666.60	27.26
	1-13-87	29.56	1666.54	27.32
	3-6-87	29.30	1666.80	27.06
	4-21-87	29.30	1666.80	27.06
	6-3-87	29.13	1666.97	26.89
	5-11-88	29.86	1666.24	27.62
	9-12-88	30.35	1665.75	28.11
	1-4-89	29.66	1666.44	27.42
56	10-16-86	42.52	1653.90	39.96
	11-21-86	39.93	1656.49	37.37
	1-13-87	39.96	1656.46	37.40
	3-6-87	39.83	1656.59	37.27
	4-21-87	39.40	1657.02	36.84
	6-3-87	39.54	1656.88	36.98
	5-11-88	41.08	1655.34	38.52
	9-12-88	42.06	1654.36	39.50
	1-4-89	42.88	1653.54	40.32

HESKETT SWL INFORMATION

WELL NO.	DATE	SWL-TOP	SWL-MSL	SWL-BLS
60	9-11-86	32.58	1683.84	30.39
	10-16-86	32.51	1683.91	30.32
	11-21-86	32.35	1684.07	30.16
	1-13-87	32.35	1684.07	30.16
	3-6-87	32.51	1683.91	30.32
	4-21-87	32.29	1684.13	30.10
	6-3-87	32.25	1684.17	30.06
	5-11-88	34.61	1681.81	32.42
	9-12-88	35.47	1680.95	33.28
	1-4-89	35.92	1680.50	33.73
61	10-16-86	32.55	1683.98	30.25
	11-21-86	32.38	1684.15	30.08
	1-13-87	32.38	1684.15	30.08
	3-6-87	32.55	1683.98	30.25
	4-21-87	32.32	1684.21	30.02
	6-3-87	32.32	1684.21	30.02
	5-11-88	34.65	1681.88	32.35
	9-12-88	35.47	1681.06	33.17
	1-4-89	35.96	1680.57	33.66
62	10-16-86	32.74	1683.93	30.39
	11-21-86	32.55	1684.12	30.20
	1-13-87	32.51	1684.16	30.16
	3-6-87	32.71	1683.96	30.36
	4-21-87	32.48	1684.19	30.13
	6-3-87	32.48	1684.19	30.13
	5-11-88	34.81	1681.86	32.46
	9-12-88	dry		
	1-4-89	dry		
70	9-11-86	55.02	1680.65	52.53
	10-16-86	54.99	1680.68	52.50
	11-21-86	54.56	1681.11	52.07
	1-13-87	54.46	1681.21	51.97
	3-6-87	54.40	1681.27	51.91
	4-21-87	54.53	1681.14	52.04
	6-3-87	54.43	1681.24	51.94
	5-11-88	54.56	1681.11	52.07
	9-12-88	54.82	1680.85	52.33
	1-4-89	54.92	1680.75	52.43

HESKETT SWL INFORMATION

WELL NO.	DATE	SWL-TOP	SWL-MSL	SWL-BLS
WS1	9-4-86	25.00	1656.71	22.90
	10-16-86	25.13	1656.58	23.03
	11-21-86	25.56	1656.15	23.46
	1-13-87*	28.15	1655.52	24.09
	3-6-87	26.77	1656.90	22.71
	4-21-87	24.97	1658.70	20.91
	6-3-87	25.36	1658.31	21.30
	5-11-88	29.00	1654.67	24.94
	9-12-88	30.32	1653.35	26.26
	1-4-89	29.86	1653.81	25.80
	* = WELL CASING REPAIRED			
WS1A	9-4-86	dry		
	10-16-86	dry		
	11-21-86	dry		
	1-13-87	dry		
	3-6-87	24.31	1657.92	21.18
	4-21-87	22.18	1660.05	19.05
	6-3-87	22.38	1659.85	19.25
	5-11-88	dry		
	9-12-88	dry		
1-4-89	dry			
WS1B	9-4-86	25.33	1656.74	22.06
	10-16-86	25.53	1656.54	22.26
	11-21-86	26.08	1655.99	22.81
	1-13-87	27.07	1655.00	23.80
	3-6-87	24.35	1657.72	21.08
	4-21-87	21.82	1660.25	18.55
	6-3-87	22.77	1659.30	19.50
	5-11-88	28.22	1653.85	24.95
	9-12-88	30.18	1651.89	26.91
	1-4-89	29.92	1652.15	26.65
WS2	9-4-86	33.96	1664.68	31.32
	10-16-86	33.66	1664.98	31.02
	11-21-86	33.47	1665.17	30.83
	1-13-87	33.79	1664.85	31.15
	3-6-87	33.73	1664.91	31.09
	4-21-87	32.91	1665.73	30.27
	6-3-87	33.04	1665.60	30.40
	5-11-88	35.33	1663.31	32.69
	9-12-88	36.68	1661.96	34.04
	1-4-89	37.17	1661.47	34.53

HESKETT SWL INFORMATION

WELL NO.	DATE	SWL-TOP	SWL-MSL	SWL-BLS
WS3	9-4-86	14.67	1646.33	11.67
	10-16-86	14.44	1646.56	11.44
	11-21-86	14.40	1646.60	11.40
	1-13-87	13.98	1647.02	10.98
	3-6-87	14.80	1646.20	11.80
	4-21-87	13.94	1647.06	10.94
	6-3-87	14.60	1646.40	11.60
	5-11-88	17.52	1643.48	14.52
	9-12-88	17.88	1643.12	14.88
	1-4-89	17.68	1643.32	14.68
WS3A	10-16-86	8.30	1652.51	5.19
	11-21-86	8.43	1652.38	5.32
	1-13-87	9.55	1651.26	6.44
	3-6-87	10.17	1650.64	7.06
	4-21-87	6.82	1653.99	3.71
	6-3-87	8.73	1652.08	5.62
	5-11-88	13.71	1647.10	10.60
	9-12-88	13.81	1647.00	10.70
	1-4-89	14.73	1646.08	11.62
	WS4	9-4-86	19.62	1642.99
10-16-86		19.52	1643.09	16.52
11-21-86		19.42	1643.19	16.42
1-13-87		18.83	1643.78	15.83
3-6-87		19.16	1643.45	16.16
4-21-87		19.00	1643.61	16.00
6-3-87		19.39	1643.22	16.39
5-11-88		21.46	1641.15	18.46
9-12-88		21.95	1640.66	18.95
1-4-89		21.23	1641.38	18.23
WS4A	9-4-86	17.29	1645.20	14.29
	10-16-86	17.16	1645.33	14.16
	11-21-86	17.13	1645.36	14.13
	1-13-87	17.39	1645.10	14.39
	3-6-87	17.62	1644.87	14.62
	4-21-87	15.81	1646.68	12.81
	6-3-87	16.93	1645.56	13.93
	5-11-88	19.36	1643.13	16.36
	9-12-88	20.11	1642.38	17.11
	1-4-89	19.75	1642.74	16.75
WS4B	9-4-86	17.39	1645.36	14.39
	10-16-86	17.23	1645.52	14.23
	11-21-86	17.16	1645.59	14.16
	1-13-87	17.42	1645.33	14.42
	3-6-87	17.65	1645.10	14.65
	4-21-87	15.81	1646.94	12.81
	6-3-87	17.06	1645.69	14.06
	5-11-88	19.55	1643.20	16.55
	9-12-88	20.28	1642.47	17.28
	1-4-89	19.92	1642.83	16.92

EXHIBIT 5-H

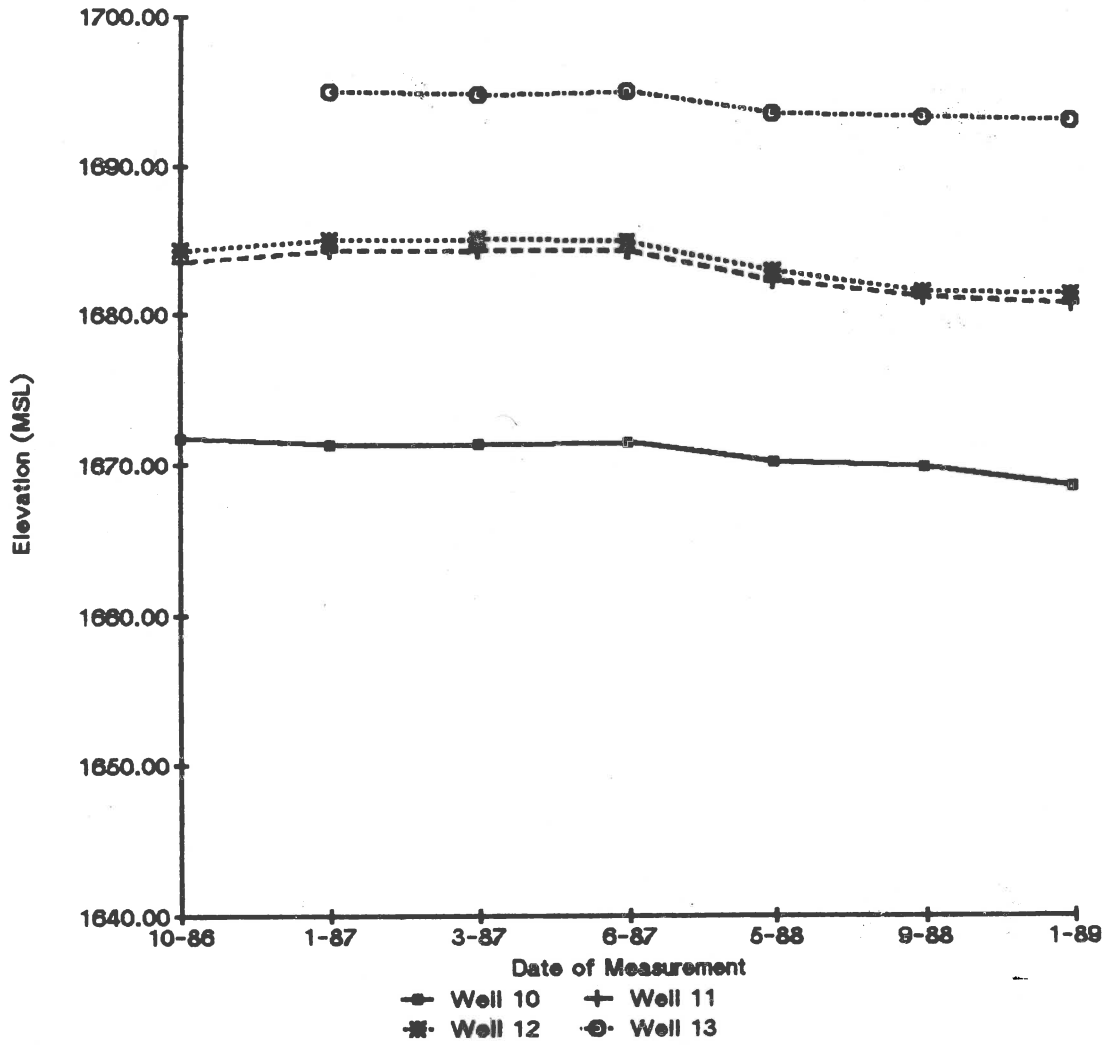
WATER TABLE ELEVATION CONTOUR MAP

EXHIBIT 5-I

SITE HYDROGRAPHS

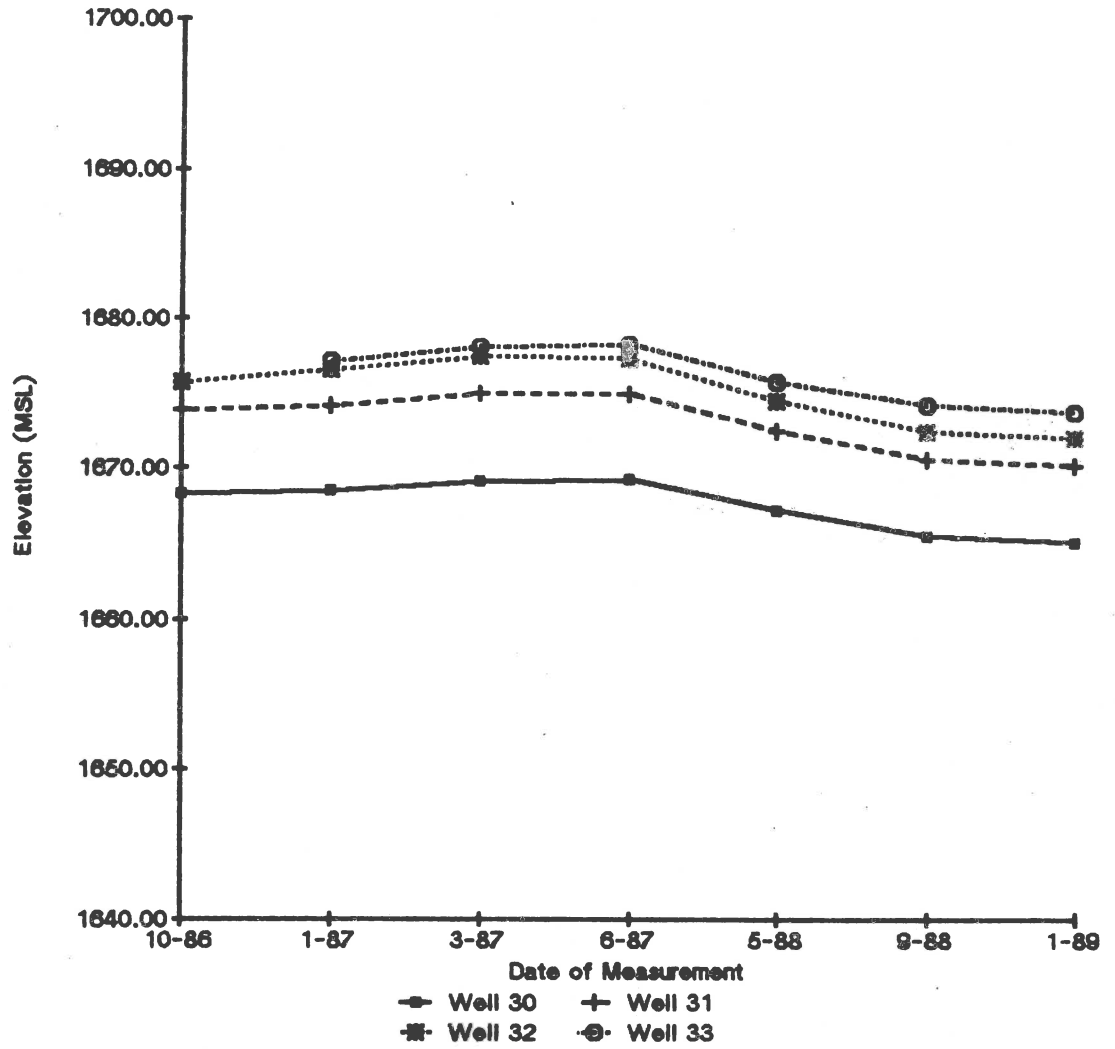
HYDROGRAPH

Wells 10, 11, 12, 13



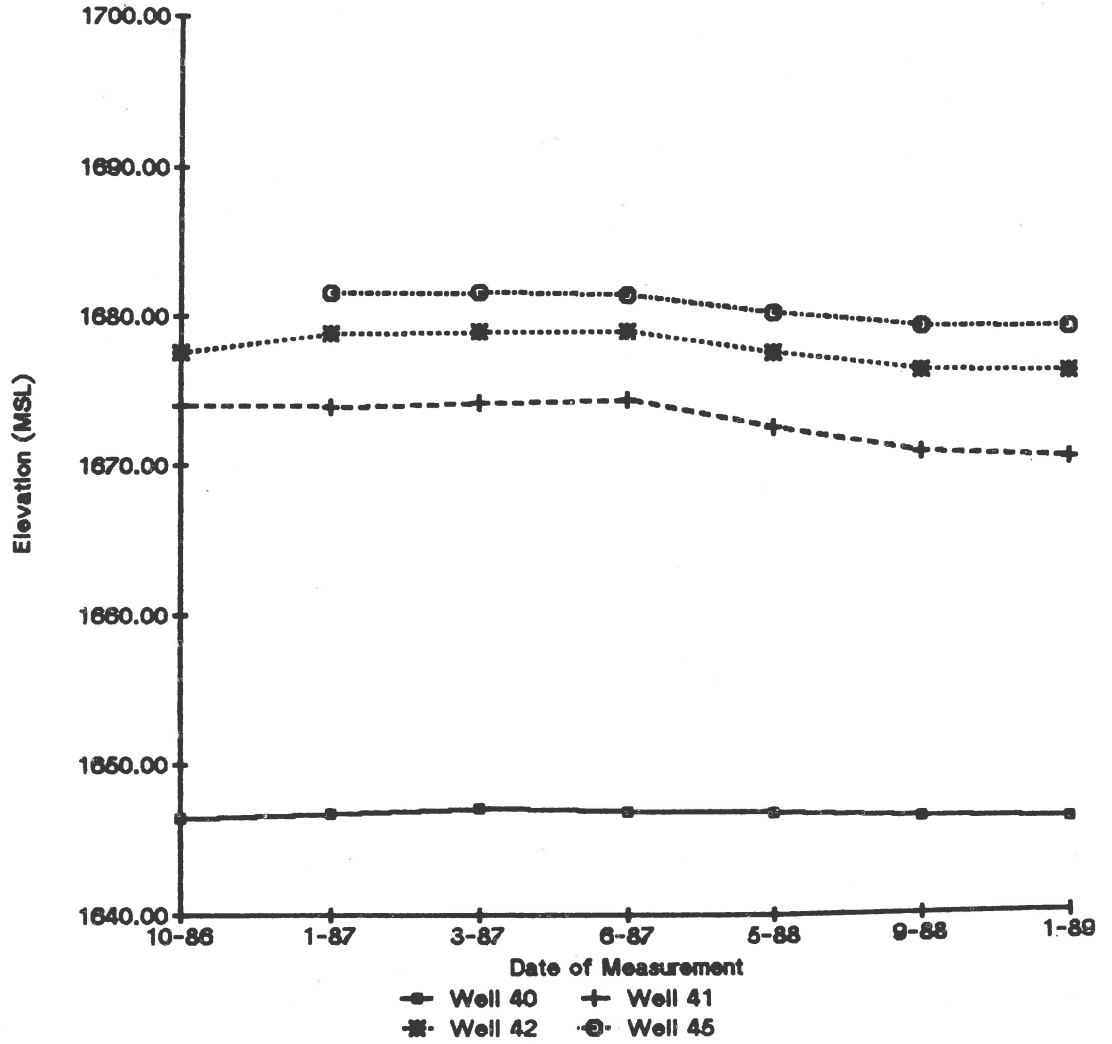
HYDROGRAPH

Wells 30, 31, 32, 33



HYDROGRAPH

Wells 40, 41, 42, 45



HYDROGRAPH

Wells 50, 51, 52

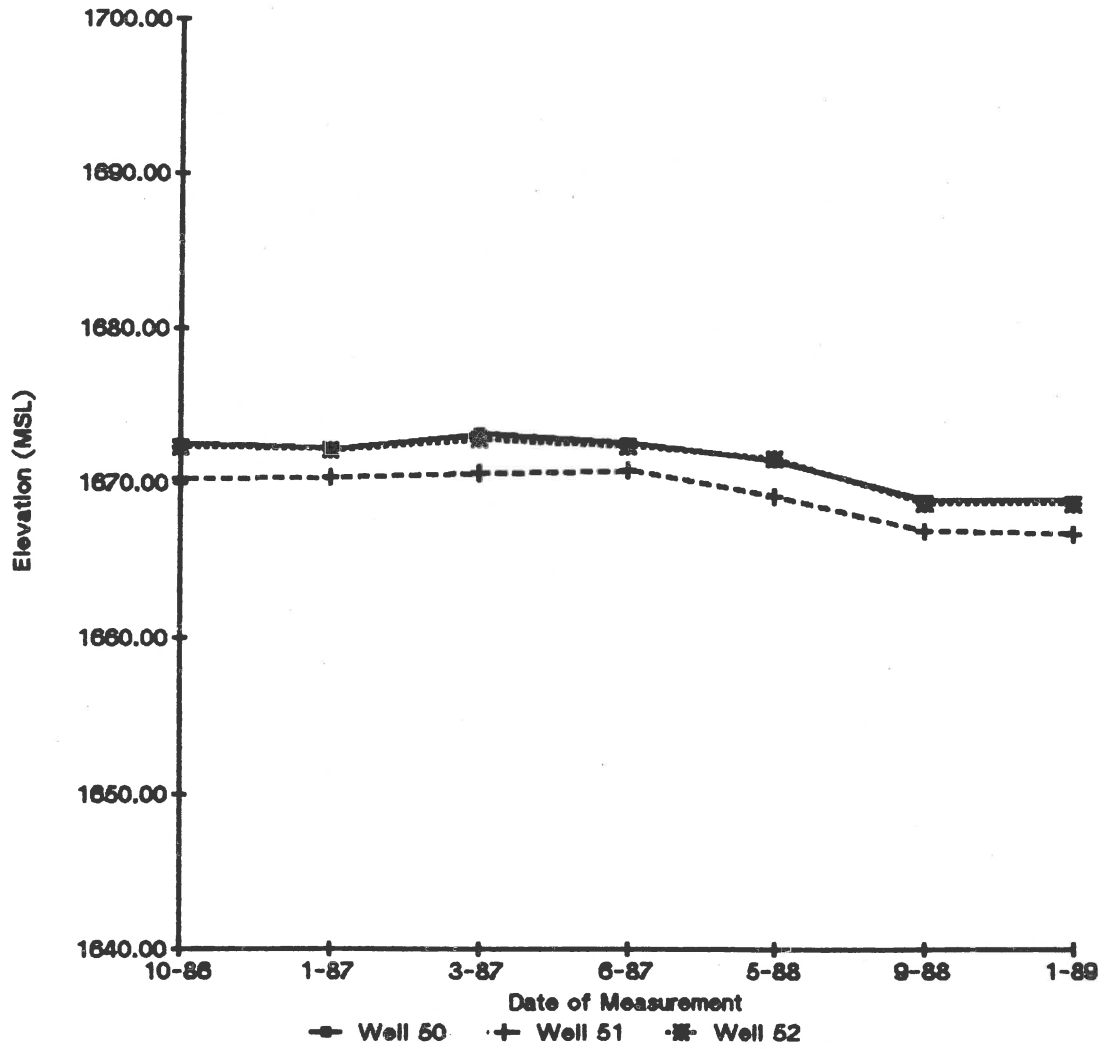


EXHIBIT 5-J

GROUNDWATER CHEMICAL ANALYSIS

Drinking Water Standards

Constituent	Recommended Concentration Limit ¹	
Total Dissolved Solids	(mg/L)	500
Sulfate (SO ₄)	(mg/L)	250
Chloride (Cl)	(mg/L)	250
Nitrate (NO ₃)	(mg/L)	45
Iron (Fe)	(mg/L)	0.3
Manganese (Mn)	(mg/L)	0.05
Copper (Cu)	(mg/L)	1.0
Zinc (Zn)	(mg/L)	5.0
Boron (B)	(mg/L)	1.0
Hydrogen Sulfide (H ₂ S)	(mg/L)	0.05
	Maximum Permissible Concentration ²	
Arsenic (As)	(mg/L)	0.05
Antimony (Sb)	(mg/L)	0.01
Barium (Ba)	(mg/L)	1.0
Cadmium (Cd)	(mg/L)	0.01
Chromium (Cr)	(mg/L)	0.05
Lead (Pb)	(mg/L)	0.050
Mercury (Hg)	(mg/L)	0.002
Selenium (Se)	(mg/L)	0.01
Silver (Ag)	(mg/L)	0.050
Fluoride (F)	(mg/L)	1.4-2.41 ³
Organics:		
Cyanide	(mg/L)	0.05
Phenol	(mg/L)	0.001
Synthetic Detergents	(mg/L)	0.5

¹Recommended concentration limits for these constituents are mainly to provide esthetic and taste characteristics.

²Maximum permissible limits are set according to health criteria.

³Limit depends on average air temperature of the region; fluoride is toxic at about 5-10 mg/L if water is consumed over a long period of time.

Chemical Analyses of Selected Wells

Parameter	Well 10	Well 12	Well 30
Sample Collection Date	9-11-86	9-11-86	9-11-86
Water Level ¹ (ft)	51.6	42.4	49.4
Elevation; Screen Center (ft)	1606.0	1653.5	1597.6
Field Water Temp (°C)	8.0	8.4	8.0
Field pH (standard units)	7.6	7.2	8.1
Field Sp.Cond. (umhos/cm)	7370.0	8070.0	1350.0
Total Dissolved Solids ² (mg/L)	9736.0	10396.0	1286.0
Total Alkalinity as CaCO ₃ (mg/L)	674.0	645.0	425.0
Bicarbonate (HCO ₃) (mg/L)	825.0	789.0	520.0
Boron (B) (mg/L)			
Calcium (Ca) (mg/L)	339.0	422.0	33.0
Chloride (Cl) (mg/L)	20.8	20.7	2.1
Fluoride (F) (mg/L)	0.3	<.2	0.4
Iron (Fe) (mg/L)	<.2	0.6	<.2
Potassium (K) (mg/L)	16.0	13.0	5.8
Magnesium (Mg) (mg/L)	302.0	318.0	34.0
Nitrate (NO ₃) (mg/L)	<1	<1	<1
Sodium (Na) ³ (mg/L)	2232.0	2438.0	352.0
Sulfate (SO ₄) (mg/L)	6443.0	6818.0	606.0

TRACE ELEMENTS:

Arsenic (Ar) (mg/L)	<.002	.0025	<.002
Barium (Ba) (mg/L)	0.090	0.157	0.030
Cadmium (Cd) (mg/L)	0.0020	0.0012	<.001
Chromium (Cr) (mg/L)	<.002	<.002	<.002
Lead (Pb) (mg/L)	<.002	<.002	<.002
Manganese (Mn) (mg/L)	0.986	2.130	0.124
Mercury (Hg) (mg/L)	<.0003	<.0003	<.0003
Molybdenum (Mo) (mg/L)	0.018	<.010	<.010
Selenium (Se) (mg/L)	<.002	<.002	<.002
Silver (Ag) (mg/L)	<.001	<.001	<.001

¹From top of PCV casing.

²TDS is calculated.

Chemical Analyses of Selected Wells

Parameter		Well 32	Well 40	Well 42
Sample Collection Date		9-11-86	9-11-86	9-11-86
Water Level ¹	(ft)	42.5	63.8	33.3
Elevation; Screen Center	(ft)	1651.7	1594.3	1662.6
Field Water Temp	(°C)	8.3	8.6	8.5
Field pH	(standard units)	6.9	7.5	7.0
Field Sp.Cond.	(umhos/cm)	3150.0	4290.0	3700.0
Total Dissolved Solids ²	(mg/L)	3927.0	5333.0	4658.0
Total Alkalinity as CaCO ₃	(mg/L)	467.0	565.0	424.0
Bicarbonate (HCO ₃)	(mg/L)	571.0	691.0	519.0
Boron (B)	(mg/L)			
Calcium (Ca)	(mg/L)	313.0	422.0	432.0
Chloride (Cl)	(mg/L)	10.0	15.2	46.8
Fluoride (F)	(mg/L)	0.3	0.2	0.3
Iron (Fe)	(mg/L)	<.2	<.2	0.3
Potassium (K)	(mg/L)	14.0	12.0	15.0
Magnesium (Mg)	(mg/L)	318.0	136.0	250.0
Nitrate (NO ₃)	(mg/L)	<1	<1	4.3
Sodium (Na) ³	(mg/L)	464.0	1047.0	648.0
Sulfate (SO ₄)	(mg/L)	2538.0	3378.0	3058.0
TRACE ELEMENTS:				
Arsenic (Ar)	(mg/L)	<.002	<.002	<.002
Barium (Ba)	(mg/L)	0.093	0.083	0.198
Cadmium (Cd)	(mg/L)	<.001	<.001	<.001
Chromium (Cr)	(mg/L)	<.002	<.002	<.002
Lead (Pb)	(mg/L)	<.002	<.002	<.002
Manganese (Mn)	(mg/L)	0.462	0.037	0.670
Mercury (Hg)	(mg/L)	<.0003	<.0003	<.0003
Molybdenum (Mo)	(mg/L)	0.014	<.010	<.010
Selenium (Se)	(mg/L)	<.002	0.005	0.032
Silver (Ag)	(mg/L)	<.001	<.001	<.001

¹From top of PCV casing.

²TDS is calculated.

Chemical Analyses of Selected Wells

Parameter	Well 44	Well 50	Well 50
Sample Collection Date	11-21-86	9-11-86	11-21-86
Water Level ¹ (ft)	21.85	5.5	4.17
Elevation; Screen Center (ft)	1687.9	1657.5	1657.5
Field Water Temp (°C)	6.5	9.7	8.5
Field pH (standard units)	6.76	7.5	7.37
Field Sp.Cond. (umhos/cm)	7580.0	4310.0	3620.0
Total Dissolved Solids ² (mg/L)	11240.0	4999.0	5196.0
Total Alkalinity as CaCO ₃ (mg/L)	401.0	418.0	416.0
Bicarbonate (HCO ₃) (mg/L)	491.0	511.0	509.2
Boron (B) (mg/L)			
Calcium (Ca) (mg/L)	648.0	313.0	391.0
Chloride (Cl) (mg/L)	558.0	34.8	33.0
Fluoride (F) (mg/L)	0.5	0.3	<0.2
Iron (Fe) (mg/L)	<0.2	<.2	<0.2
Potassium (K) (mg/L)	51.0	12.0	13.0
Magnesium (Mg) (mg/L)	1322.0	250.0	257.0
Nitrate (NO ₃) (mg/L)	30.0	23.5	112.0
Sodium (Na) (mg/L)	1589.0	871.0	902.0
Sulfate (SO ₄) (mg/L)	7390.0	3302.0	3384.0

TRACE ELEMENTS:

Arsenic (Ar) (mg/L)	<.002	<.002	<.002
Barium (Ba) (mg/L)	0.156	0.084	0.128
Cadmium (Cd) (mg/L)	<.001	<.001	<.001
Chromium (Cr) (mg/L)	<0.001	<.002	0.003
Lead (Pb) (mg/L)	<.005	<.002	<.005
Manganese (Mn) (mg/L)	0.218	0.010	0.005
Mercury (Hg) (mg/L)	<.0003	<.0003	<.0003
Molybdenum (Mo) (mg/L)	<.010	<.010	<.010
Selenium (Se) (mg/L)	0.086	0.055	0.076
Silver (Ag) (mg/L)	<.002	<.001	<.002
Phenol (mg/L)	<1.0	<1.0	<1.0
Oil & Grease (mg/L)	<3.0	<3.0	<3.0

¹From top of PCV casing.

²TDS is calculated.

Chemical Analyses of Selected Wells

Parameter	Well 52	Well 54	Well 55
Sample Collection Date	11-21-86	11-21-86	11-21-86
Water Level ¹	(ft) 4.07	20.97	29.50
Elevation; Screen Center	(ft) 1663.0	1635.1	1648.9
Field Water Temp	(oC) 8.7	6.9	7.5
Field pH (standard units)	7.38	8.03	6.81
Field Sp.Cond.	(umhos/cm) 4650.0	4570.0	9007.0
Total Dissolved Solids ²	(mg/L) 6072.0	7223.0	13081.0
Total Alkalinity as CaCO ₃	(mg/L) 424.0	616.0	528.0
Bicarbonate (HCO ₃)	(mg/L) 519.0	754.0	646.3
Boron (B)	(mg/L)		
Calcium (Ca)	(mg/L) 392.0	295.0	445.0
Chloride (Cl)	(mg/L) 45.0	92.0	81.0
Fluoride (F)	(mg/L) <0.2	0.3	0.7
Iron (Fe)	(mg/L) <0.2	<0.2	<0.2
Potassium (K)	(mg/L) 15.0	13.0	28.0
Magnesium (Mg)	(mg/L) 305.0	439.0	862.0
Nitrate (NO ₃)	(mg/L) 148.0	6.0	154.0
Sodium (Na)	(mg/L) 1115.0	1490.0	2423.0
Sulfate (SO ₄)	(mg/L) 3991.0	4617.0	9007.0

TRACE ELEMENTS:

Arsenic (Ar)	(mg/L) <.002	<.002	<.002
Barium (Ba)	(mg/L) 0.125	0.105	0.133
Cadmium (Cd)	(mg/L) <.001	<.001	<.001
Chromium (Cr)	(mg/L) 0.003	0.003	0.003
Lead (Pb)	(mg/L) <.005	<.005	<.005
Manganese (Mn)	(mg/L) 0.004	1.080	0.045
Mercury (Hg)	(mg/L) <.0003	<.0003	<.0003
Molybdenum (Mo)	(mg/L) <.010	0.041	<.010
Selenium (Se)	(mg/L) 0.088	0.025	0.386
Silver (Ag)	(mg/L) <.002	<.002	<.002
Phenol	(mg/L)	<1.0	
Oil & Grease	(mg/L)	<3.0	

¹From top of PCV casing.

²TDS is calculated.

Chemical Analyses of Selected Wells

Parameter	Well 60	Well 70
Sample Collection Date	11-21-86	9-11-86
Water Level ¹	(ft) 32.35	55.0
Elevation; Screen Center	(ft) 1677.0	1636.4
Field Water Temp	(°C) 7.6	8.6
Field pH (standard units)	6.83	8.3
Field Sp. Cond.	(umhos/cm) 10440.0	10370.0
Total Dissolved Solids ²	(mg/L) 14917.0	13129.0
Total Alkalinity as CaCO ₃	(mg/L) 540.0	491.0
Bicarbonate (HCO ₃)	(mg/L) 661.0	600.0
Boron (B)	(mg/L)	
Calcium (Ca)	(mg/L) 417.0	192.0
Chloride (Cl)	(mg/L) 208.0	10.9
Fluoride (F)	(mg/L) 0.5	0.3
Iron (Fe)	(mg/L) <0.2	<.2
Potassium (K)	(mg/L) 41.0	22.0
Magnesium (Mg)	(mg/L) 1355.0	121.0
Nitrate (NO ₃)	(mg/L) 170.0	<1
Sodium (Na)	(mg/L) 1148.0	3682.0
Sulfate (SO ₄)	(mg/L) 11632.0	8818.0

TRACE ELEMENTS:

Arsenic (Ar)	(mg/L) <.002	.0032
Barium (Ba)	(mg/L) 0.151	0.080
Cadmium (Cd)	(mg/L) <.001	0.0010
Chromium (Cr)	(mg/L) 0.004	<.002
Lead (Pb)	(mg/L) <.005	<.002
Manganese (Mn)	(mg/L) 0.033	0.110
Mercury (Hg)	(mg/L) <.0003	<.0003
Molybdenum (Mo)	(mg/L) <.010	0.017
Selenium (Se)	(mg/L) 0.195	<.002
Silver (Ag)	(mg/L) <.002	<.001
Phenol	(mg/L) <1.0	
Oil & Grease	(mg/L) <3.0	

¹From top of PCV casing.

²TDS is calculated.

GENERAL INFORMATION

Sample Location/I.D. 52 60 33 70
 Casing Diameter 2" PVC 2" PVC 2" PVC 2" PVC
 Total Well Depth 17' ? 48' ? 38' ? 40' ?
 Past Static Water Level 7.7' 35.8' 36.8' 31.9'
 Approximate Volume of Water 1.5 gal 2 gal .25 gal 1.5 gal 7.5 gal

STATIC LEVEL MEASUREMENT

Date 12/19/88 12/19/88 12/19/88 12/19/88 12/19/88
 Time 14:20 14:45 15:00 15:25 16:35
 Datum PVC Top PVC Top PVC Top PVC Top PVC Top
 Measurement Equipment SteelTape SteelTape SteelTape SteelTape SteelTape
 Static Water Level 30.60 7.65 35.80 36.80 31.92 54.85

PRE-SAMPLING PREPARATION

Pre-Sample Technique/Equip. PVCbailer PVCbailer PVCbailer PVCbailer PVCbailer
 Volume Removed 1.5 gal 2 gal .5 gal 1.5 gal 6 gal
 (dirty) (dirty)

SAMPLING

Date 12/20/88 12/20/88 12/20/88 12/20/88 12/21/88 12/21/88
 Time 10:15 10:45 11:25 12:00 15:50 16:22
 Measurement Equipment SteelTape SteelTape SteelTape SteelTape SteelTape SteelTape
 Static Water Level 31.05 7.95 35.86 36.92 31.85 54.90
 Sampling Technique/Equip. PVCbailer PVCbailer PVCbailer PVCbailer PVCbailer PVCbailer
 Field Temperature (C) 6 5 5 4 7 6
 Field pH 5.60 5.80 5.50 5.60 5.90 6.40
 Field Conductivity 3800 7200 1400 5900 1190 1380

Samples Collected
 Raw-Unfiltered 2 liters 2 liters 2 liters 2 liters 2 liters 2 liters
 Unfiltered/Sulfuric Acid 2 125ml 2 125ml 2 125ml 2 125ml 2 125ml 2 125ml
 Filtered/Nitric Acid 1 125ml 1 125ml 1 125ml 1 125ml 1 125ml 1 125ml
 Other (unfiltered/untreat) 1 125ml 1 125ml 1 125ml 1 125ml 1 125ml 1 125ml

DELIVERY

Date 12/20/88 - 12/22/88
 Time 4:30 - 10:30
 Delivered To Minnesota Valley Testing Laboratories, Inc.
 Via Hand Delivered
 Delivery Container Cooler with Ice

COMMENTS

* Well 33 had insufficient water for any samples - field parameters taken
 Well 45 - samples were dirty



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MINNESOTA VALLEY TESTING LABORATORIES, Inc.

1411 SOUTH 12TH STREET • P.O. BOX 1873
BISMARCK, NORTH DAKOTA 58502-1873



WATER ANALYSIS REPORT

Montana-Dakota Utilities
400 North Fourth
Bismarck, ND 58501

Date: January 27, 1989

W.O. #: 82-045

Attention: John Verwey

Lab. #: M- 156

Sample MDU - Heskett
Identification: #13 15:50 CST
12/20/88

P.O. #: M04548

Date Received: 12/22/88

PHYSICAL PARAMETERS:

Color units of apparent color	_____
Conductivity micromhos/cm @ 25°C	<u>12078</u>
pH	<u>7.2</u>
Solids (Total) mg/l	_____
Solids (Total Dissolved) mg/l	<u>11967</u>
Solids (Total Suspended) mg/l	_____
Solids (Total Volatile) mg/l	_____
Turbidity — NTU	_____
COMMON IONS:	
Calcium mg/l	<u>366.0</u>
Magnesium mg/l	<u>642.0</u>
Sodium mg/l	<u>1965.0</u>
Potassium mg/l	<u>27.0</u>
Acidity as CaCO ₃ mg/l	_____
Alkalinity (Total) as CaCO ₃ mg/l	<u>600</u>
Bicarbonate as CaCO ₃ mg/l	<u>600</u>
Bicarbonate as HCO ₃ mg/l	_____
Carbonate as CaCO ₃ mg/l	<u>0</u>
P-Alkalinity as CaCO ₃ mg/l	_____
Sulfate mg/l	<u>6774.9</u>
Chloride mg/l	<u>327.6</u>
Total Hardness as CaCO ₃ mg/l	<u>3556</u>
Sodium Adsorption Ratio	<u>14.37</u>
Cations	<u>157.9</u>
Anions	<u>164.2</u>
% Error	<u>2.0</u>

NUTRIENTS:

Ammonia-Nitrogen mg/l	_____
Nitrite-Nitrogen as N mg/l	_____
Nitrate-Nitrogen as N mg/l	<u>25.8</u>
Organic-Nitrogen mg/l	_____
Total - Kjeldahl Nitrogen mg/l	_____
Ortho-phosphate as P mg/l	_____
Phosphorus (Total) as P mg/l	_____
Phosphorus (Dissolved) as P mg/l	_____

METALS:

Copper (Total) mg/l	_____
Iron (Total) mg/l	_____
Manganese (Total) mg/l	_____

MISCELLANEOUS:

ADA g/l	_____
Biochemical Oxygen Demand mg/l	_____
Chemical Oxygen Demand mg/l	_____
Cyanide mg/l	_____
Fecal Coliform Count — Millipore filter/100 ml	_____
Fluoride mg/l	<u>0.62</u>
Iron Bacteria	_____
Oil & Grease mg/l	_____
Phenols mg/l	_____
Total Organic Carbon mg/l	_____
Total Plate Count per 100ml	_____

TRACE ELEMENTS:

Aluminum mg/l	_____	Cobalt mg/l	_____	Silver mg/l	<u>0.034</u>
Antimony mg/l	_____	Copper mg/l	_____	Strontium mg/l	_____
Arsenic mg/l	<u>0.007</u>	Iron mg/l	<u>0.11</u>	Thallium mg/l	_____
Barium mg/l	<u><0.100</u>	Lead mg/l	<u><0.001</u>	Thorium mg/l	_____
Beryllium mg/l	_____	Manganese mg/l	<u><0.05</u>	Tin mg/l	_____
Boron mg/l	<u>1.500</u>	Mercury mg/l	<u>0.0011</u>	Titanium mg/l	_____
Bromide mg/l	_____	Molybdenum mg/l	<u><0.100</u>	Vanadium mg/l	_____
Cadmium mg/l	<u><0.001</u>	Nickel mg/l	_____	Zinc mg/l	_____
Chromium mg/l	<u><0.050</u>	Selenium mg/l	<u><0.002</u>		

***** Metals are reported as dissolved, unless otherwise indicated. *****

FIELD DATA:

Flow	-	T ° C	<u>7.0°C</u>
E. C.	<u>1190</u>	pH	<u>5.90</u>
Static Water Level			<u>31.85</u>

Catherine A. Phelps, Chemist



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MINNESOTA VALLEY TESTING LABORATORIES, Inc.

1411 SOUTH 12TH STREET • P.O. BOX 1873
BISMARCK, NORTH DAKOTA 58502-1873



WATER ANALYSIS REPORT

Montana-Dakota Utilities
400 North Fourth
Bismarck, ND 58501

Date: January 24, 1989

W.O. #: 82-041

Attention: John Verwey

Lab. #: M-145

Sample Identification: MDU - Heskett
#45 10:15 CST
12-20-88

P.O. #: M04548

Date Received: 12-21-88

PHYSICAL PARAMETERS:

Color	units of apparent color	_____
Conductivity	micromhos/cm @ 25°C	<u>3937</u>
pH		<u>7.5</u>
Solids (Total)	mg/l	_____
Solids (Total Dissolved)	mg/l	<u>3611</u>
Solids (Total Suspended)	mg/l	_____
Solids (Total Volatile)	mg/l	_____
Turbidity - NTU		_____

COMMON IONS:

Calcium	mg/l	<u>465.0</u>
Magnesium	mg/l	<u>171.0</u>
Sodium	mg/l	<u>247.0</u>
Potassium	mg/l	<u>11.7</u>
Acidity as CaCO ₃	mg/l	_____
Alkalinity (Total) as CaCO ₃	mg/l	<u>340</u>
Bicarbonate as CaCO ₃	mg/l	<u>340</u>
Bicarbonate as HCO ₃	mg/l	_____
Carbonate as CaCO ₃	mg/l	<u>0</u>
P-Alkalinity as CaCO ₃	mg/l	_____
Sulfate	mg/l	<u>1840.0</u>
Chloride	mg/l	<u>124.1</u>
Total Hardness as CaCO ₃	mg/l	<u>1865</u>
Sodium Adsorption Ratio		<u>2.50</u>
Cations		<u>48.5</u>
Anions		<u>49.0</u>
% Error		<u>0.5</u>

TRACE ELEMENTS:

Aluminum	mg/l	_____	Cobalt	mg/l	_____	Silver	mg/l	<u>0.019</u>
Antimony	mg/l	_____	Copper	mg/l	_____	Strontium	mg/l	_____
Arsenic	mg/l	<u>0.005</u>	Iron	mg/l	<u><0.10</u>	Thallium	mg/l	_____
Barium	mg/l	<u><0.10</u>	Lead	mg/l	<u><0.001</u>	Thorium	mg/l	_____
Beryllium	mg/l	_____	Manganese	mg/l	<u><0.05</u>	Tin	mg/l	_____
Boron	mg/l	<u>1.000</u>	Mercury	mg/l	<u>0.0008</u>	Titanium	mg/l	_____
Bromide	mg/l	_____	Molybdenum	mg/l	<u><0.10</u>	Vanadium	mg/l	_____
Cadmium	mg/l	<u><0.001*</u>	Nickel	mg/l	_____	Zinc	mg/l	_____
Chromium	mg/l	<u><0.05</u>	Selenium	mg/l	<u><0.002</u>			

***** Metals are reported as dissolved, unless otherwise indicated. ***** *CEP

FIELD DATA:

Flow	-	T ° C	<u>6.0° C</u>
E. C.	<u>3800</u>	pH	<u>5.6</u>
Static Water Level			<u>31.05</u>

*Analysis completed by Controls for Environmental Pollution; Santa Fe, New Mexico

Catherine Anne Phelps

Catherine A. Phelps, Chemist



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MINNESOTA VALLEY TESTING LABORATORIES, Inc.

1411 SOUTH 12TH STREET • P.O. BOX 1873
BISMARCK, NORTH DAKOTA 58502-1873



WATER ANALYSIS REPORT

Montana-Dakota Utilities
400 North Fourth
Bismarck, ND 58501

Date: January 24, 1989

W.O. #: 82-041

Attention: John Verwey

Lab. #: M-146

Sample MDU - Heskett
Identification: #52 10:45 CST
12-20-88

P.O. #: M04548

Date Received: 12-21-88

PHYSICAL PARAMETERS:

Color	units of apparent color	_____
Conductivity	micromhos/cm @ 25°C	7300
pH		7.6
Solids (Total)	mg/l	_____
Solids (Total Dissolved)	mg/l	6724
Solids (Total Suspended)	mg/l	_____
Solids (Total Volatile)	mg/l	_____
Turbidity — NTU		_____
COMMON IONS:		
Calcium	mg/l	421.0
Magnesium	mg/l	285.0
Sodium	mg/l	1060.0
Potassium	mg/l	14.3
Acidity as CaCO ₃	mg/l	_____
Alkalinity (Total) as CaCO ₃	mg/l	438
Bicarbonate as CaCO ₃	mg/l	438
Bicarbonate as HCO ₃	mg/l	_____
Carbonate as CaCO ₃	mg/l	0
P-Alkalinity as CaCO ₃	mg/l	_____
Sulfate	mg/l	3535.6
Chloride	mg/l	99.3
Total Hardness as CaCO ₃	mg/l	2224
Sodium Adsorption Ratio		9.80
Cations		91.3
Anions		87.2
% Error		2.3

NUTRIENTS:

Ammonia-Nitrogen	mg/l	_____
Nitrite-Nitrogen as N	mg/l	_____
Nitrate-Nitrogen as N	mg/l	27.8
Organic-Nitrogen	mg/l	_____
Total - Kjeldahl Nitrogen	mg/l	_____
Ortho-phosphate as P	mg/l	_____
Phosphorus (Total) as P	mg/l	_____
Phosphorus (Dissolved) as P	mg/l	_____

METALS:

Copper (Total)	mg/l	_____
Iron (Total)	mg/l	_____
Manganese (Total)	mg/l	_____

MISCELLANEOUS:

ADA	g/l	_____
Biochemical Oxygen Demand	mg/l	_____
Chemical Oxygen Demand	mg/l	_____
Cyanide	mg/l	_____
Fecal Coliform Count — Millipore	filter/100 ml	_____
Fluoride	mg/l	0.29
Iron Bacteria		_____
Oil & Grease	mg/l	_____
Phenols	mg/l	_____
Total Organic Carbon	mg/l	_____
Total Plate Count per 100ml		_____

TRACE ELEMENTS:

Aluminum	mg/l	_____	Cobalt	mg/l	_____	Silver	mg/l	0.02
Antimony	mg/l	_____	Copper	mg/l	_____	Strontium	mg/l	_____
Arsenic	mg/l	0.004	Iron	mg/l	<0.10	Thallium	mg/l	_____
Barium	mg/l	<0.10	Lead	mg/l	<0.001	Thorium	mg/l	_____
Beryllium	mg/l	_____	Manganese	mg/l	0.06	Tin	mg/l	_____
Boron	mg/l	1.200	Mercury	mg/l	0.001	Titanium	mg/l	_____
Bromide	mg/l	_____	Molybdenum	mg/l	<0.10	Vanadium	mg/l	_____
Cadmium	mg/l	<0.001*	Nickel	mg/l	_____	Zinc	mg/l	_____
Chromium	mg/l	<0.05	Selenium	mg/l	0.005	*CEP		

***** Metals are reported as dissolved, unless otherwise indicated. *****

FIELD DATA:

Flow _____ T° C 5.0° C
 E. C. 7200 pH 5.8
 Static Water Level 7.95

*Analysis completed by Controls for Environmental Pollution; Santa Fe, New Mexico

Catherine A. Phelps, Chemist



PHONE (701) 258-9720

MINNESOTA VALLEY TESTING LABORATORIES, Inc.



1411 SOUTH 12TH STREET • P.O. BOX 1873
BISMARCK, NORTH DAKOTA 58502-1873

WATER ANALYSIS REPORT

• Montana-Dakota Utilities
400 North Fourth
Bismarck, ND 58501

Date: January 24, 1989

W.O. #: 82-041

Attention: John Verwey

Lab. #: M- 147

Sample Identification: MDU - Heskett
60 11:25 CST
12-20-88

P.O. #: M04548

Date Received: 12-21-88

PHYSICAL PARAMETERS:

Color	units of apparent color	_____
Conductivity	micromhos/cm @ 25°C	15,166
pH		7.0
Solids (Total)	mg/l	_____
Solids (Total Dissolved)	mg/l	17,634**
Solids (Total Suspended)	mg/l	_____
Solids (Total Volatile)	mg/l	_____
Turbidity — NTU		_____

COMMON IONS:

Calcium	mg/l	415.0
Magnesium	mg/l	1,340.0
Sodium	mg/l	2,245.0
Potassium	mg/l	33.8
Acidity as CaCO ₃	mg/l	_____
Alkalinity (Total) as CaCO ₃	mg/l	524
Bicarbonate as CaCO ₃	mg/l	524
Bicarbonate as HCO ₃	mg/l	_____
Carbonate as CaCO ₃	mg/l	0
P-Alkalinity as CaCO ₃	mg/l	_____
Sulfate	mg/l	10,779.8
Chloride	mg/l	273.0
Total Hardness as CaCO ₃	mg/l	6,552
Sodium Adsorption Ratio		12.09
Cations		230.4
Anions		244.2
% Error		2.9

TRACE ELEMENTS:

Aluminum	mg/l	_____	Cobalt	mg/l	_____	Silver	mg/l	0.04
Antimony	mg/l	_____	Copper	mg/l	_____	Strontium	mg/l	_____
Arsenic	mg/l	<0.002	Iron	mg/l	0.20	Thallium	mg/l	_____
Barium	mg/l	<0.10	Lead	mg/l	<0.001	Thorium	mg/l	_____
Beryllium	mg/l	_____	Manganese	mg/l	0.08	Tin	mg/l	_____
Boron	mg/l	1.800	Mercury	mg/l	0.001	Titanium	mg/l	_____
Bromide	mg/l	_____	Molybdenum	mg/l	<0.10	Vanadium	mg/l	_____
Cadmium	mg/l	<0.001*	Nickel	mg/l	_____	Zinc	mg/l	_____
Chromium	mg/l	<0.05	Selenium	mg/l	<0.002			

***** Metals are reported as dissolved, unless otherwise indicated. *****

NUTRIENTS:

Ammonia-Nitrogen	mg/l	_____
Nitrite-Nitrogen as N	mg/l	_____
Nitrate-Nitrogen as N	mg/l	19.4
Organic-Nitrogen	mg/l	_____
Total - Kjeldahl Nitrogen	mg/l	_____
Ortho-phosphate as P	mg/l	_____
Phosphorus (Total) as P	mg/l	_____
Phosphorus (Dissolved) as P	mg/l	_____

METALS:

Copper (Total)	mg/l	_____
Iron (Total)	mg/l	_____
Manganese (Total)	mg/l	_____

MISCELLANEOUS:

ADA	g/l	_____
Biochemical Oxygen Demand	mg/l	_____
Chemical Oxygen Demand	mg/l	_____
Cyanide	mg/l	_____
Fecal Coliform Count — Millipore filter/100 ml		_____
Fluoride	mg/l	0.64
Iron Bacteria		_____
Oil & Grease	mg/l	_____
Phenols	mg/l	_____
Total Organic Carbon	mg/l	_____
Total Plate Count per 100ml		_____

**High TDS due to hygroscopic nature of cations and anions.

FIELD DATA:

Flow	-	T° C	5.0° C
E. C.	1400	pH	5.5
Static Water Level	_____		35.86

*Analysis completed by Controls for Environmental Pollution; Santa Fe, New Mexico

Catherine Anne Phelps

Catherine A. Phelps, Chemist



PHONE (701) 258-9720

MINNESOTA VALLEY TESTING LABORATORIES, Inc.

1411 SOUTH 12TH STREET • P.O. BOX 1873
BISMARCK, NORTH DAKOTA 58502-1873



WATER ANALYSIS REPORT

Montana-Dakota Utilities
400 North Fourth
Bismarck, ND 58501

Date: January 27, 1989

W.O. #: 82-045

Attention: John Verwey

Lab. #: M- 157

Sample Identification: MDU - Heskett
#70 16:22 CST
12/20/88

P.O. #: M04548

Date Received: 12/22/88

PHYSICAL PARAMETERS:

Color	units of apparent color	_____
Conductivity	micromhos/cm @ 25°C	<u>14841</u>
pH		<u>8.0</u>
Solids (Total)	mg/l	_____
Solids (Total Dissolved)	mg/l	<u>13393</u>
Solids (Total Suspended)	mg/l	_____
Solids (Total Volatile)	mg/l	_____
Turbidity — NTU		_____

COMMON IONS:

Calcium	mg/l	<u>212.5</u>
Magnesium	mg/l	<u>117.0</u>
Sodium	mg/l	<u>3880.0</u>
Potassium	mg/l	<u>26.5</u>
Acidity as CaCO ₃	mg/l	_____
Alkalinity (Total) as CaCO ₃	mg/l	<u>510</u>
Bicarbonate as CaCO ₃	mg/l	<u>510</u>
Bicarbonate as HCO ₃	mg/l	_____
Carbonate as CaCO ₃	mg/l	<u>0</u>
P-Alkalinity as CaCO ₃	mg/l	_____
Sulfate	mg/l	<u>8334.9</u>
Chloride	mg/l	<u>19.9</u>
Total Hardness as CaCO ₃	mg/l	<u>1012</u>
Sodium Adsorption Ratio		<u>53.19</u>
Cations		<u>190.4</u>
Anions		<u>184.4</u>
% Error		<u>1.6</u>

NUTRIENTS:

Ammonia-Nitrogen	mg/l	_____
Nitrite-Nitrogen as N	mg/l	_____
Nitrate-Nitrogen as N	mg/l	<u><1.0</u>
Organic-Nitrogen	mg/l	_____
Total - Kjeldahl Nitrogen	mg/l	_____
Ortho-phosphate as P	mg/l	_____
Phosphorus (Total) as P	mg/l	_____
Phosphorus (Dissolved) as P	mg/l	_____

METALS:

Copper (Total)	mg/l	_____
Iron (Total)	mg/l	_____
Manganese (Total)	mg/l	_____

MISCELLANEOUS:

ADA	g/l	_____
Biochemical Oxygen Demand	mg/l	_____
Chemical Oxygen Demand	mg/l	_____
Cyanide	mg/l	_____
Fecal Coliform Count — Millipore filter/100 ml		<u>0.27</u>
Fluoride	mg/l	_____
Iron Bacteria		_____
Oil & Grease	mg/l	_____
Phenols	mg/l	_____
Total Organic Carbon	mg/l	_____
Total Plate Count per 100ml		_____

TRACE ELEMENTS:

Aluminum	mg/l	_____	Cobalt	mg/l	_____	Silver	mg/l	<u>0.030</u>
Antimony	mg/l	_____	Copper	mg/l	_____	Strontium	mg/l	_____
Arsenic	mg/l	<u>0.002</u>	Iron	mg/l	<u>0.14</u>	Thallium	mg/l	_____
Barium	mg/l	<u><0.100</u>	Lead	mg/l	<u><0.001</u>	Thorium	mg/l	_____
Beryllium	mg/l	_____	Manganese	mg/l	<u>0.28</u>	Tin	mg/l	_____
Boron	mg/l	<u>2.800</u>	Mercury	mg/l	<u>0.0010</u>	Titanium	mg/l	_____
Bromide	mg/l	_____	Molybdenum	mg/l	<u><0.100</u>	Vanadium	mg/l	_____
Cadmium	mg/l	<u><0.001</u>	Nickel	mg/l	_____	Zinc	mg/l	_____
Chromium	mg/l	<u><0.050</u>	Selenium	mg/l	<u><0.002</u>			

***** Metals are reported as dissolved, unless otherwise indicated. *****

FIELD DATA:

Flow	_____	T ° C	<u>6.0°C</u>
E. C.	<u>1380</u>	pH	<u>6.40</u>
Static Water Level	_____		<u>54.90</u>

Catherine Anne Phelps

Catherine A. Phelps, Chemist

EXHIBIT 5-K

HYDRAULIC CONDUCTIVITIES, CATION EXCHANGE CAPACITIES,

AND PARTICLE SIZE ANALYSES

(WELLS 60, WS1, WS2, WS3, AND WS4)



3100 EAST BROADWAY
P.O. BOX 1114
BISMARCK, ND 58502
PHONE 701/223-6149

LABORATORY TEST RESULTS
PROPOSED ASH PIT HESKETT STATION
MANDAN, NORTH DAKOTA

PROJECT:

Montana-Dakota Utilities

DATE: September 18, 1986

REPORTED TO:

Attn: John Verwey
400 North 4th Street
Bismarck, ND 58501

FURNISHED BY:

COPIES TO:

LABORATORY No. 5200-86-454

INTRODUCTION

A sample of fat clay was submitted to Twin City Testing Corporation on August 14, 1986. We were authorized by you to perform an Atterberg limit test, standard proctor test and permeability test. We are transmitting two (2) copies of this report.

RESULTS

The test results can be found on the attached drafts. The permeability test was performed with the falling head method on a sample remolded to 14.5% of the maximum dry density at a moisture content of 32.4%, or 0.1% above the optimum moisture content. The maximum dry density and optimum moisture content were determined in accordance with ASTM:D698.

The test results indicate that the coefficient of permeability is 2.0×10^{-7} centimeters per second on the remolded sample.

CLOSURE

If you desire to test the coefficient of permeability at a higher remolded compaction level and/or higher moisture content, please contact us. Also contact us if you have any questions in regards to this report or if we can be of further service to you.

AS A MUTUAL PROTECTION TO CLIENTS, THE PUBLIC AND OURSELVES, ALL REPORTS ARE SUBMITTED AS THE CONFIDENTIAL PROPERTY OF CLIENTS, AND AUTHORIZATION FOR PUBLICATION OF STATEMENTS, CONCLUSIONS OR EXTRACTS FROM OR REGARDING OUR REPORTS IS RESERVED PENDING OUR WRITTEN APPROVAL.

Twin City Testing Corporation

By

John Zelinger



MOISTURE - DENSITY CURVE

SAMPLE NO. 1 - Hole 60, 20'-40'

PROJECT: PROPOSED ASH PIT HESKETT STATION
 MANDAN, NORTH DAKOTA
REPORTED TO: Montana-Dakota Utilities Company
 Attn: John Verwey
LABORATORY NO. 5200-86-454

DATE: August 21, 1986

COPIES TO:

*LIQUID LIMIT: 59.4

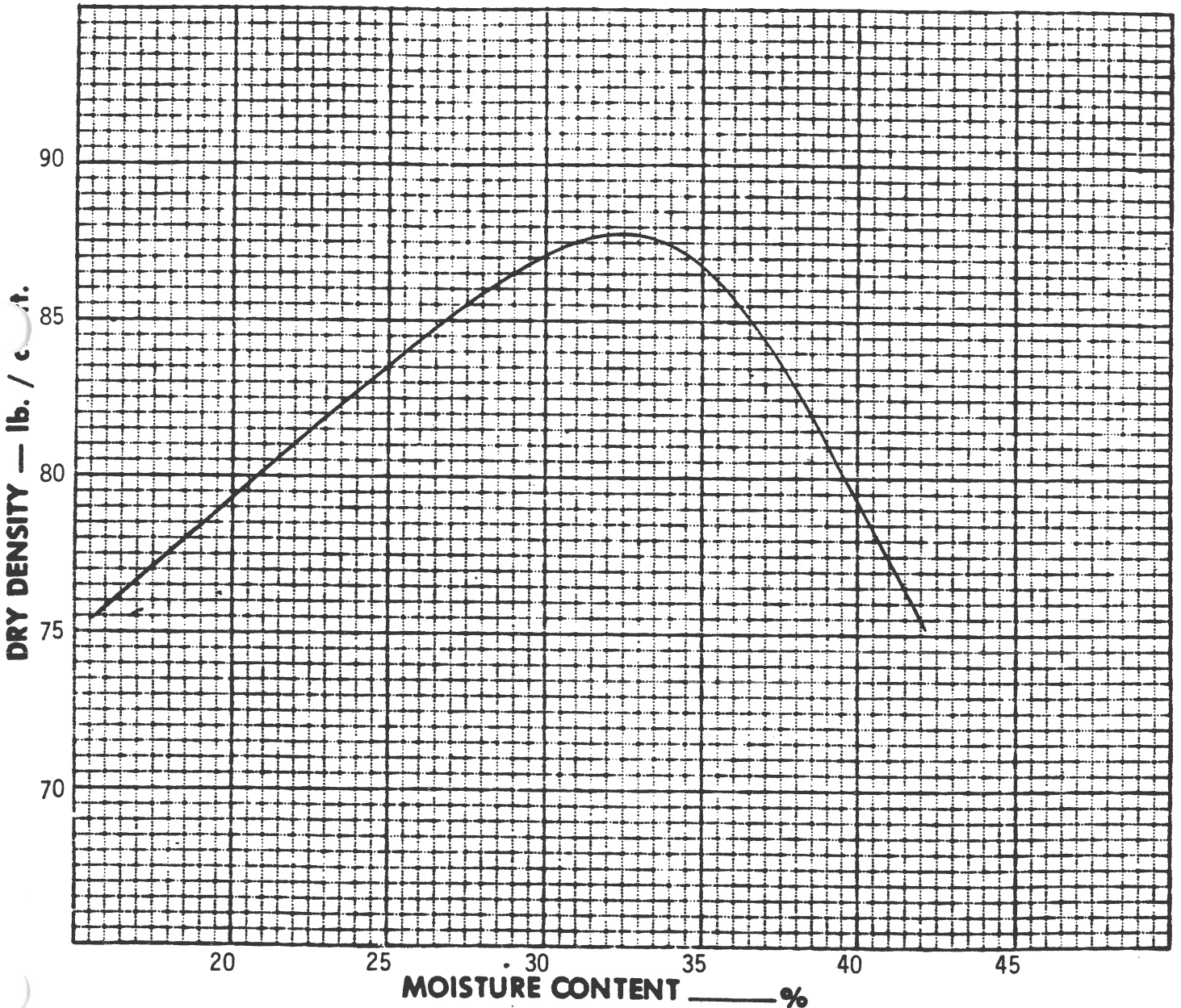
*PLASTIC LIMIT: 23.9

METHOD OF TEST: ASTM:D698-78, Method "A"

TYPE OF MATERIAL: Fat Clay, brown (CH)

MAXIMUM DENSITY: 87.8 lb./cu. ft.

OPTIMUM MOISTURE 32.3 %



Twin City Testing and Engineering Laboratory, Inc.

By David P. Johnson

LABORATORY TEST DATA

PROJECT: PROPOSED ASH PIT-HESKETT STATION-MANDAN, NORTH DAKOTA

REPORTED TO: Montana-Dakota Utilities Company
Attn: John Verwey

JOB NO.: 5200-86-454

Boring No.				
Sample No. Sample Designation	Hole 60			
Depth (ft)	20-40			
Type of Sample	Bag			
Soil Classification (ASTM:D2487)	Fat Clay (CH)			
In-Place Moisture Content (%)	-			
Moisture-Density Relation of Soil (ASTM:D698)				
Max. Dry Density (PCF)	87.8			
Optimum Moisture Content (%)	32.3			
Permeability Test				
Trial No.	6.8			
Type of Test	Falling Head			
Type of Specimen	Compacted			
Specimen Height (inches)	3.00			
Specimen Diameter (inches)	2.82			
Dry Density (PCF)	82.9			
Percent of Max. Density	94.5			
Moisture Content (%)	32.4			
Max. Head Differential (ft)	5.0			
Confining Pressure (effective - PSI)	2.0			
Water Temperature (°C)	21			
Coefficient of Permeability K @ 20°C (cm/sec)	2×10^{-7}			
K @ 20°C (ft/min)	4×10^{-7}			
Atterberg Limits				
Liquid Limit (%)	59.4			
Plastic Limit (%)	23.9			
Plasticity Index	35.5			

December 14, 1981

Water Supply, Inc
PO Box 1191
Bismarck, ND 58502

Attn: Roger Schmid

Gentlemen

Subj: Soil Testing for MDU Heskett Power Plant
Mandan, North Dakota
Invoice #52-0688

Attached herewith, please find our laboratory test results for permeability tests, cation exchange capacity, particle size distribution curves and U.S.D.A. textural classification charts.

If you have any questions or need any additional information, please contact us at the Bismarck office.

Very truly yours,



Gary L. Arman, P.E.
Operations Manager
Western North Dakota

GLA:djs

Encs

LABORATORY TEST DATA

PROJECT: SOIL TESTING FOR MDU HESKETT POWER PLANT - MANDAN, ND

DATE: December 14, 1981

REPORTED TO: Water Supply, Inc

JOB NO.: 52-0688

Boring No.	MDU Heskett 1	MDU Heskett 1	MDU Heskett 1	MDU Heskett 2
Sample No. Sample Designation				
Depth (ft)	20-21	25-26	30-31	29-30
Type of Sample	Core	Core	Core	Core
Soil Classification (ASTM:D2487)	SILTY CLAY & FAT CLAY (CL & CH)	SILTY CLAY & FAT CLAY (CL & CH)	SILTY CLAY & FAT CLAY (CL & CH)	SHALE, (Tex- tural Classi- fication: Fat Clay) (CH)
In-Place Moisture Content (%)				
Moisture-Density Relation of Soil (ASTM:D698)				
Max. Dry Density (PCF)				
Optimum Moisture Content (%)				
Permeability Test				
Trial No.	1	1	1	1
Type of Test	Falling Head	Falling Head	Falling Head	Falling Head
Type of Specimen	Natural	Natural	Natural	Natural
Specimen Height (inches)	4.36	3.49	3.76	2.08
Specimen Diameter (inches)	4.00	2.86	4.00	1.98
Dry Density (PCF)				
Percent of Max. Density				
Moisture Content (%)				
Max. Head Differential (ft)	5.0	5.0	5.0	5.0
Confining Pressure (effective - PSI)	2.0	2.0	2.0	2.0
Water Temperature (°C)	21	21	20	21
Coefficient of Permeability K @ 20°C (cm/sec)	2.6×10^{-8}	1.5×10^{-8}	1.7×10^{-8}	2.7×10^{-9}
K @ 20°C (ft/min)	5.2×10^{-8}	2.9×10^{-8}	3.4×10^{-8}	5.4×10^{-9}
Atterberg Limits				
Liquid Limit (%)				
Plastic Limit (%)				
Plasticity Index				

TWIN CITY TESTING LAB

LABORATORY TEST DATA

PROJECT: SOIL TESTING FOR MDU HESKETT POWER PLANT - MANDAN, ND

DATE: December 14, 1981

REPORTED TO: Water Supply, Inc

JOB NO.: 52-0688

Boring No.	MDU Heskett 2	MDU Heskett 2	MDU Heskett 3	MDU Heskett 3
Sample No. Sample Designation				
Depth (ft)	61-62	73-74	15-16	19-20
Type of Sample	Core	Core	Core	Core
Soil Classification (ASTM:D2487)	SHALE, (Textural Classification: Fat Clay) (CH)	SHALE, (Textural Classification: Fat Clay) (CH)	SILTY CLAY (CL-ML)	FAT CLAY & SILTY CLAY (CH & CL)
In-Place Moisture Content (%)				
Moisture-Density Relation of Soil (ASTM:D698)				
Max. Dry Density (PCF)				
Optimum Moisture Content (%)				
Permeability Test				
Trial No.	1	1	1	1
Type of Test	Falling Head	Falling Head	Falling Head	Falling Head
Type of Specimen	Natural	Natural	Natural	Natural
Specimen Height (inches)	1.96	0.80	2.93	3.29
Specimen Diameter (inches)	1.99	1.98	4.00	4.00
Dry Density (PCF)				
Percent of Max. Density				
Moisture Content (%)				
Max. Head Differential (ft)	5.0	5.0	5.0	50.0
Confining Pressure (effective - PSI)	2.0	2.0	2.0	2.0
Water Temperature (°C)	21	19	22	22
Coefficient of Permeability K @ 20°C (cm/sec)	3.6×10^{-8}	1.8×10^{-8}	8.5×10^{-8}	1.8×10^{-9}
K @ 20°C (ft/min)	7.1×10^{-8}	3.6×10^{-8}	1.7×10^{-7}	3.5×10^{-9}
Atterberg Limits				
Liquid Limit (%)				
Plastic Limit (%)				
Plasticity Index				

TWIN CITY TESTING LAB

LABORATORY TEST DATA

PROJECT: SOIL TESTING FOR MDU HESKETT POWER PLANT - MANDAN, ND

DATE: December 14, 1981

REPORTED TO: Water Supply, Inc

JOB NO.: 52-0688

Boring No.	MDU Heskett 3	MDU Heskett 4	MDU Heskett 4	MDU Heskett 4
Sample No. Sample Designation				
Depth (ft)	31-32	9-10	41-42	51-52
Type of Sample	Core	Core	Core	Core
Soil Classification (ASTM:D2487)	SILTY CLAY & FAT CLAY (CL & CH)	FAT CLAY & SILTY CLAY (CH & CL)	SHALE, (Tex- tural Classi- fication: Organic Fat Clay (CH-OH))	SHALE, (Tex- tural Classi- fication: Silty Clay (CL))
In-Place Moisture Content (%)				
Moisture-Density Relation of Soil (ASTM:D698)				
Max. Dry Density (PCF)				
Optimum Moisture Content (%)				
Permeability Test				
Trial No.	1	1	1	1
Type of Test	Falling Head	Falling Head	Falling Head	Falling Head
Type of Specimen	Natural	Natural	Natural	Natural
Specimen Height (inches)	2.20	3.63	2.31	2.31
Specimen Diameter (inches)	4.00	4.00	1.98	1.45
Dry Density (PCF)				
Percent of Max. Density				
Moisture Content (%)				
Max. Head Differential (ft)	30.0	50.0	5.0	5.0
Confining Pressure (effective - PSI)	2.0	2.0	2.0	2.0
Water Temperature (°C)	21	22	20	21
Coefficient of Permeability K @ 20°C (cm/sec)	9.1×10^{-9}	7.2×10^{-9}	7.6×10^{-9}	1.9×10^{-7}
K @ 20°C (ft/min)	1.8×10^{-8}	1.4×10^{-8}	1.5×10^{-8}	3.7×10^{-7}
Atterberg Limits				
Liquid Limit (%)				
Plastic Limit (%)				
Plasticity Index				

TWIN CITY TESTING LAB



REPORT OF: CATION EXCHANGE CAPACITY

SOIL TESTING FOR MDU HESKETT POWER

PLANT - MANDAN, NORTH DAKOTA

DATE: December 14, 1981

PROJECT:

REPORTED TO:

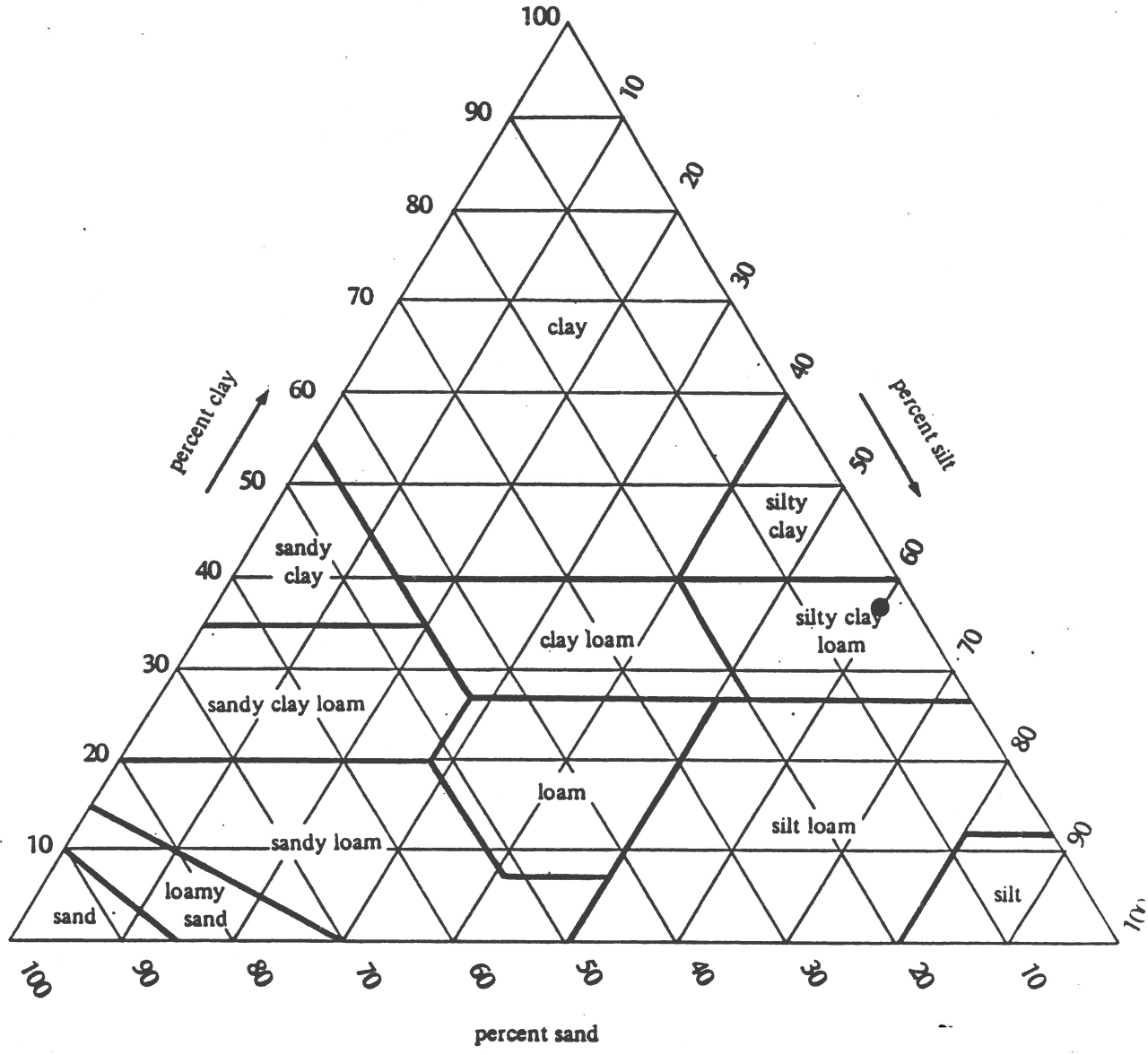
Water Supply, Inc
PO Box 1191
Bismarck, ND 58502
Attn: Roger Schmid

LABORATORY No. 52-0688

<u>SAMPLE NUMBER</u>	<u>DEPTHS</u>	<u>CATION EXCHANGE CAPACITY (meq/100g) (milliequivalents/100 gr)</u>
MDU Heskett #1	20'-21'	71.8
#1	25'-26'	12.3
#1	30'-31'	74.2
#1	40'-41'	27.4
MDU Heskett #2	29'-30'	92.2
#2	56'-57'	69.7
#2	61'-62'	12.0
#2	73'-74'	48.4
MDU Heskett #3	15'-16'	70.1
#3	19'-20'	58.1
#3	31'-32'	35.6
MDU Heskett #4	9'-10'	40.4
#4	15'-16'	60.9
#4	31'-32'	26.1
#4	41'-42'	51.3
#4	51'-52'	56.4

USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #1, 20'-21'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

Size Range in Millimeters (Mean Diameter)												
75	2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008	
GRAVEL	SAND					SILT			CLAY			
	Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine	
	10	18	35	60	140	300						
U.S. Standard Sieve Numbers												

TWIN CITY TESTING LAB



Twin City Testing
and engineering laboratory, inc.
662 CROMWELL AVENUE
ST. PAUL, MN 55114
PHONE 612/645-3601

Job No. 52-0688

Sample No. MDU Heskett #1 Depth: 25' -26'

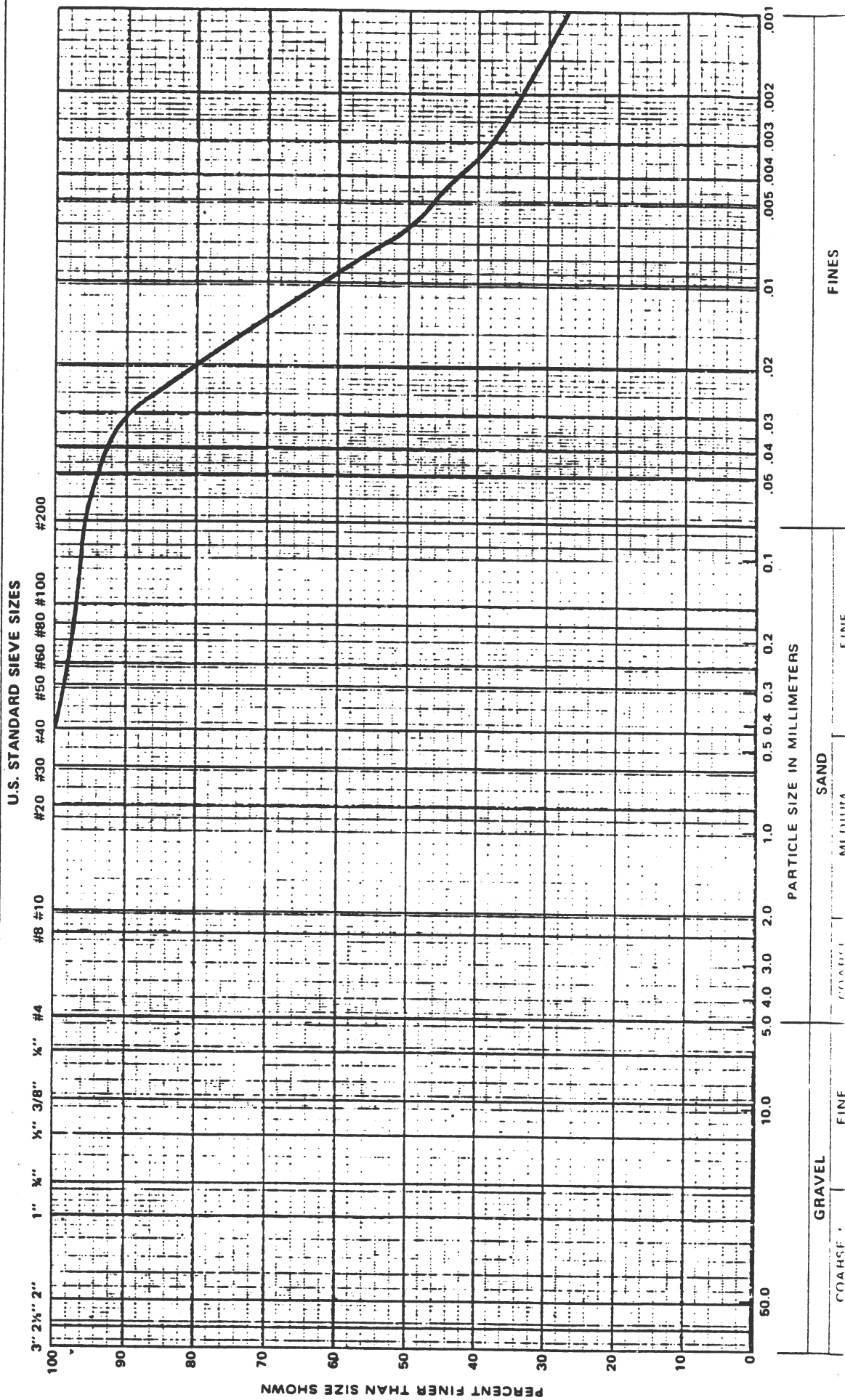
Classification (ASTM:D2487) CL & CH

Description SILTY CLAY & FAT CLAY

Project: SOIL TESTING FOR MDU HESKETT
POWER PLANT - MANDAN, NORTH DAKOTA

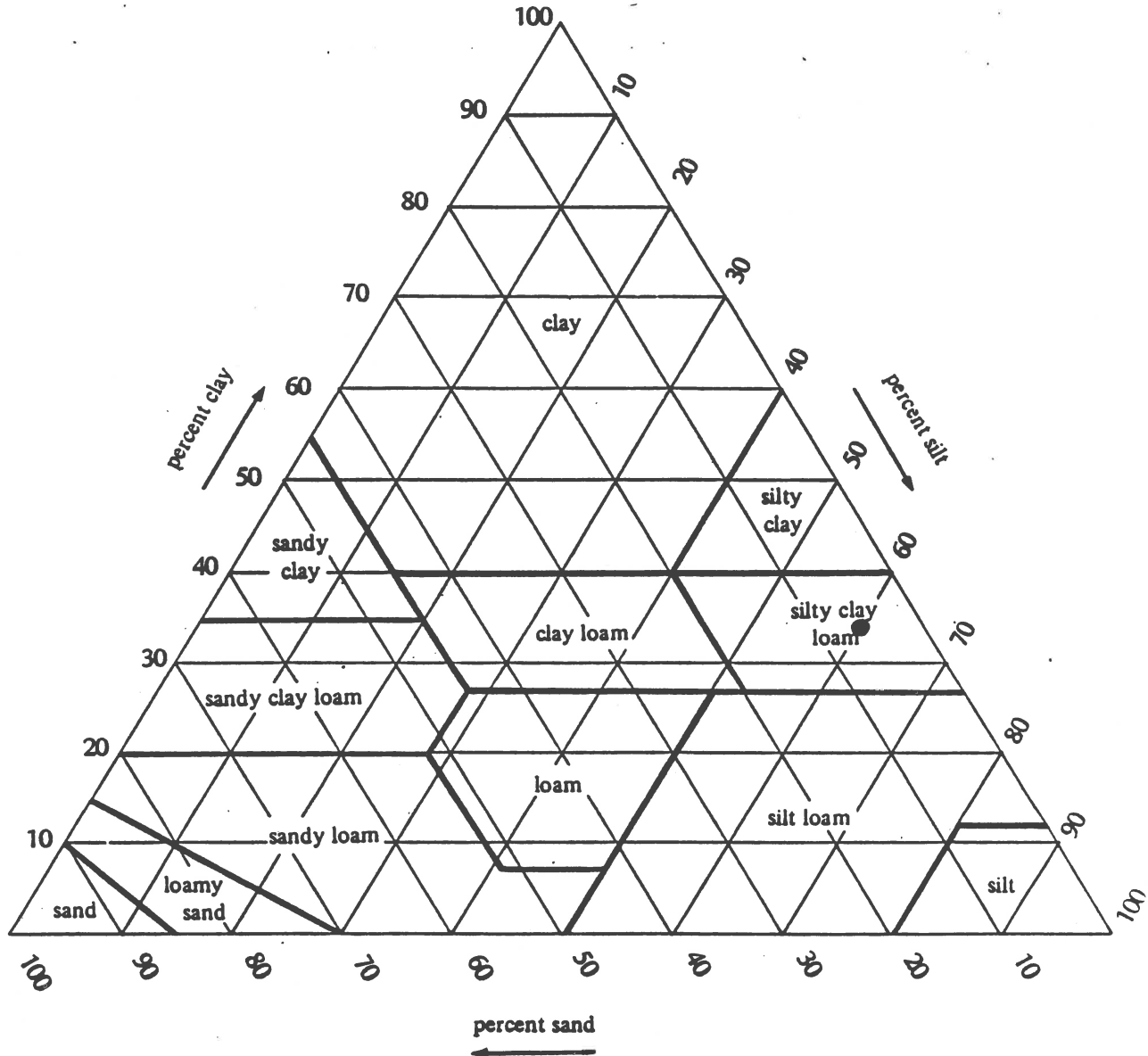
Reported To: Water Supply, Inc.

GRAIN SIZE DISTRIBUTION CURVE



USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #1, 25'-26'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

Size Range in Millimeters (Mean Diameter)												
75	2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008	
GRAVEL	SAND					SILT			CLAY			
	Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine	
	10	18	35	60	140	300						

U.S. Standard Sieve Numbers

TWIN CITY TESTING LAB



twin city testing
and engineering laboratory, inc.
662 CROWWELL AVENUE
ST PAUL, MN 55114
PHONE 612/645-3601

Job No. 52-0688

Sample No. MDU Heskett #1 Depth: 30' -31'

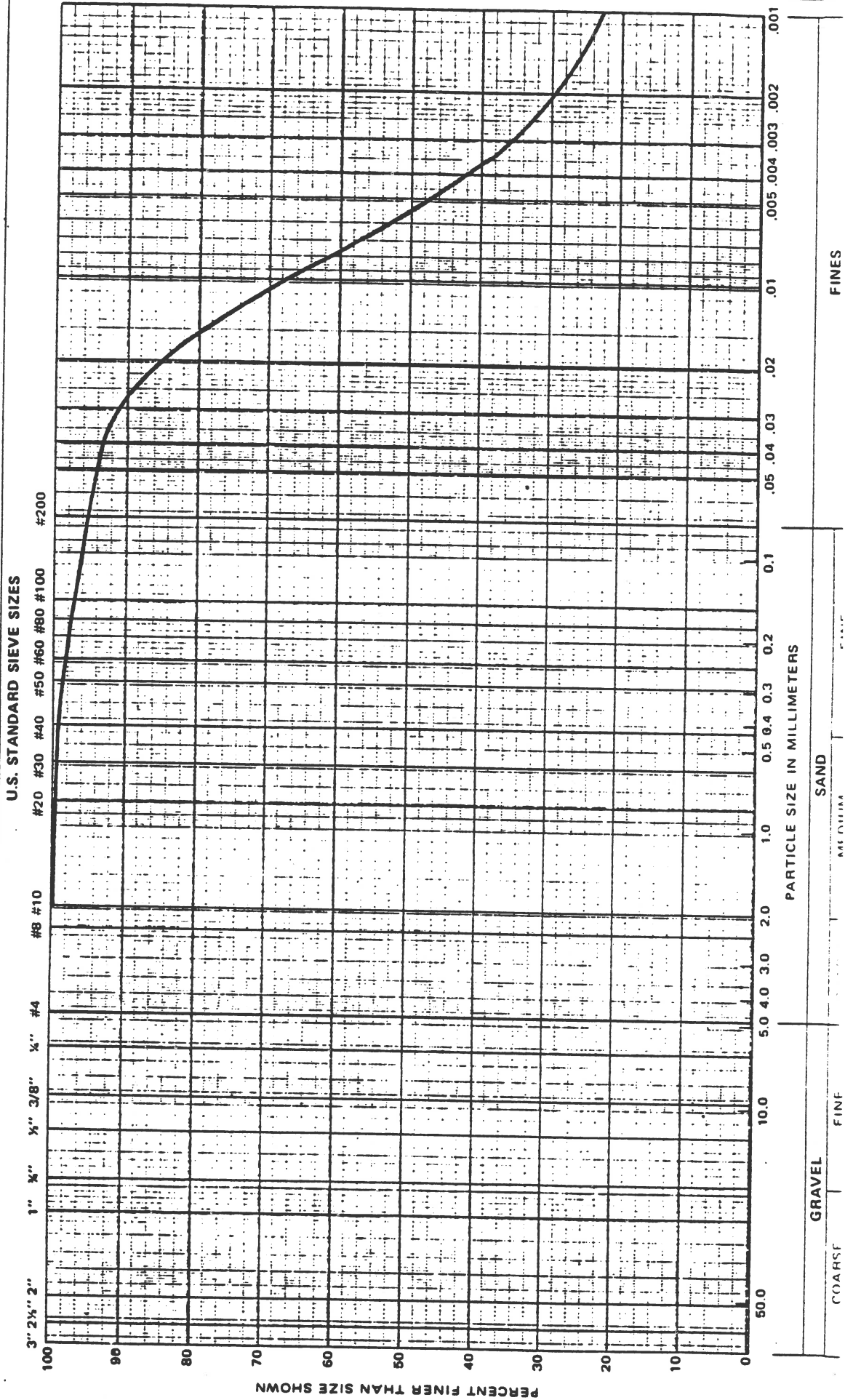
Classification (ASTM:D2487) CL & CH

Description SILTY CLAY & FAT CLAY

Project: SOIL TESTING FOR MDU HESKETT
POWER PLANT - MANDAN, NORTH DAKOTA

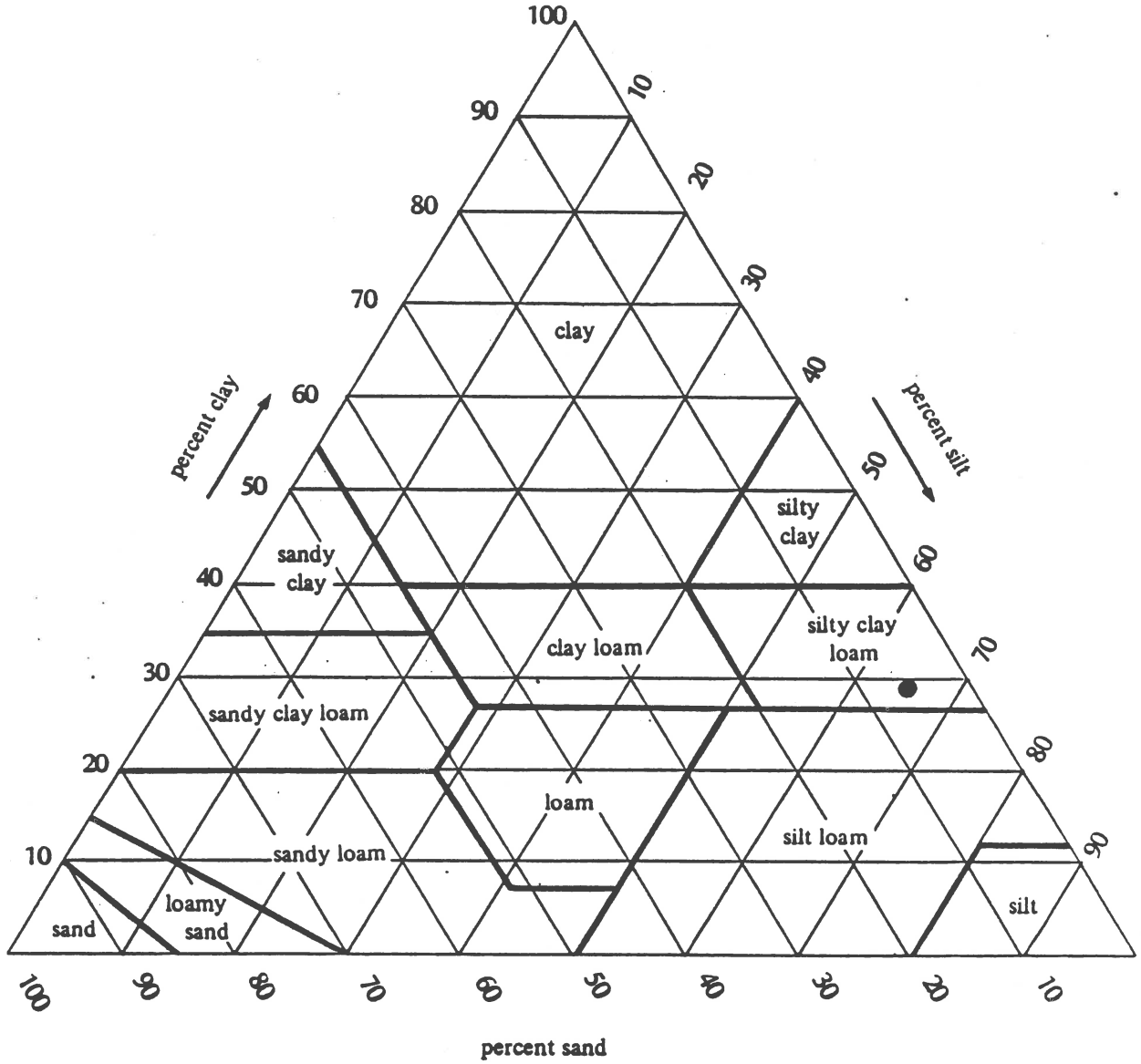
Reported To: Water Supply, Inc.

GRAIN SIZE DISTRIBUTION CURVE



USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #1, 30'-31'



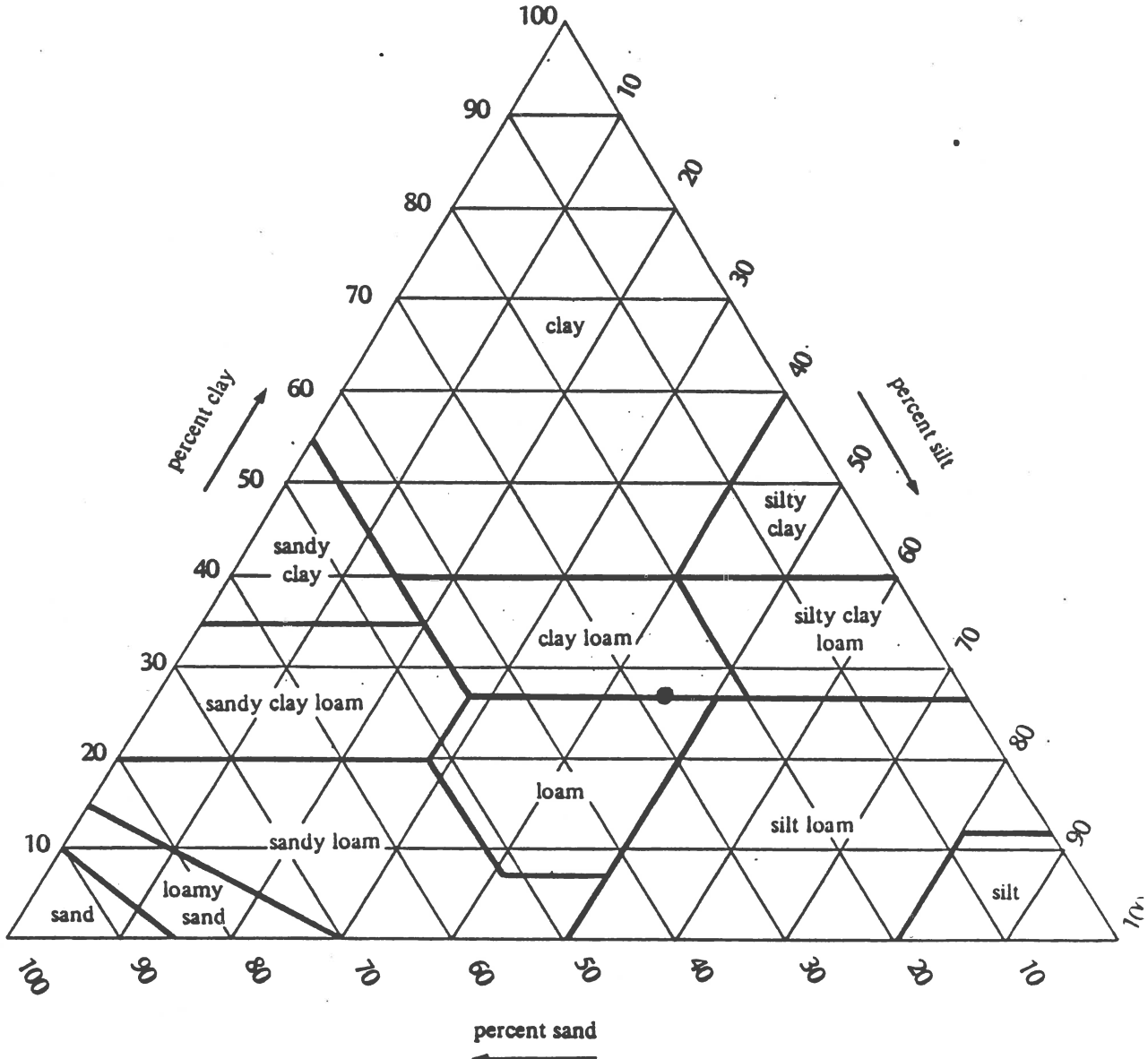
COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

Size Range in Millimeters (Mean Diameter)											
75	2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008
GRAVEL	SAND					SILT			CLAY		
	Very Coarse	Coarse	Me- dium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine
	10	18	35	60	140	300					
U.S. Standard Sieve Numbers											

TWIN CITY TESTING LAB

USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #2, 29'-30'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

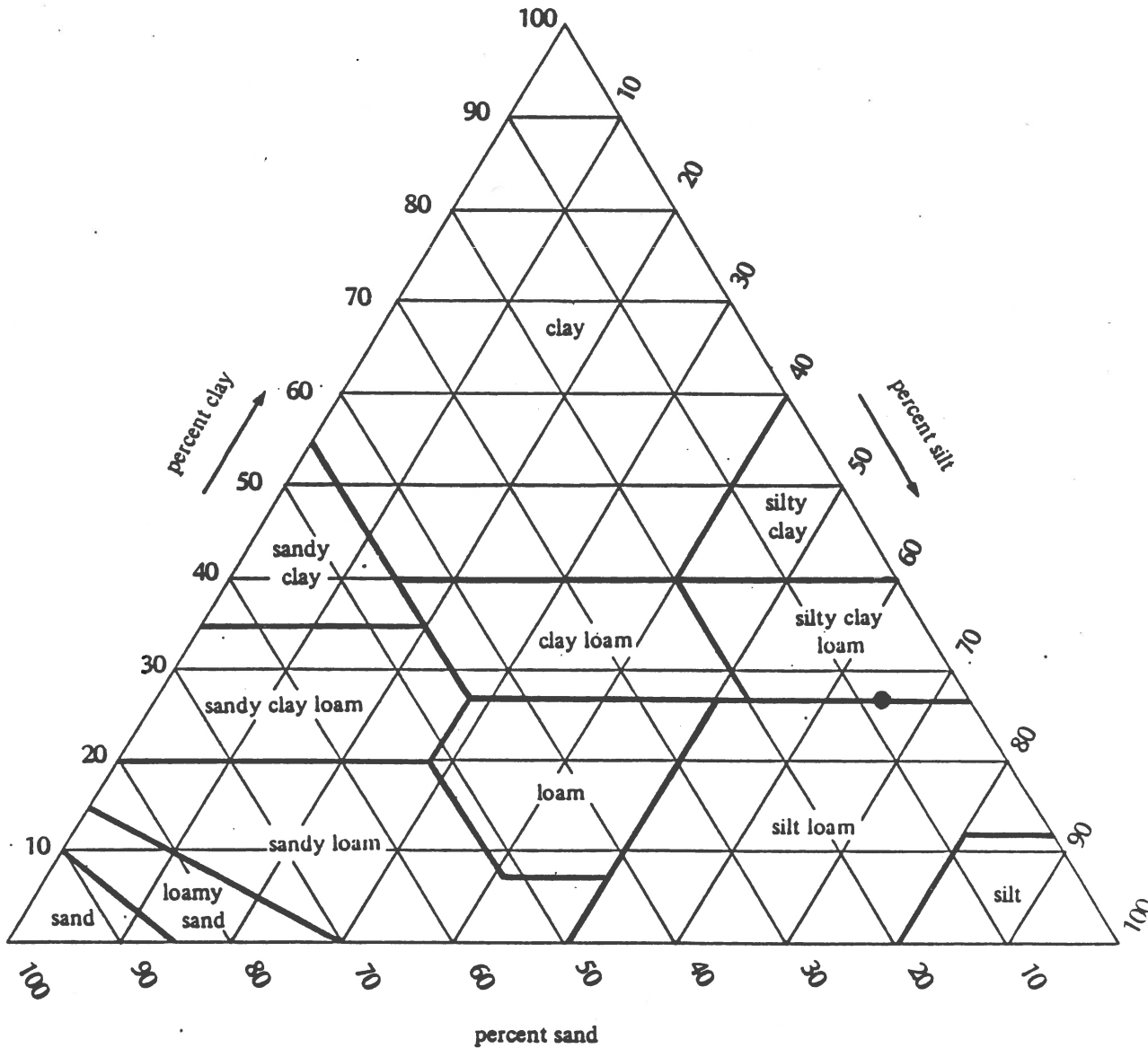
Size Range in Millimeters (Mean Diameter)												
75	2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008	
GRAVEL	SAND					SILT			CLAY			
	Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine	
	10	18	35	60	140	300						

U.S. Standard Sieve Numbers

TWIN CITY TESTING LAB

USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #2, 61'-62'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

Size Range in Millimeters (Mean Diameter)

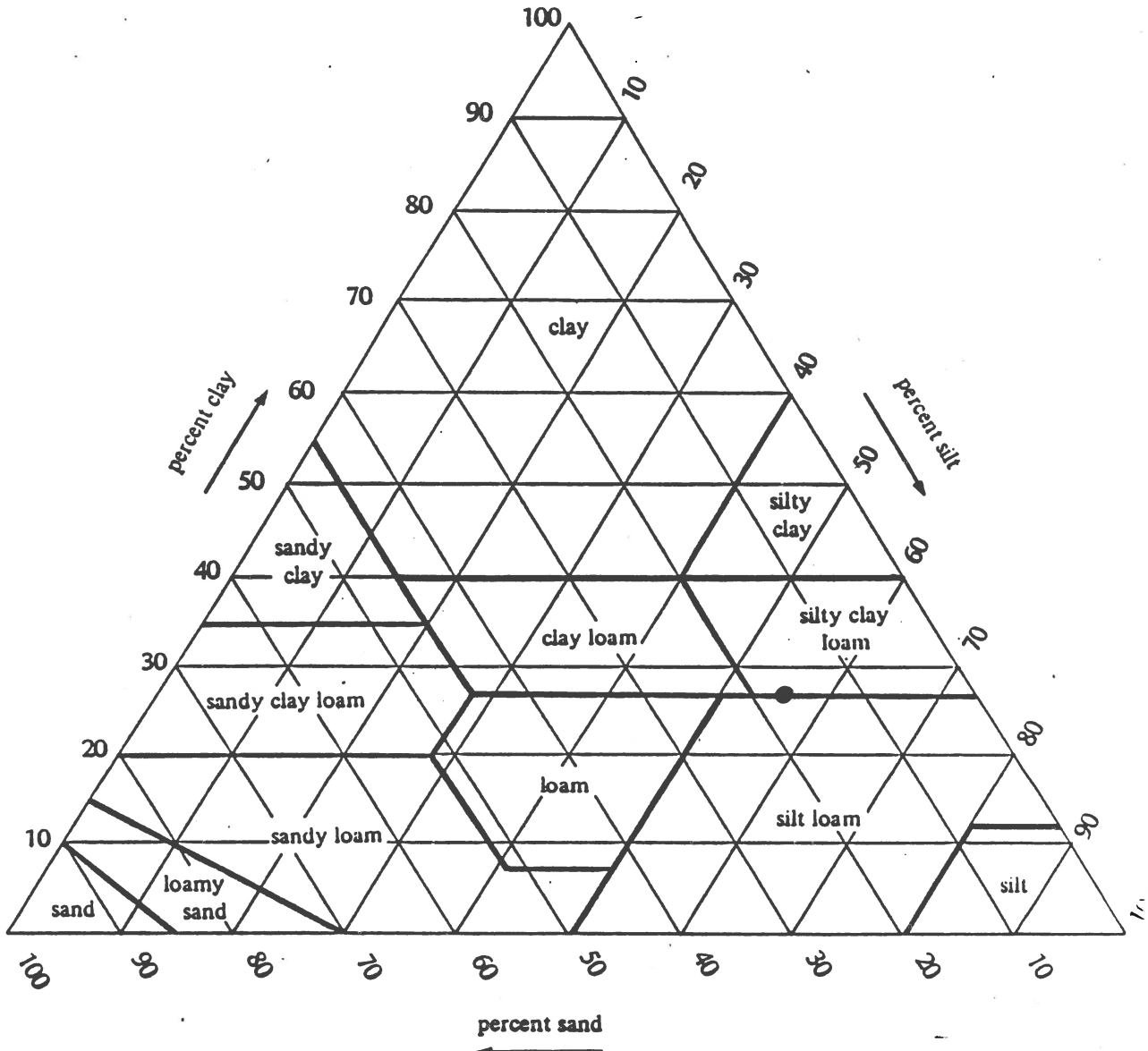
		2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008
GRAVEL	SAND					SILT				CLAY		
	Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine	
	10	18	35	60	140	300						

U.S. Standard Sieve Numbers

TWIN CITY TESTING LAB

USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #2, 73'-74'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

Size Range in Millimeters (Mean Diameter)

	75	2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008
GRAVEL	SAND					SILT			CLAY			
	Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine	
	10	18	35	60	140	300						
	U.S. Standard Sieve Numbers											

TWIN CITY TESTING LAB



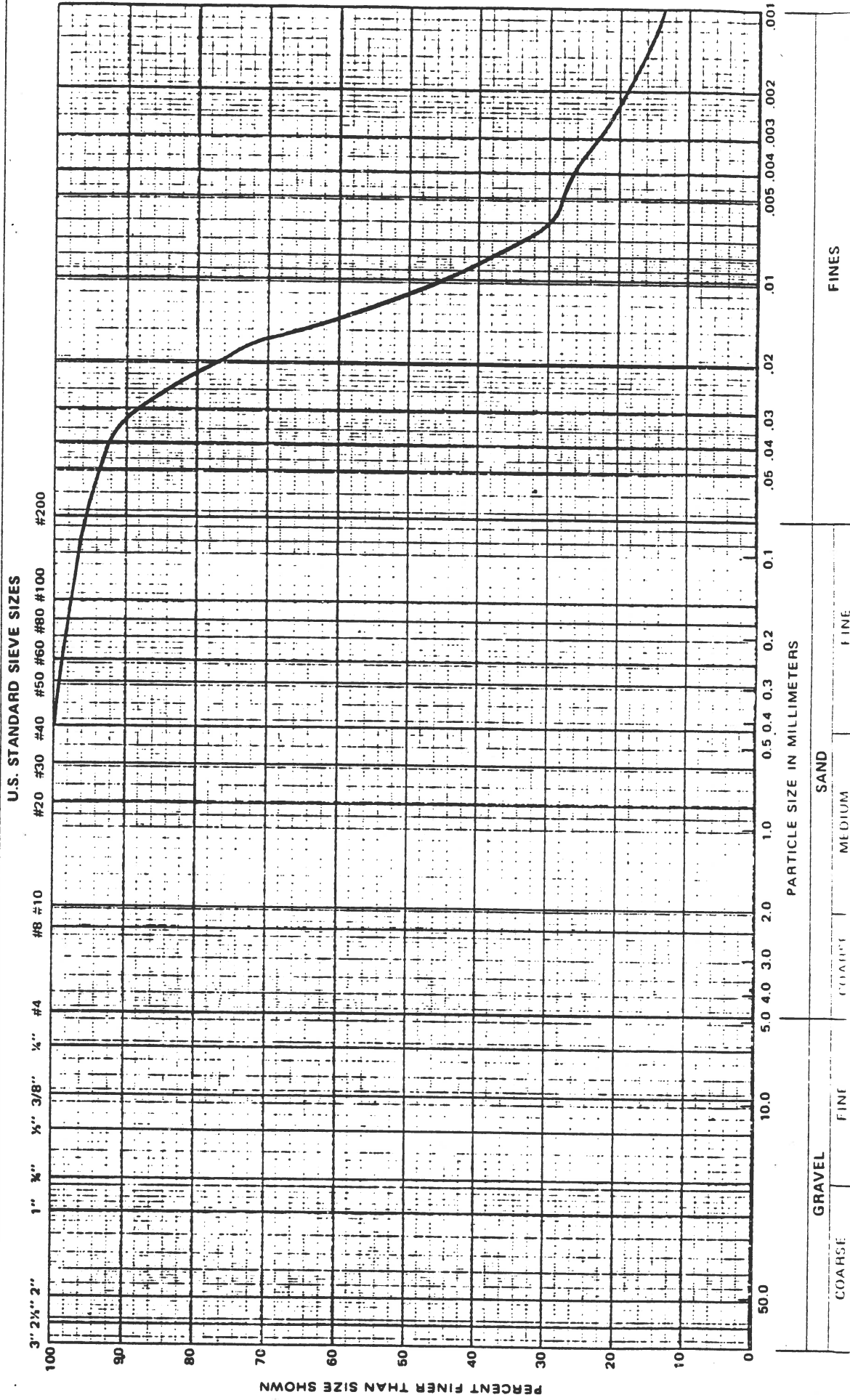
twin city testing
and engineering laboratory, inc.
662 CROMWELL AVENUE
ST. PAUL, MN 55114
PHONE 612/645-3601

Job No. 52-0688
Sample No. MDU Heskett #3 Dept.: 15'-16'
Classification (ASTM: D2487) CL-ML
Description SILTY CLAY

Project: SOIL TESTING FOR MDU HESKETT
POWER PLANT - MANDAN, NORTH DAKOTA

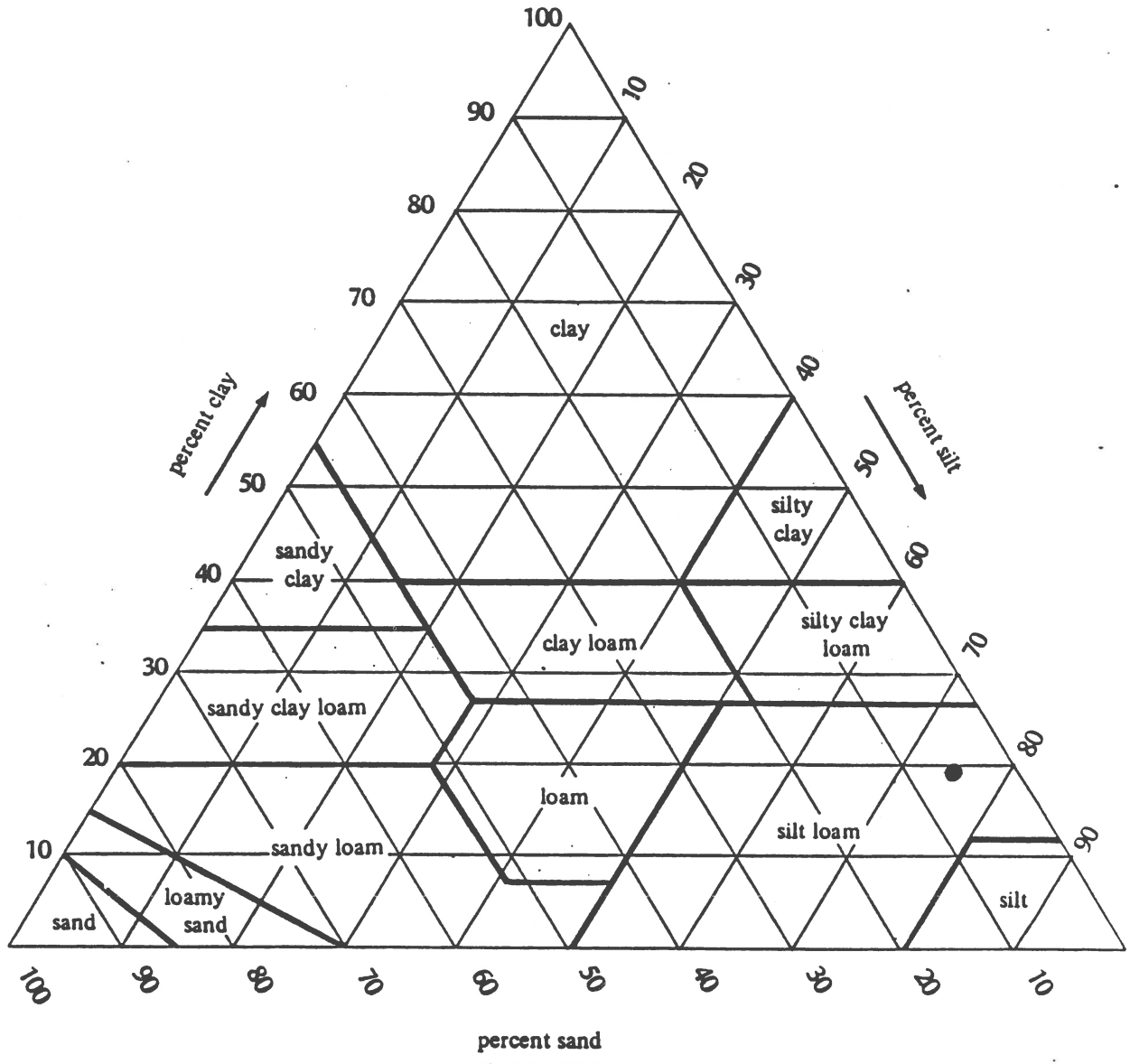
Reported To: Water Supply, Inc.

GRAIN SIZE DISTRIBUTION CURVE



USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #3, 15'-16'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

Size Range in Millimeters (Mean Diameter)												
75	2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008	
GRAVEL	SAND					SILT			CLAY			
	Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine	
	10	18	35	60	140	300						
U.S. Standard Sieve Numbers												

TWIN CITY TESTING LAB



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PHONE 612/645-3601

Job No. 52-0688

Sample No. MDU Heskett #3 Dept.: 19'-20'

Classification (ASTM: D2487) CH & CL

Description FAT CLAY & SILTY CLAY (Note: Distribution curve based on -10 material used for hydrometer test rather than total sample due to small boulder in a small sample.)

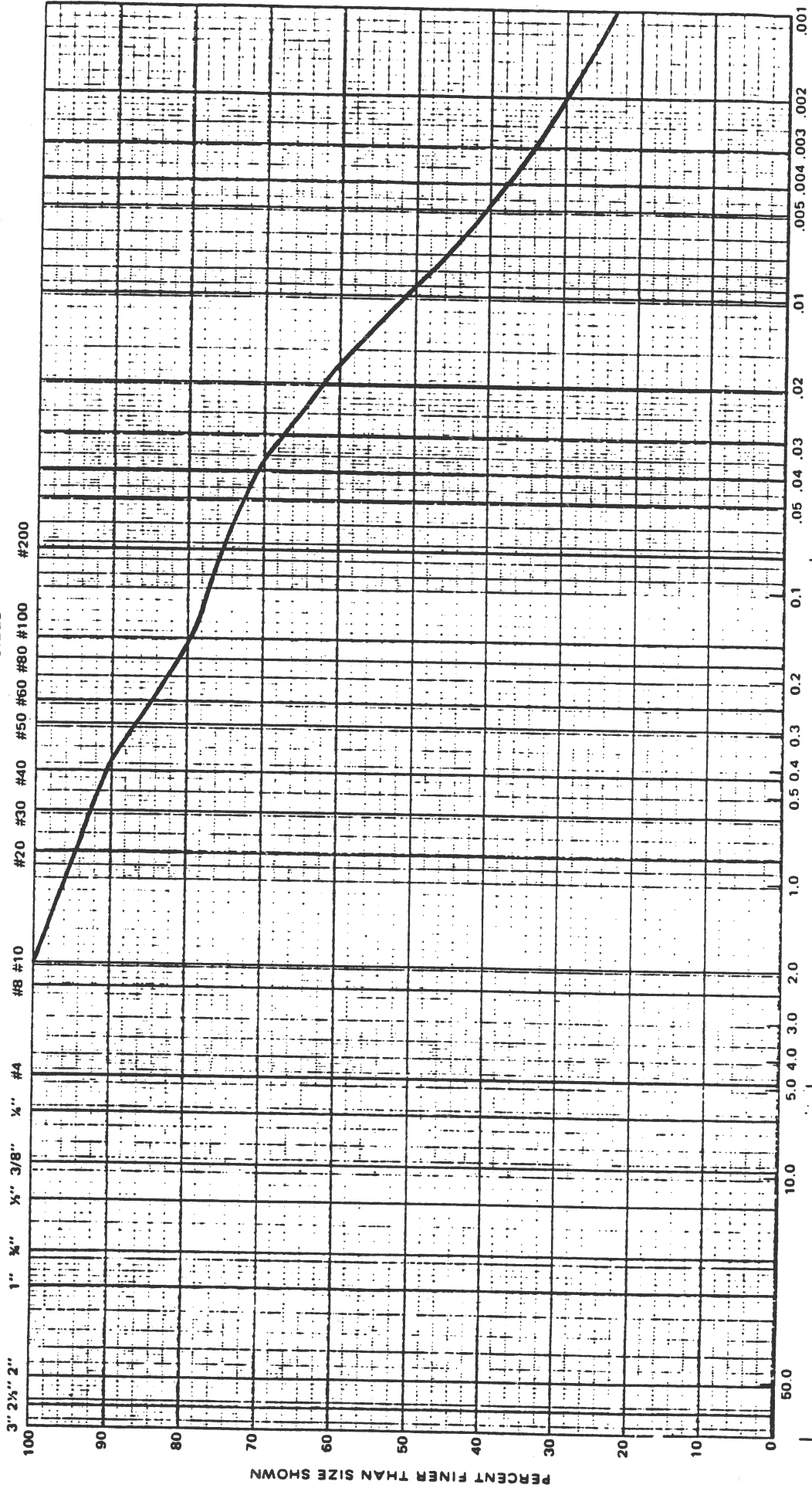
Project: SOIL TESTING FOR MDU HESKETT

POWER PLANT - MANDAN, NORTH DAKOTA

Reported To: Water Supply, Inc

GRAIN SIZE DISTRIBUTION CURVE

U.S. STANDARD SIEVE SIZES

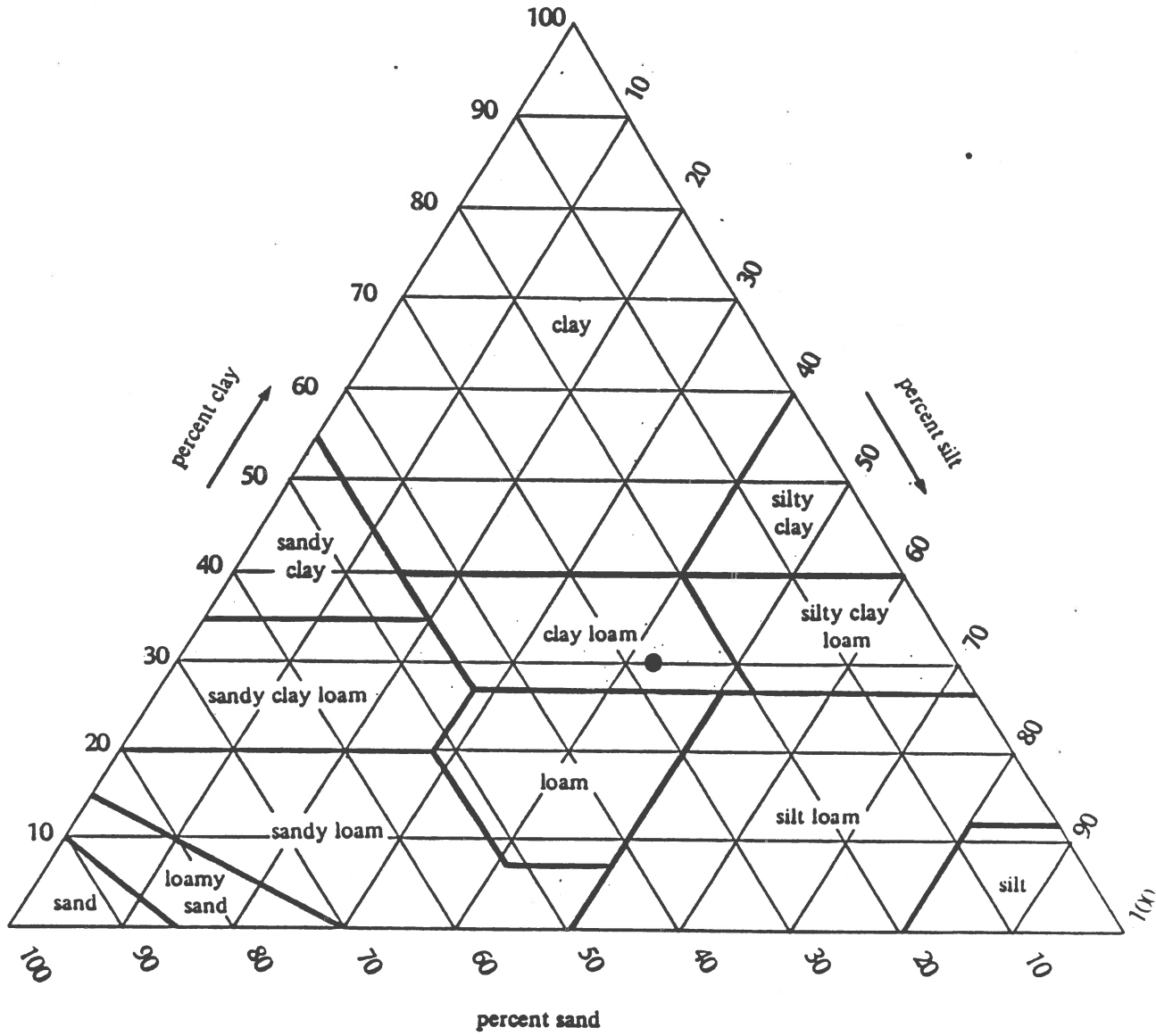


PARTICLE SIZE IN MILLIMETERS

GRAVEL: COARSE, FINE
SAND: MEDIUM, FINE
FINES

USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #3, 19'-20'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

Size Range in Millimeters (Mean Diameter)												
75	2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008	
GRAVEL	SAND					SILT			CLAY			
	Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine	
	10	18	35	60	140	300						
U.S. Standard Sieve Numbers												

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Job No. 52-0688

Sample No. MDU Heskett #3 Depth: 31' - 32'

Classification (ASTM:D2487) CL & CH

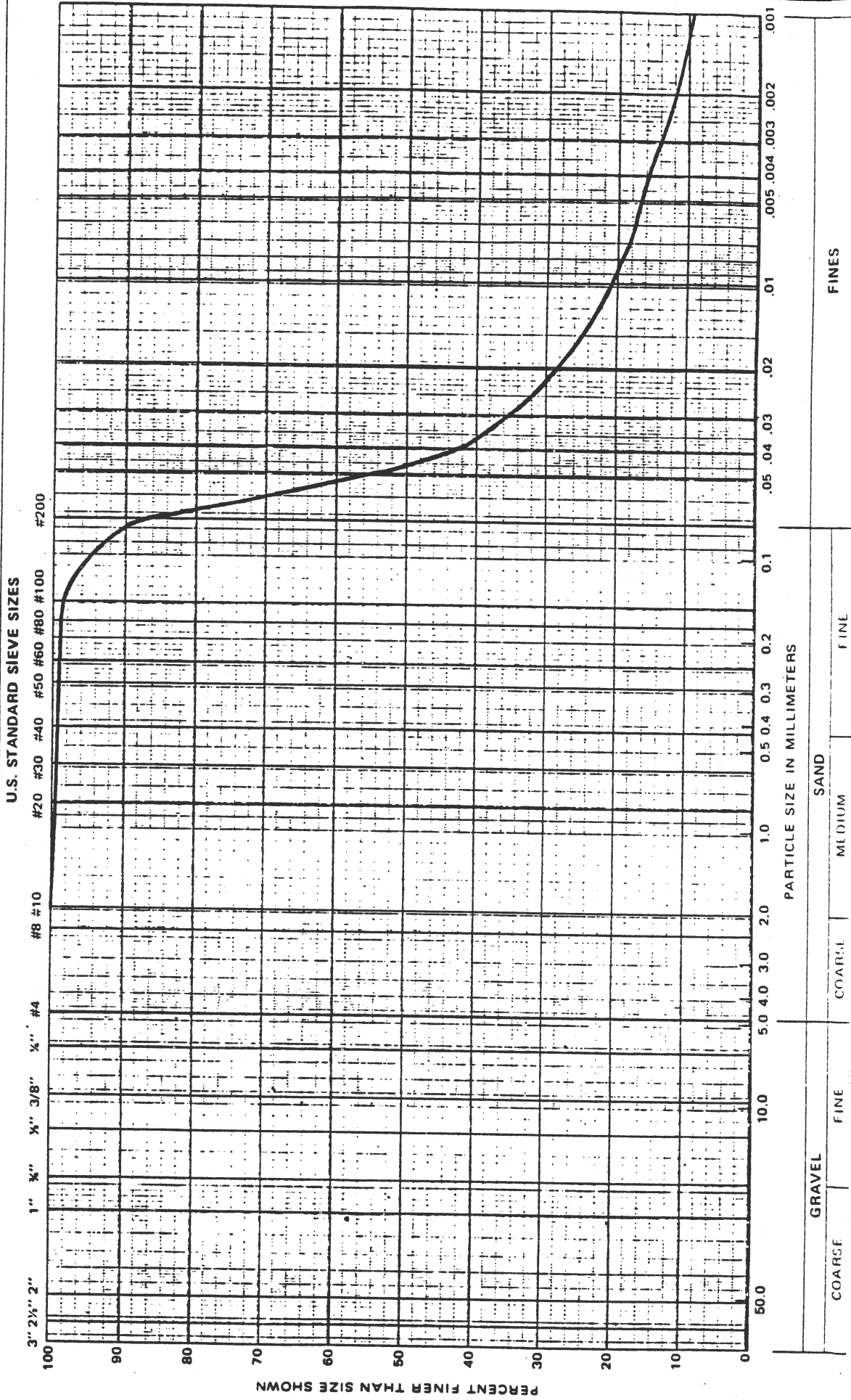
Description SILTY CLAY & FAT-CLAY

Project: SOIL TESTING FOR MDU HESKETT

POWER PLANT - MANDAN, NORTH DAKOTA

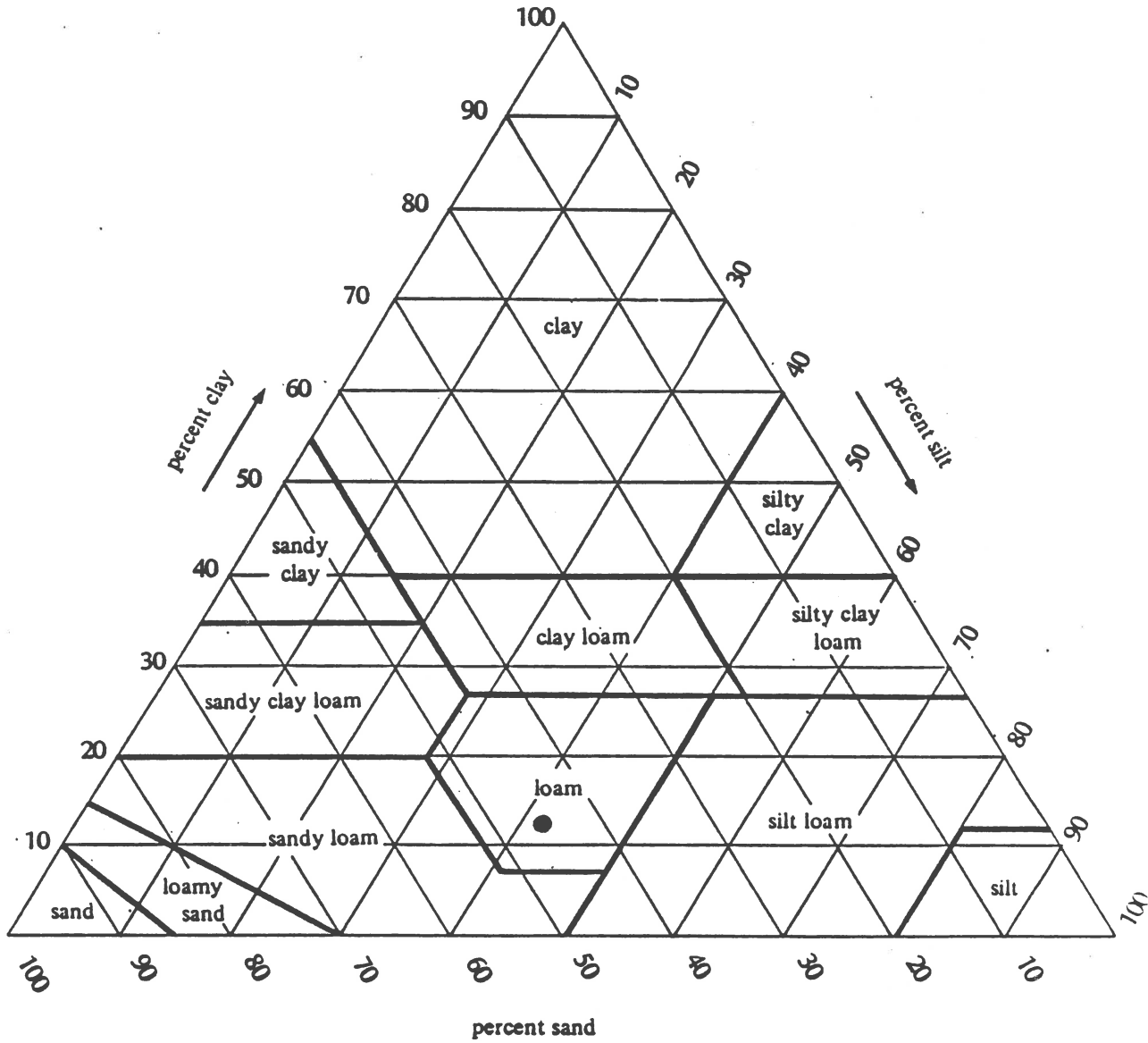
Reported To: Water Supply, Inc.

GRAIN SIZE DISTRIBUTION CURVE



USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #3, 31'-32'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

Size Range in Millimeters (Mean Diameter)											
75	2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008
GRAVEL	SAND					SILT			CLAY		
	Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine
	10	18	35	60	140	300					
U.S. Standard Sieve Numbers											

TWIN CITY TESTING LAB

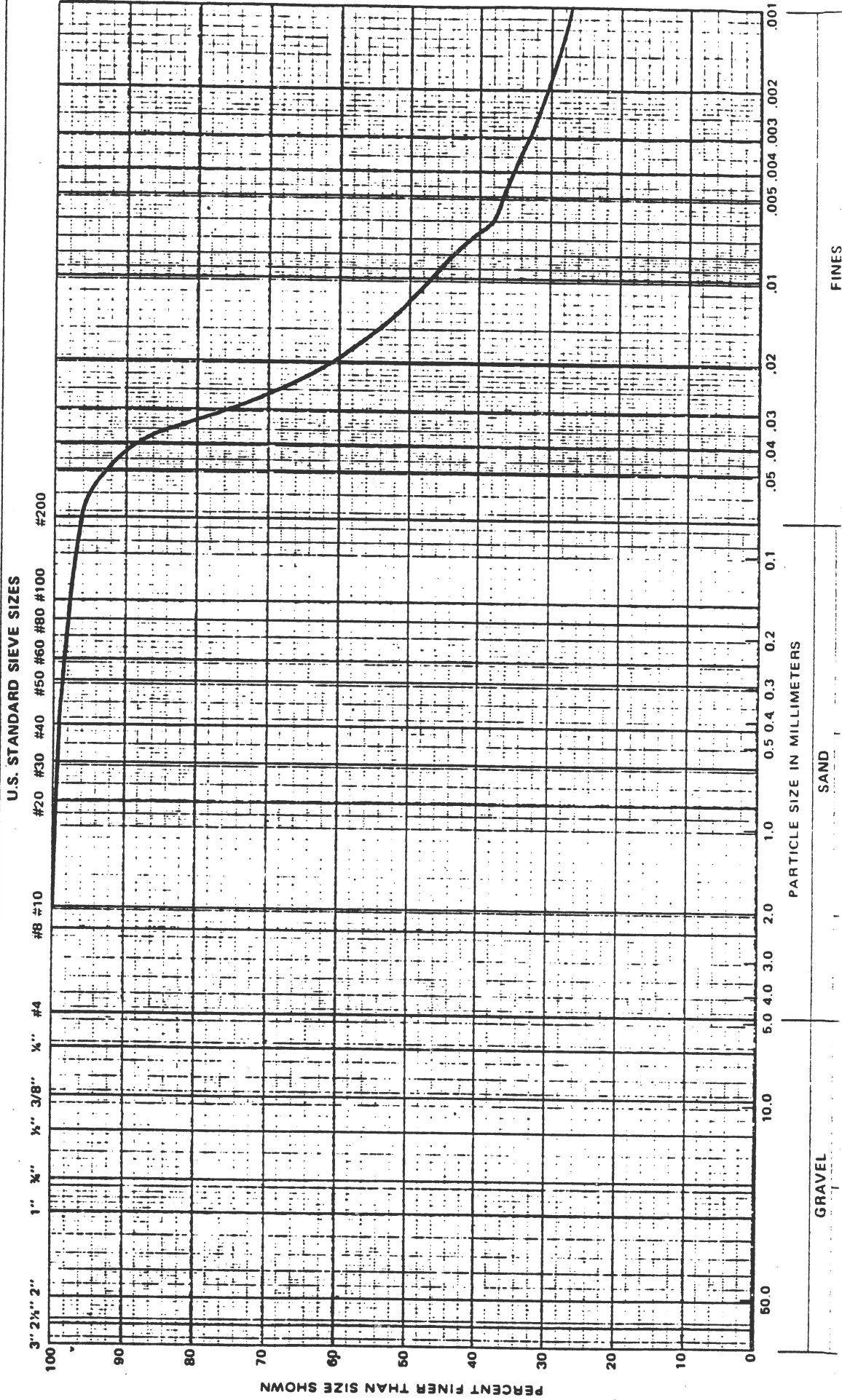


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and engineering laboratory, inc.
667 CROWELL AVENUE
ST. PAUL, MN 55114
PHONE 612/645-3601

Job No. 52-0688
SAMPLE NO. MDU Heskett #4 Dept.: 9' - 10'
Classification (ASTM: D2487) CH & CL
Description FAT CLAY & SILTY CLAY

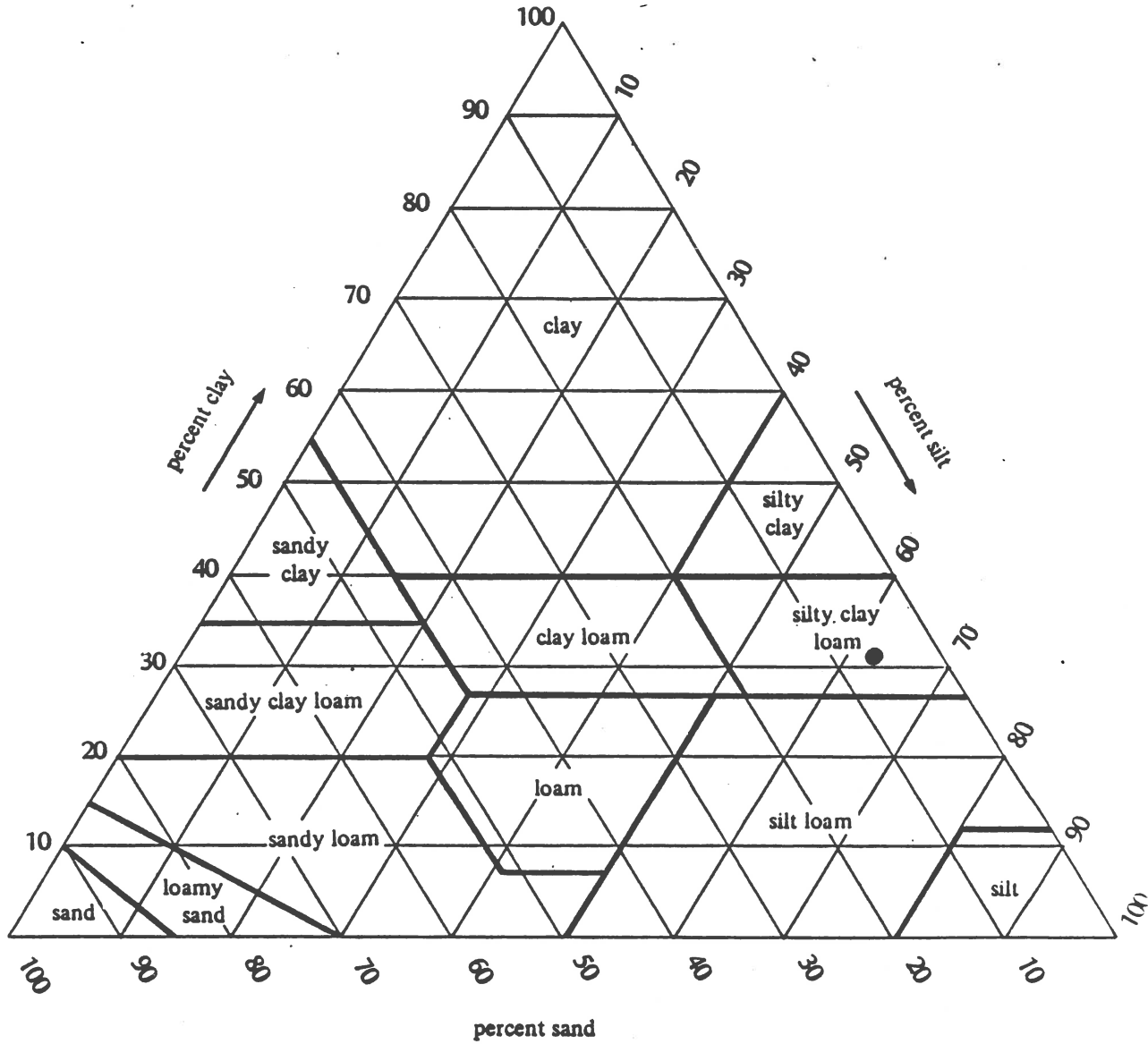
Project: SOIL TESTING FOR MDU HESKETT
POWER PLANT - MANDAN, NORTH DAKOTA
Reported To: Water Supply, Inc.

GRAIN SIZE DISTRIBUTION CURVE



USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #4, 9'-10'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

Size Range in Millimeters (Mean Diameter)												
75	2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008	
GRAVEL	SAND					SILT			CLAY			
	Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine	
	10	18	35	60	140	300						
U.S. Standard Sieve Numbers												

TWIN CITY TESTING LAB



Job No. 52-0688

Sample No. MDU Heskett #4 Depth: 15'-16'

Classification (ASTM:D2487) CL & CH

Description SILTY CLAY & FAT CLAY

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PHONE 612/645-3601

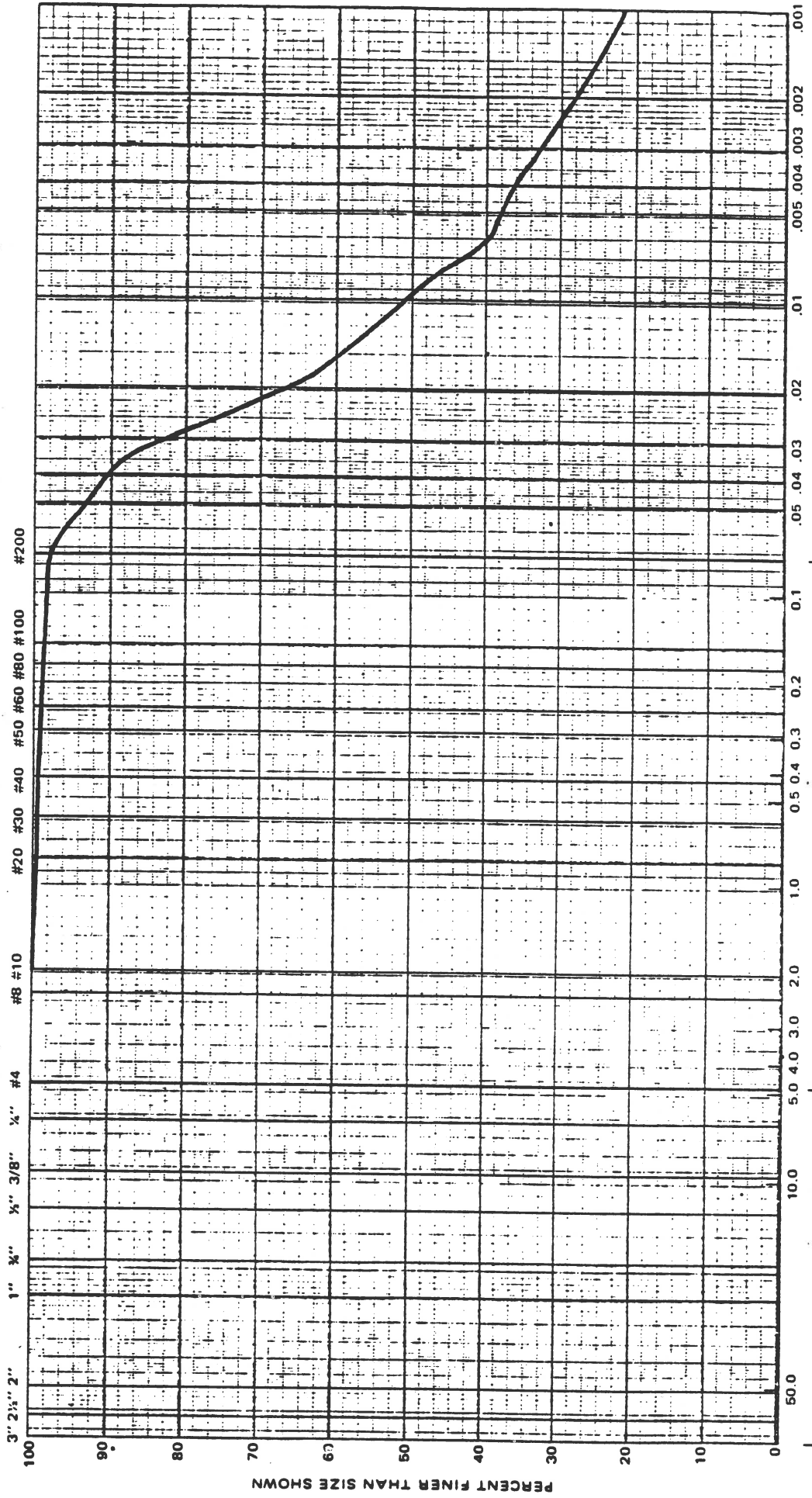
Project: SOIL TESTING FOR MDU HESKETT

POWER PLANT - MANDAN, NORTH DAKOTA

Reported To: Water Supply, Inc.

GRAIN SIZE DISTRIBUTION CURVE

U.S. STANDARD SIEVE SIZES



PARTICLE SIZE IN MILLIMETERS

GRAVEL

COARSE

FINE

SAND

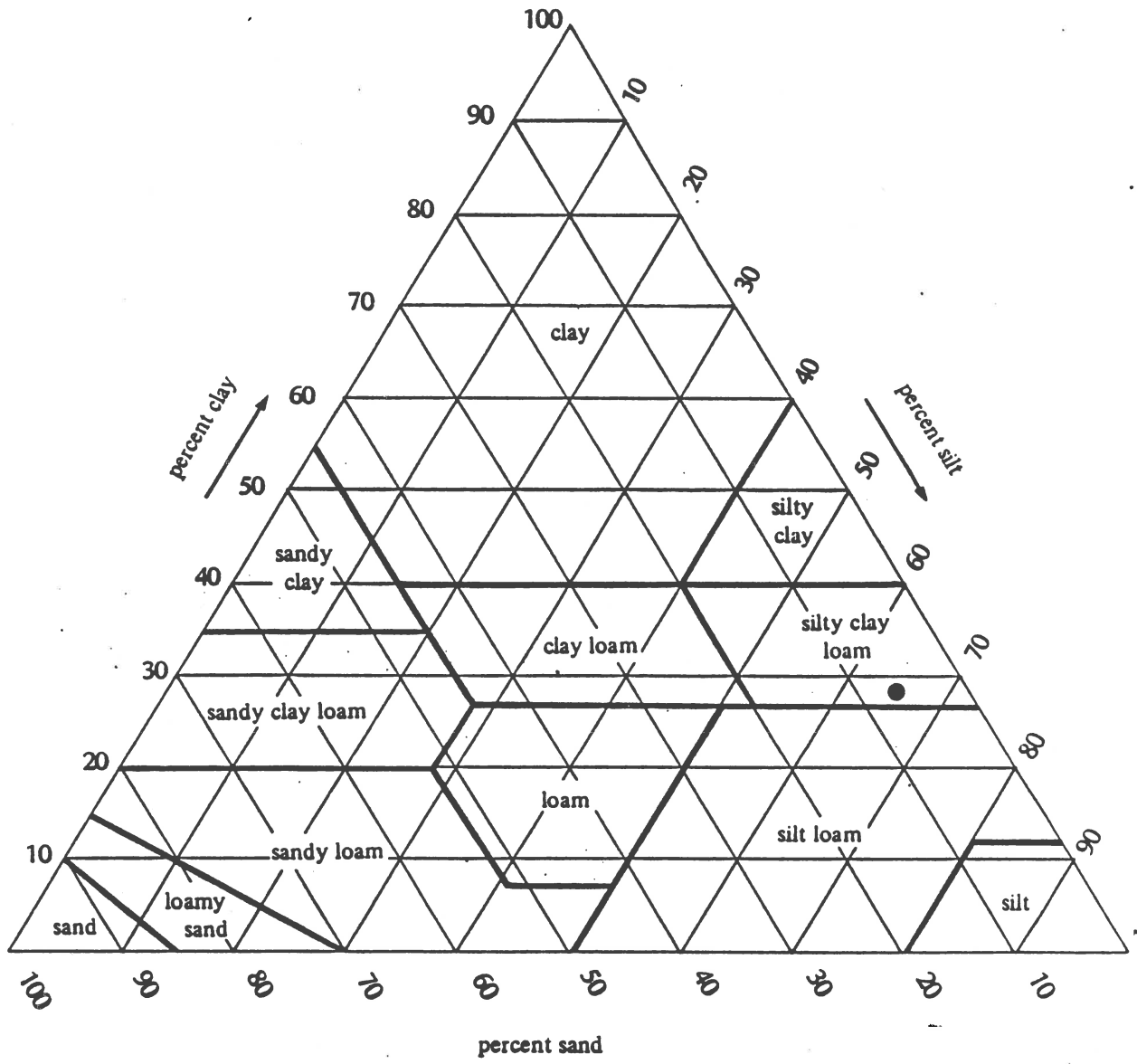
MEDIUM

FINE

FINES

USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #4, 15'-16'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

Size Range in Millimeters (Mean Diameter)

	2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008
GRAVEL	SAND					SILT			CLAY		
	Very Coarse	Coarse	Me- dium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine
	10	18	35	60	140	300					
	U.S. Standard Sieve Numbers										

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ST PAUL, MN 55114
PHONE 612/645-3601

Job No. 52-0688

Sample No. MDU Heskett #4 Depth: 31' -32'

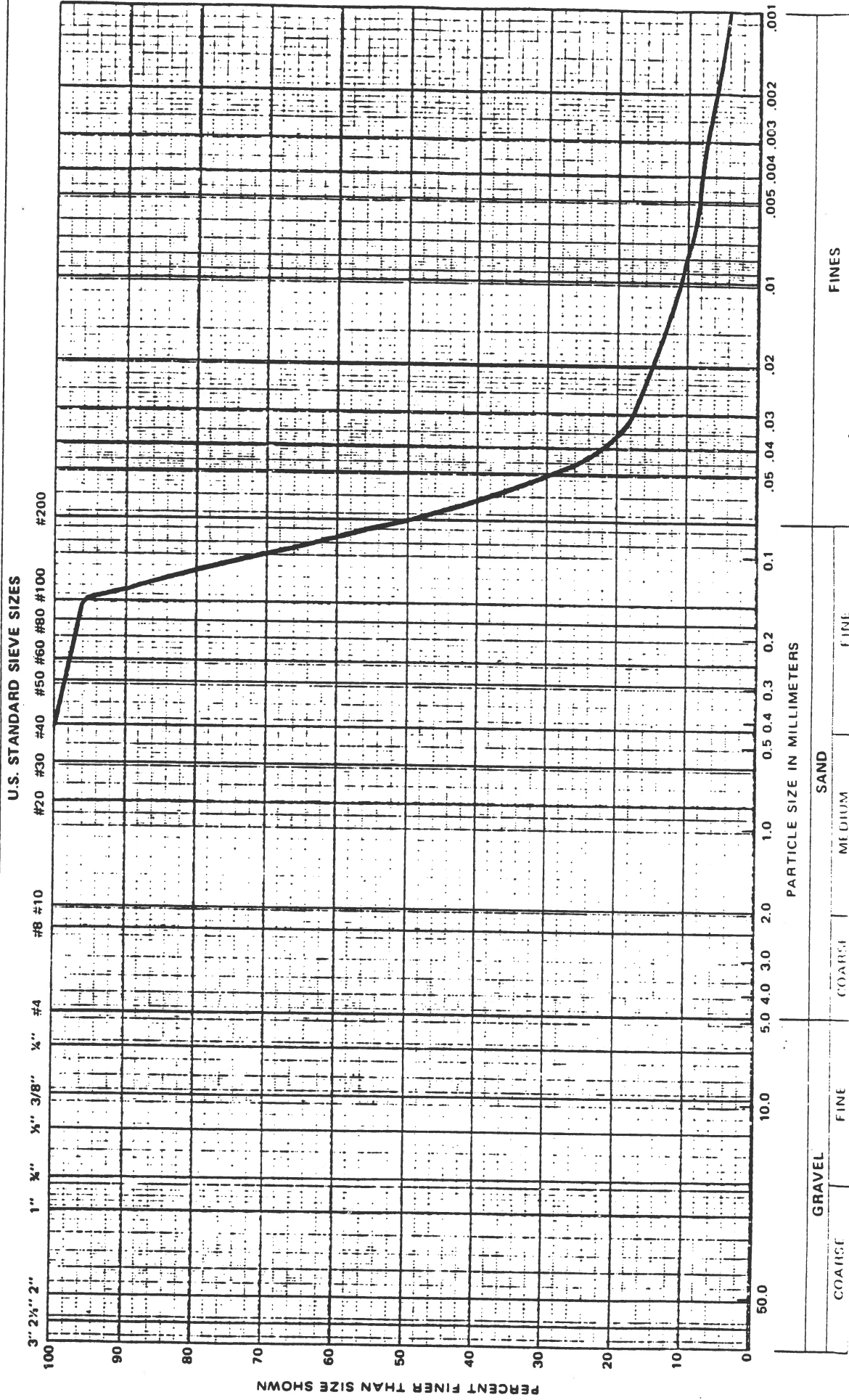
Classification (ASTM: D2487) SM

Description SILTY SAND, fine grained

Project: SOIL TESTING FOR MDU HESKETT
POWER PLANT - MANDAN, NORTH DAKOTA

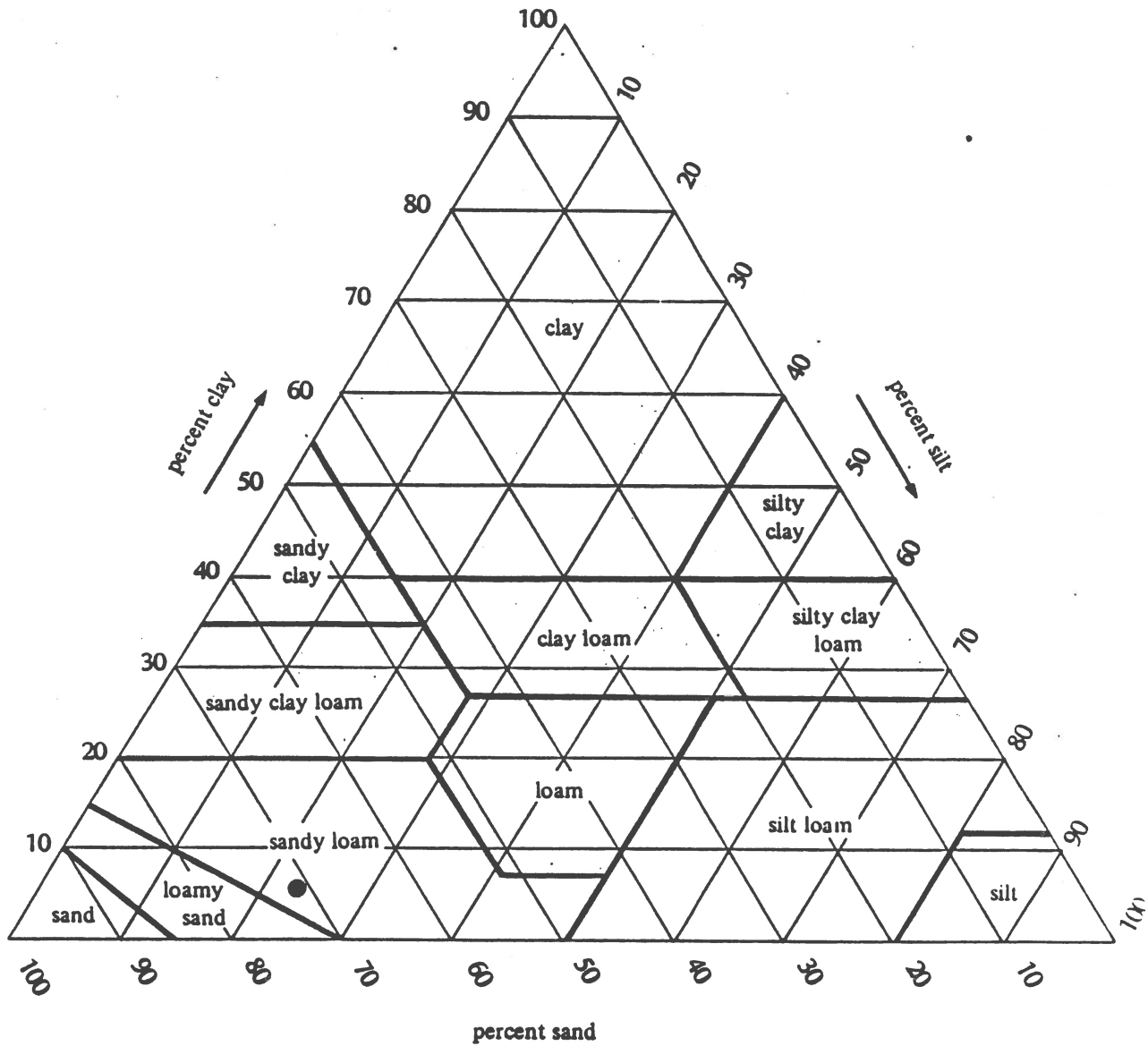
Reported To: Water Supply, Inc.

GRAIN SIZE DISTRIBUTION CURVE



USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #4, 31'-32'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

Size Range in Millimeters (Mean Diameter)												
75	2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008	
GRAVEL	SAND					SILT			CLAY			
	Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine	
	10	18	35	60	140	300						
U.S. Standard Sieve Numbers												

TWIN CITY TESTING LAB



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ST. PAUL, MN 55114
PHONE 612/645-3601

Job No. 52-0688

Sample No. MDU Heskett #4 Depth: 41'-42"

Classification (ASTM: D2487) CH-OH

Description SHALE, (Textural Classification-

tion: Organic Fat Clay)

Project: SOIL TESTING FOR MDU HESKETT

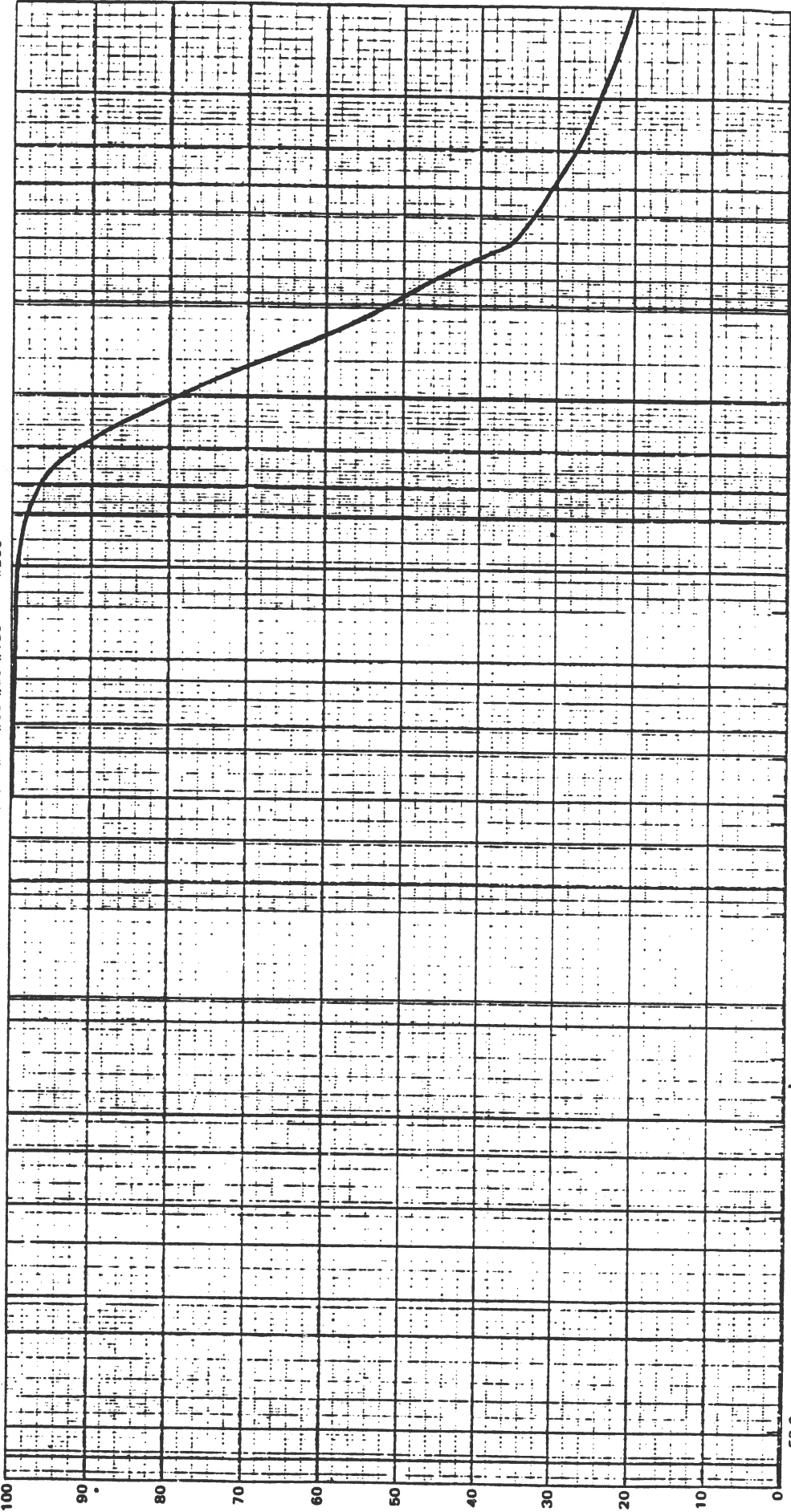
POWER PLANT - MANDAN, NORTH DAKOTA

Reported To: Water Supply, Inc.

GRAIN SIZE DISTRIBUTION CURVE

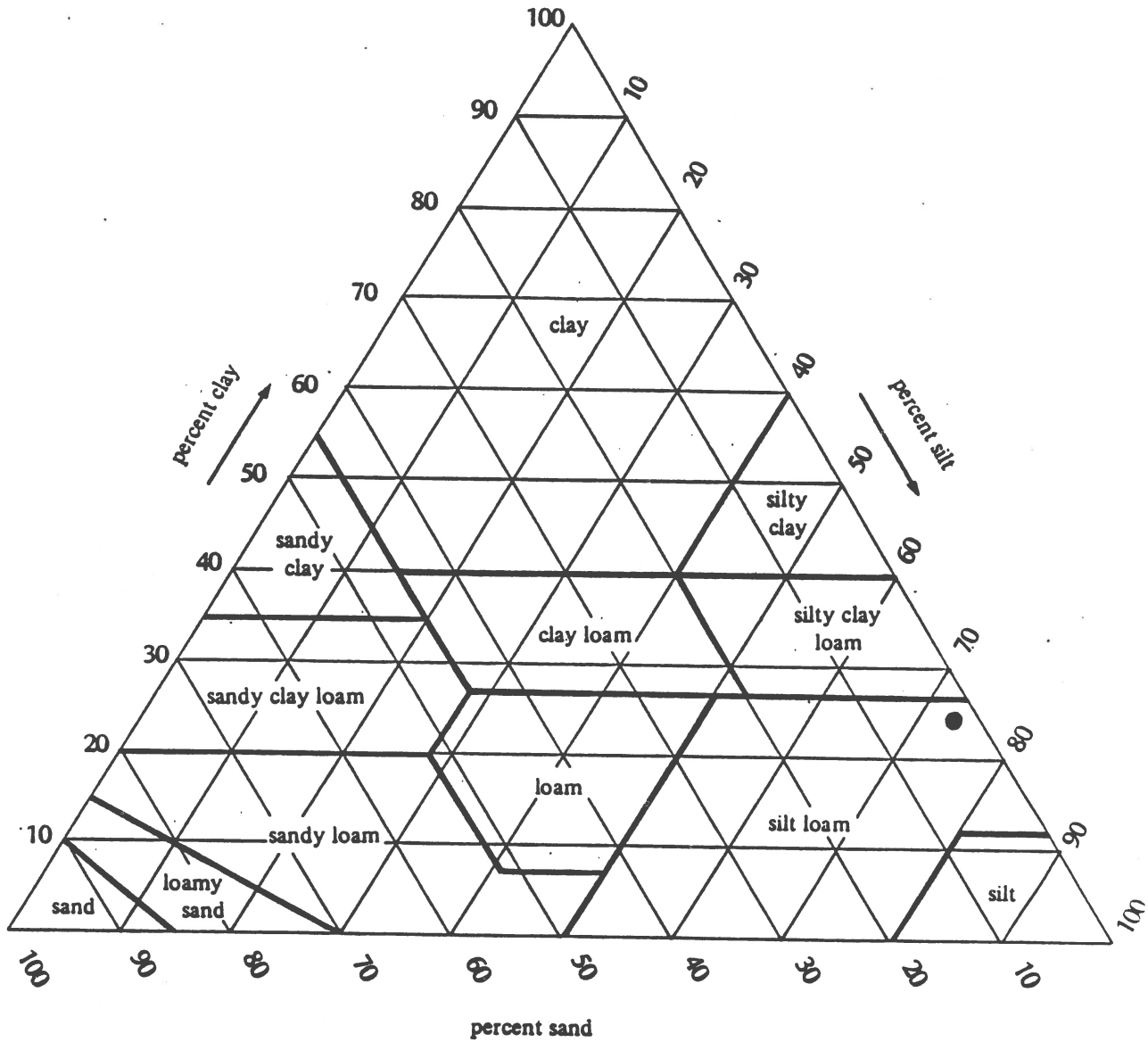
U.S. STANDARD SIEVE SIZES

3" 2 1/2" 2" 1" 3/4" 3/8" 1/4" #4 #8 #10 #20 #30 #40 #50 #60 #80 #100 #200



USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #4, 41-42'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

		Size Range in Millimeters (Mean Diameter)										
		2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008
GRAVEL		SAND					SILT			CLAY		
		Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine
		10	18	35	60	140	300					
		U.S. Standard Sieve Numbers										

TWIN CITY TESTING LAB



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PHONE 612-645-3501

Job No. 52-0688

Sample No. MDU Heskett #4 Dept. 51'-52'

Classification (ASTM: D2487) CL

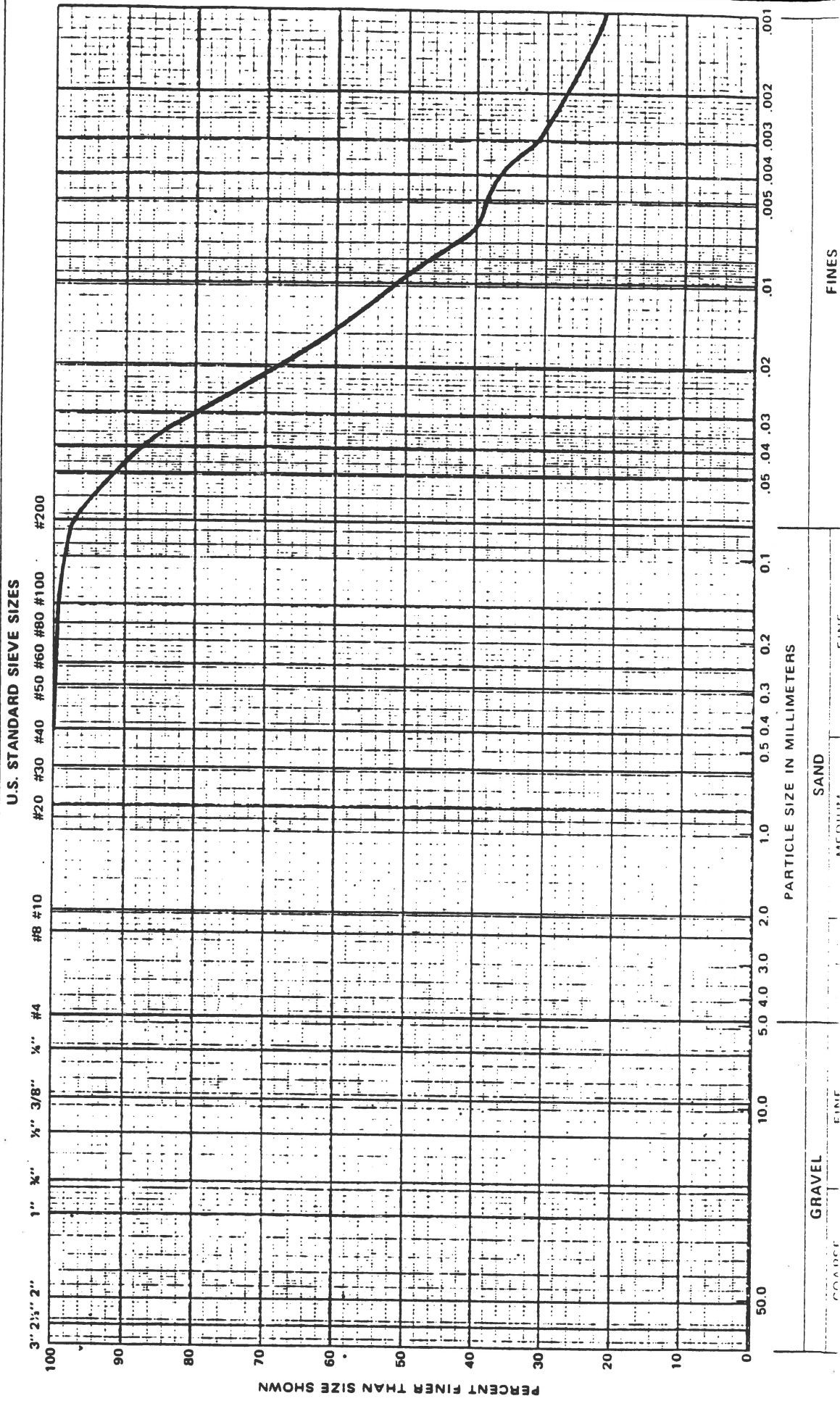
Description SHALE, (Textural Classification: Silty Clay)

Project: SOIL TESTING FOR MDU HESKETT

POWER PLANT - MANDAN, NORTH DAKOTA

Reported To: Water Supply, Inc.

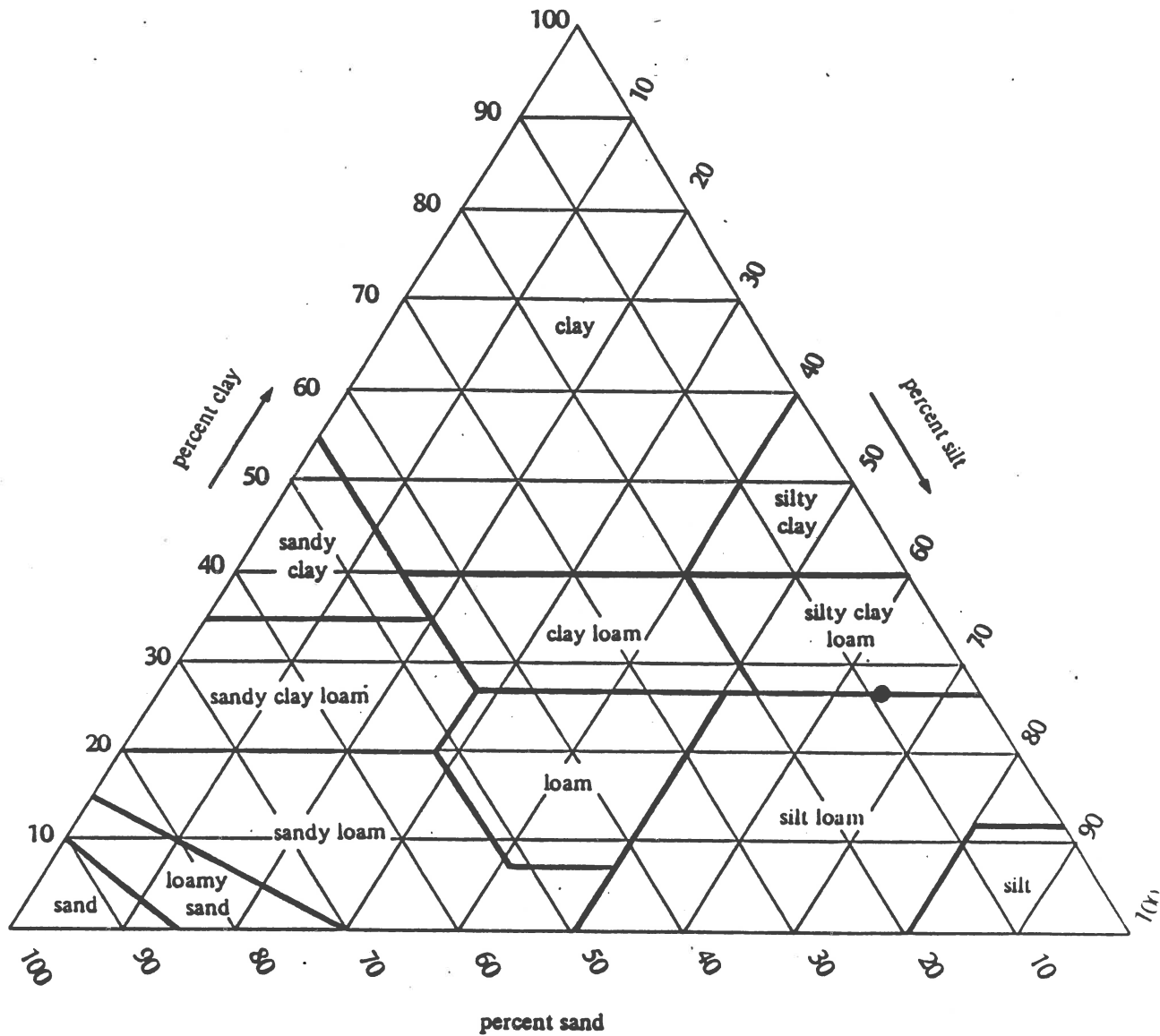
GRAIN SIZE DISTRIBUTION CURVE



PERCENT FINER THAN SIZE SHOWN

USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #4, 51'-52'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

Size Range in Millimeters (Mean Diameter)												
75	2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008	
GRAVEL	SAND					SILT			CLAY			
	Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine	
	10	18	35	60	140	300						
U.S. Standard Sieve Numbers												

TWIN CITY TESTING LAB

6.0 FACILITY CONSTRUCTION, OPERATION AND CLOSURE

6.1 Site Preparation and Construction

6.1.1 Access and Preconstruction

Exhibit 5-F presents soil information on the Heskett site currently available through the Morton County Agricultural Stabilization and Conservation Service office. Because this data was gathered from fieldwork conducted several decades ago and provides little site-specific soil depth information, a new soil survey will be commissioned. The survey will be conducted prior to the onset of construction and cover the entire permit area. Soil profiles will be developed identifying soil types and topsoil (A horizon) and subsoil (B horizon) depths. This information will be used to establish plant growth material (SPGM) salvage and replacement depths during future construction and reclamation activities.

Surface water drainage of adjoining land east of the site will be improved by the permanent installation of a grass-lined ditch (Exhibit 6-B). This drainageway will be located along the base of an existing draw and enhance movement of surface runoff waters and permitted discharges from impoundments located to the south on Amoco Refinery property. The drainageway will be about 8 feet deep, 8 feet wide at the base, and provide a slope of 1% to a discharge at Rock Haven Creek. Existing surface water drainage patterns should not be significantly altered by this installation.

Primary access to the site will be along a dedicated haul road extending eastward to Heskett Station (Exhibit 6-B). Roadbed construction will require 34,500 cy of excess earthen material removed during the excavation of the initial disposal slot. The road surface will be covered with

gravel to allow all weather access to the site. All haulage road construction activities will be performed on Montana-Dakota property and will not interfere with traffic on surrounding public roads.

Other points of access to the site will be restricted by the installation of a lockable personnel fence around the perimeter of the facility. Public access to the site will not be allowed.

6.1.2 Facility Construction

The first phase of the facility described in Exhibit 6-B will be constructed and made operational during the 1989 earthwork construction season. Waste placement will begin upon the completion of the initial waste disposal slot. To minimize impacts to the landscape and reduce potential fugitive dust and leachate generation, new disposal trenches of similar design will be excavated approximately every other year. Filled trenches will be closed and reclaimed concurrently with new trench construction

The 47 acre disposal facility will be developed in two phases. Phase I, comprising the disposal area on the north side of the haul road, will provide about 13 years (approximately 700,000 cy) of disposal capacity. The initial disposal slot will be constructed along the western edge of the Phase I area. Subsequent excavations will proceed eastward until the Phase I area is filled. Phase II of the disposal site lies south of the haul road and will provide disposal capacity for about 15 years (approximately 600,000 cy). Phase II development (Exhibit 6-C) will begin parallel to the southern edge of the haul road and proceed southward. The final trench excavation at the site will lie parallel to the southern edge of the site. It is not currently expected that ash will be placed directly beneath the on-site portion of the

haul road. However, ash emplacement beneath the road may be considered as a contingency if needed.

Exhibit 6-D provides information regarding earth quantity movements for each disposal trench. These estimates (and the subsequent size of the trenches) may be adjusted somewhat if ash waste generation rates markedly differ from projections. The initial slot of Phase I will be constructed to contain slightly over one year of waste (60,000 cy). Subsequent trenches will be constructed to contain all ash generated during the ensuing one to two years.

All construction activities will be performed during the normal earthwork construction season. Equipment such as bulldozers, scrapers, graders, and compactors will remove, modify, and/or replace earthen materials. Most material excavation and relocation operations will rely upon scrapers.

Each trench will have a compacted in-situ clay liner along its base to restrict downward migration of in-pit liquids. Available information (see Exhibits 5-E and 5-K) indicates an abundance of naturally occurring clay and silt which will be uncovered in conjunction with trench excavations. These materials will be scarified to a depth of 18 inches and recompact to a permeability of not more than 1×10^{-7} cm sec⁻¹. Occurrences of sand or gravel will be removed and replaced with clay-rich spoil. In-situ materials providing marginally acceptable rates of permeability will be replaced, treated with a soil liner admixture such as bentonite, or thickened to provide the equivalent permeability of 18 inches of 1×10^{-7} cm sec⁻¹ material. The in-situ liner will cover the entire floor of the trench, the liquids collection sump, and be extended to include the lower five feet of the trench sidewall. Liner installations associated with new trench construction will be keyed into the previous trench liners, thereby providing contiguous liquids

6.1.3 Excavated Materials

The removal and stockpiling of suitable plant growth material (SPGM) will be completed prior to any operation which would interfere with the use and integrity of the top soil. Top soil thickness information provided by the soil survey (see Section 6.1.1) will be used to establish SPGM salvage depth. SPGM will be removed by scraper in two lifts; soil horizon A will be removed in the first lift, soil horizon B will comprise the second lift. Each lift will be separately stockpiled in an area described in the Site Plan of Exhibit 6-B. Because filled trenches will be closed in conjunction with new trench construction, removed SPGM shall be stockpiled only when it is not practical for direct placement in areas concurrently undergoing reclamation.

Exhibit 6-D projects the amount of earthen materials which will be excavated. The largest single Phase I excavation (59,000 cy) will be the initial trench construction. Resulting excess materials from drainage ditch and disposal slot excavation will be used in the construction of the access road, evaporation pond, and a permanent visual obstruction berm along the southern perimeter of the site. Excess spoil may be diverted to the closure of the adjacent Heskett ash pile if available. Because future excavations will generate volumes of materials which approximate requirements for closure (i.e., cap construction and overburden placement) relatively little material should require stockpiling along the western edge of the site. Stockpile Area No. 1 and 2 may be converted into an additional visual obstruction berm if excess spoils require permanent dislocation from the reclamation area.

All temporary SPGM and clay material stockpiles will be maintained in a manner which minimizes the effects of erosion yet maintains soil integrity. Protective measures will be applied and include the planting of cover crops, mulching, use of chemical binders, contour tillage, or other site specific

infiltration protection. Verification of construction quality and attainment of proper rates of permeability will be made by an independent registered professional engineer.

Each trench floor will be positioned to provide at least five feet of separation between the waste and the 1986 water table elevation. Additionally, the base of each slot will be contoured to provide a positive drainage slope of not less than 1% both laterally and lengthwise, thus promoting rapid movement of in-pit liquids away from the waste and into the collection sump.

Exhibit 6-C, Section X-X illustrates a typical cross-section of the leachate collection pipe which will be permanently installed with each new trench. A perforated pipe will gather liquids from the operational and closed portions of the facility and discharge them into the liquids collection sump in use at that time. Liquids will continue to be gathered by the collection line after the closure of Phase I and discharge directly into the evaporation pond. Waste leachates collected by the Phase II line will not discharge into the active sump but rather directly into the evaporation pond.

All liquids collected within the pit sump and leachate collection lines will be evaporated in a 53,000 square foot evaporation pond (Exhibit 6-B, Section D-D). This pond will be constructed to contain in-pit liquids resulting from normally-occurring rainfall plus a single 24 hour 2.5 inch precipitation event. The evaporation pond will have 5 foot side walls and be equipped with a three foot thick clay liner possessing a permeability of not more than 1×10^{-7} cm sec⁻¹. The evaporation pond will service the disposal facility throughout the operational life of the site.

treatments. Annual cover crops may be planted in areas of frequent stockpile disturbance if necessary to control wind and water erosion. Obstructional berms will be permanently reclaimed to native grasses as soon as possible after completion.

6.2 Operation and Management

6.2.1 Waste Placement

Coal combustion ash will be loaded onto trucks and slightly wetted for dust control before transportation to the disposal site via the ash haul road. Haulage will take place daily during daylight hours; only in emergencies will ash haulage occur after nightfall. Spilled waste material on the haul road and at the site will be immediately cleaned-up and placed in the disposal trench. Ash waste will not be temporarily stored at the site prior to disposal.

Haul trucks will enter the trench by way of ramps located at the end of the trench with the highest elevation (Exhibit 6-B, Operational Schematic). Waste will be initially placed in each trench near the ramp and expanded to provide a surface for unloading activities. Vehicular traffic upon the disposal slot floor will be held to a minimum to reduce inadvertent liner damage. Dumped waste will be leveled with a front end loader and spread across the trench floor in lifts 5 to 8 feet thick. The active sump area will not be filled with waste. Ash will not be dumped from the pit highwall into the trench.

Because initial disposal activity will be conducted at an elevation below ground surface the waste will receive only moderate exposure to surface winds. Consequently, little fugitive dust is expected to be generated. As

the waste elevation increases, however, strong surface winds might produce increasing amounts of airborne nuisance particulates. Dust suppression measures will be implemented as required to control fugitive dust. These measures will include the selective placement of AFBC bottom ash (a relatively low dust emitting material) over other ash wastes or the thin spreading of earthen or other dust control material. A 2,500 gallon water spray truck is available for dust control applications over the ash haul road. Water spray will not be used for dust control over the disposed of waste.

Montana-Dakota personnel will perform all daily operational monitoring and disposal activities at the site. Facility points-of-contact are:

Station Superintendent - Duane Steen

Fuel and Grounds Supervisor - Darhl Bowers

Facility Telephone - (701) 663-9576

The Fuel and Grounds Supervisor (or his designee) at Heskett Station will have general supervision of the site and verify that procedures specified in this permit application are adhered to. The site will be monitored daily in conjunction with normal ash haulage activities. Weekly log entries will be made concerning the amount of ash hauled, waste-contaminated water transferences, and unusual operational occurrences such as waste spillages or failures in site reclamation. Corrective actions will also be noted.

6.2.2 Surface Water Management

Ground surface runoff waters will be prevented from entering the pit by either a positive slope away from the edge of the pit or the construction of diversionary trenches or berms. Uncontaminated ground surface runoff waters

will not be controlled at the site except in instances where erosion and/or sedimentation is occurring. Waste spillages at the site and on the haul road will be immediately cleaned-up after each incident; consequently no contaminated waters should be generated in these areas. The ash haul road will be graded to promote surface water run off away from the active disposal area (see Exhibit 6-B, Section b-b and Exhibit 6-C, Section b-b) and into the drainage ditch.

The in-pit sump will hold all meteoric-source precipitation falling within the trench (both waste contacting and non-contacting liquids) and infiltrated water gathered by the leachate collection line (Phase I only). Each collection sump will be sized to provide 100% retention of normal rainfall plus one 2.5 inch precipitation event occurring in a 24-hour period. The sumps will be equipped with an 18 inch compacted clay liner similar in design to the rest of the pit floor. When accumulated liquids approach 3 feet in depth (see Exhibit 6-B, Section X-X), the liquids will be transferred to the evaporation pond. It should be noted that restraints regarding weather, accessibility, equipment or personnel availability may occasionally change the 3 foot liquids volume transfer standard.

Liquid transfer to the evaporation pond will be performed through the use of a portable pump and an overland pipe constructed of PVC or similar material. Pumping activities will normally be conducted during periods of ash haulage and will be continually monitored for leakage during operation. Pumping will not be performed at night or during freezing conditions which could damage the pipe.

Minimal care should be required around the evaporation pond. Surface discharges will not be made from the pond. Growth of vegetation in the impoundment will be controlled through additions of herbicide or mechanical

cutting whenever damage to the clay liner is considered likely. The pond will be monitored monthly for evidence of deterioration and leakage. The groundwater monitoring plan provides for the installation of a water table elevation and quality monitoring well immediately downgradient of the impoundment. Samples of impounded liquids will be taken (if available) semi-annually in conjunction with the groundwater sampling program and analyzed for the same chemical parameters. Surface impoundment analytical data will be combined with the groundwater quality information and submitted to the NDS DH according to the schedule specified in Section 7.3

6.2.3 Contingencies and Potential Impacts

The proposed waste facility was sited and designed to reasonably ensure that groundwater will not intrude upon the waste. Two consecutive years of potentiometric monitoring has shown a relatively stable water table elevation with little apparent seasonal fluctuation. This general stability, even during the severe drought of 1988, might be partially attributable to constant upgradient recharge provided by surface impoundments on Amoco Refinery property to the south. Discussions with Amoco personnel has indicated there are no proposals to expand or otherwise modify this impoundment system.

The facility will be located over a marginal groundwater resource. Groundwater chemical characterizations (Exhibit 5-J) indicate it to be of comparable quality with the waste leachate (Exhibit 2-A). Furthermore, recent studies (referenced in Section 5.2.4) have shown that heavy metals which exist in the leachate (such as arsenic, cadmium, and lead) are effectively attenuated by clay and silt materials which naturally occur in abundance throughout the Heskett Site. The Cannonball Formation water at the Heskett Site is unsuitable for most domestic or agricultural purposes without prior

purification. Area residences rely upon other underlying aquifers such as the Ludlow for their domestic water supplies. Consequently, the proposed facility will not pose a threat to a desirable groundwater resource. Indeed, even major releases of Heskett ash leachate to the underlying groundwater might be expected to result in only minor deviations from normal background chemical makeup.

A number of simple remedial measures are available at the site should groundwater elevations rise to intrude upon the waste, thereby endangering an area resource. Because Rock Haven Creek on the west and north of the site, along with the small draw located to east, already provides natural points of surface discharge to a rising groundwater table, modification to these topographic depressions or the installation of a shallow subsurface drainage system in their vicinity would serve to allow groundwater discharge at a lower elevation. This would serve to permanently lessen the potentiometric level of the water table. Increasing the depth of the drainageway might be particularly appropriate due to its close proximity to the lowest point of waste placement (i.e. the eastern edges of Phases I and II). Another option includes the permanent installation of a subsurface drainage pipe or french drain five to eight feet below the southern edge of the last Phase II trench. Such a system would intercept the groundwater below and upgradient of the waste and divert flow laterally to a discharge point on the drainageway. This would hydraulically isolate the waste.

An in-pit leachate collection system will be constructed to detect and gather in-waste liquids that would occur during the operational life of the site. Significant leachate collections may extend the life of the gathering pipes (and evaporation pond) beyond the site closure date until the problem is remedied. The in-pit sump and evaporation pond will have compacted clay

liners to assure minimal rates of subsurface leachate migration. The evaporation pond will be monitored monthly to determine liquids volume and detect evidence of deterioration, erosion, seepage, or overtopping. The in-pit collection sump will be similarly inspected weekly and after precipitation events. Should a sudden drop occur in the liquids level of the impoundment or groundwater quality monitoring indicate significant leakage is occurring, repair or replacement of the liner with a soil-based or admixed liner will be performed. Similarly, the size of in-pit collection sumps will be expanded in subsequent trench excavations should it become apparent that more retention volume is needed.

Provisions have been made which allow for visual and acoustical obstructions (earthen berms and tree shelter belts) between facility operations and residences to the south. Additional tree plants and berm construction (depending upon materials availability) may be emplaced around the facility perimeter at a future date. Shelter belts or berms will not be placed over waste disposal areas. Decisions regarding these features will be made after the facility becomes operational and their need at a specific location becomes apparent. Dust control measures (as described in Section 6.2.1) will be implemented until these features become permanently established.

6.3 Closure and Reclamation

6.3.1 Closure Methods

As each trench is brought to its final waste elevation, a 1 to 3 inch layer of earthen material will be applied to the waste if fugitive waste dust requires suppression. New trenches will be first constructed adjacent to the

disposal area intended for closure. Excavated materials from the new trench will be used to close the waste filled trench. Excess excavated material may be temporarily stockpiled in the area described in Exhibit 6-B or used in permanent berm construction. Similarly, new trenches providing inadequate volumes of earth for closure work will require withdrawal from stockpiled inventories.

A two-foot thick compacted clay cap will be constructed over the waste (Exhibit 6-C, Sections A-A and B-B). The cap will be developed from clay-rich spoil materials such as those documented in Exhibit 5-K. Earth moving equipment such as bulldozers, scrapers, graders, and compactors will emplace materials so that compaction of approximately 95% of maximum dry density and a permeability of 1×10^{-7} cm sec⁻¹ or less is attained. If available materials cannot provide for a two-foot thickness of 1×10^{-7} cm sec⁻¹ permeability, cap thickness will be increase commensurably and/or treated with an admixture to a point which affords equivalent moisture infiltration protection. Verification of adequate construction quality and permeability will be made by an independent registered professional engineer.

Uncompacted spoil will be immediately spread over the completed clay cap and shaped to prevent surface water ponding. Surface slopes will range from 4% to 10%. Spread depth will be adequate to create a total earthen material profile above the waste (i.e., clay cap, uncompacted spoil, and SPGM) of not less than eight feet.

SPGM will be spread over the spoil material at a uniform depth determined by material availability. The respread will be done in accordance with currently accepted practices and procedures which assure proper interlift adhesion. Compaction of materials will be held to a minimum.

The final Phase II trench closure (thus leading to final site closure) will include the removal of the waste haulage road surface and the evaporation pond. All waste-contaminated material will be placed with the waste in the final disposal trench. Disturbed areas will be shaped to the topography illustrated in the site plan of Exhibit 6-D and reclaimed. The leachate collection lines will be abandoned in-place and will not be monitored or maintained. Points of access to the leachate collection line will be sealed during final closure for purposes of safety. The drainageway will not be modified or restored to original contours during or after final closure of the site unless deemed necessary at the time.

6.3.2 Reclamation

SPGM will be sampled and tested to determine soil nutrient status. Fertilizer application recommendations will be solicited from a soil testing laboratory and utilized in consideration of existing soil properties, topography, seed mix components, and practical experience.

The seedbed will be prepared in a fashion which would promote a stable, self-supporting prairie grassland. Rates for seed mixture will approximate:

<u>Species</u>	<u>Rate (lb/acre)</u>
Western Wheatgrass	6.0
Pubescent Wheatgrass	4.0
Smooth Brome	2.0

Seed implantation will be performed with a seed drill during the first favorable planting period; typically from April 15 through June 7, August 10 through September 15, or after October 20. A straw mulch or cover crop will be applied immediately after seeding to provide temporary erosion control. Reseeding or interseeding will be performed if grass fails to establish over

large areas. Bale dikes, excelsior mats, or other appropriate measures will be utilized for control of significant erosion features.

6.3.3 Post-Closure Surface Care

The Heskett Site will be incrementally reclaimed as individual disposal trenches are filled and closed. Post-closure surface care will continue until five years after final closure of the facility. Reclamation failures at the site would extend the surface care requirement period until such time as the deficiency is permanently corrected.

The post-closure maintenance will begin from the date of vegetation seeding. During the first year, each reclaimed area will be examined monthly and after storm events to:

1. Verify that final contours and drainages are maintained,
2. Ensure that healthy vegetative cover is established, and
3. Maintain proper erosion control measures which may be in-place at the site.

Post-closure inspections will be performed quarterly for the remaining four years of the surface care period. Inspection results and corrective actions will be logged. These records will be summarized into an annual facility status report and forwarded to the NDS DH.

The reclaimed area will resemble a gently sloping hill supporting a typical grassland prairie. The growth of woody species (whose root system might penetrate the underlying clay cap) will be suppressed through cutting or chemical treatment. Montana-Dakota may eventually sell hayland or pasture rights if the integrity and plant growth productivity of the site can be maintained with minimal care. No haying or grazing activities will be allowed

for at least three years following initial vegetation establishment of each reclaimed increment.

Montana-Dakota intends to continue ownership of the site for the foreseeable future. No plans to allow surface disturbance or agricultural utilization (except hayland or pasture usage) of the reclaimed area exist. The current industrial land use zoning classification will be retained.

EXHIBIT 6-A

EXISTING CONDITIONS AND AREA MAPS

EXHIBIT 6-B

PHASE I DEVELOPMENT

EXHIBIT 6-C

PHASE I CLOSURE - PHASE II DEVELOPMENT

EXHIBIT 6-D

FINAL CLOSURE

7.0 GROUNDWATER MONITORING

7.1 Operational Monitoring

Analysis of disposal site groundwater quality and potentiometric surfaces will focus upon the uppermost 15 feet of the Cannonball Formation saturated zone. Because facility expansion will eventually destroy most of the existing site instrumentation positioned for possible water quality monitoring purposes, a new series of monitoring wells will be installed prior to waste placement. Four new wells (3 downgradient, 1 upgradient) will be placed in the approximate areas described in Exhibit 6-B. These wells will be constructed similarly to existing site wells and fitted with a 20 foot screen, the lower 15 feet of which will be positioned below the existing water table. Each well will be lithologically logged during installation.

With the possible exception of infrequent potentiometric level determinations, all other wells existing at the site will not be relied upon for any monitoring functions. These deactivated wells will remain undisturbed until such time as their permanent closure is warranted by facility expansion.

Permanently closed wells will be sealed their entire length with grout or other appropriate material in order to assure that groundwater communication between subsurface strata does not occur along the well casing.

Wells which monitor facility operations will be sampled quarterly for the first year to establish background chemical data. The first quarterly sample will be acquired before waste is placed in the facility. The sampling frequency will thereafter be reduced to a semi-annual basis throughout the remaining operational life of the facility.

Water quality samples will be collected and analyzed by personnel experienced in groundwater characterization protocols. Static water table

elevation measurements will be made in advance of any well disturbances. Wells will be purged by pumping three to five well volumes (or until dry) immediately prior to well sampling. Delays in sampling greater than 24 hours will require re-purging.

All first-year background groundwater samples will be analyzed for water quality parameters specified in Table 7-1. This list of parameters will be reduced to a semi-annual groundwater quality characterization of Table 7-2 constituents subsequent to the completion of the first year collection of background data gathering.

7.2 Post-Closure Monitoring

Annual post-closure groundwater monitoring will continue for 30 years after final closure of the entire facility. Sampling for the first five years of the closure period will be performed on the same wells for the same chemical parameters as is in effect for operational monitoring program at the time of closure (i.e., Table 7-2 constituents).

If, after review of all accumulated operational and five years of post-closure data, no leachate contamination is statistically evident in the groundwater when compared to background levels, the suite of annually-monitored parameters will be reduced to:

pH	Static Water Level
Specific Conductance	Arsenic
Total Dissolved Solids	Boron
Carbonate	Selenium
Bicarbonate	Calcium
Sodium	Lead
Sulfate	Temperature

TABLE 7-1

Background Groundwater Quality Analysis Parameters

Alkalinity, total (as CaCO ₃)	Magnesium (Mg)
Arsenic (As)*	Manganese (Mn)*
Barium (Ba)*	Mercury (Hg)*
Bicarbonate (HCO ₃)	Molybdenum (Mo)*
Boron (B)*	Nitrate (NO ₃)
Cadmium (Cd)*	pH**
Calcium (Ca)	Potassium (K)*
Carbonate (CO ₃)	Selenium (Se)*
Chloride (Cl)	Silver (Ag)*
Chromium, total (Cr)*	Sodium (Na)
Fluorine (F)	Specific Conductance**
Hardness (as CaCO ₃)	Sulfate (SO ₄)
Iron (Fe)*	Temperature**
Lead (Pb)*	Total Dissolved Solids (TDS)

*Analyses only for dissolved metal concentration

**Field determinations

Static water levels will be measured from top-of-pipe.

TABLE 7-2

Operational Groundwater Quality Analysis Parameters

Alkalinity, total (as CaCO ₃)	Molybdenum (Mo)*
Arsenic (As)*	pH**
Bicarbonate (HCO ₃)	Potassium (K)*
Boron (B)*	Selenium (Se)*
Cadmium (Cd)*	Sodium (Na)
Calcium (Ca)	Specific Conductance**
Carbonate (CO ₃)	Sulfate (SO ₄)
Hardness (as CaCO ₃)	Temperature**
Lead (Pb)*	Total Dissolved Solids (TDS)
Magnesium (Mg)	

*Analyses only for dissolved metal concentration

**Field determinations

Static water levels will be measured from top-of-pipe.

Characterization of these groundwater quality indicator parameters will continue for the remaining 25 year post-closure groundwater monitoring period.

7.3 Quality Assurance and Data Management

Montana-Dakota currently relies upon experienced independent contractors to acquire analytical and potentiometric groundwater information. This practice is expected to continue for the foreseeable future. Minimum levels of performance for such contractors will include:

- Use of non-contaminating, non-aerating equipment for all monitoring activities. Equipment other than bailers or submersible diaphragm pumps for purging and sampling must be specifically approved by Montana-Dakota before use. Air-lift pumps may not be used in any circumstance.
- All samples must be conditioned, preserved, and analyzed according to methods and limitations prescribed in Methods for Chemical Analysis of Water and Wastes, EPA-600/4-79-020 (revised March 1983).
- Description of field sampling methods and analytical quality controls will be required of each contractor. Evidence of appropriate laboratory certification and participation in interlaboratory comparison will be requested. Brief resumes of involved personnel must also be provided.
- Cation/anion balances and replicate values for each set of data must be identified on the analysis report.

Montana-Dakota shall annually evaluate accumulated water table elevation and groundwater quality information gathered from site instrumentation by the contractor. Post-closure groundwater data obtained from wells surrounding

the adjacent Heskett ash waste pile (WS-series wells) will also be examined to determine their possible contribution to Heskett Site contamination monitoring. Data evaluation techniques will include chemical constituent comparisons between upgradient and downgradient wells at the same point in time and comparisons of individual wells to their historic background concentrations. A variety of statistical tools will be examined for application against the data base. Goodness-of-fit testing will confirm or deny the existence of normally distributed data. Specific test procedures might include hypothesis testing (t-test), parametric analysis of variance (ANOVA), ANOVA's based upon ranks, and perhaps tolerance intervals. Significance will be established at the 0.05 confidence level.

Operational groundwater monitoring will typically be performed in the second and fourth calendar quarters. Annual post-closure groundwater monitoring will be performed during the second or third quarter. All groundwater sample analysis results, water table surface elevations, and other associated information will be forwarded to the North Dakota State Department of Health within 30 days of its receipt from the independent groundwater sampling contractor. Cumulative statistical data summaries (including descriptions of the statistical methods employed) will be forwarded to the Department annually as they are completed.

8.0 PERMITTING

Upon approval by the North Dakota State Department of Health of the proposed solid waste disposal facility but before the onset of actual disposal activities, a notarized affidavit shall be recorded in the tract system of the Morton County Registrar of Deeds. This affidavit shall specify that the SW1/4 of Section 10, Range 81 West, Township 139 North, has been permitted to receive solid waste for disposal. Another affidavit shall be similarly filed upon final closure of the site which provides information concerning waste types, location, construction, and management. Copies of both instruments shall be forwarded to the North Dakota State Department of Health within 30 days of recording.

Other requirements, as specified by the North Dakota State Department of Health and other regulatory authorities, will be complied with as they become evident.

Upon the beginning of normal operations of the proposed disposal facility all waste placement at the current disposal facility (i.e. the Heskett Ash Pile) will cease. The ash pile will then be closed according to the specifications described in the relevant Special Use Disposal Site permit application (submitted to the North Dakota State Department of Health on March 10, 1986: Solid Waste Permit issuance still pending).



APPLICATION FOR PERMIT TO CONSTRUCT/OPERATE A
SPECIAL USE DISPOSAL SITE
NORTH DAKOTA STATE DEPARTMENT OF HEALTH
SFN 8376 (01/86)

NOTE: Please read the instructions for details on information and documents required to support your application.

PERSON TO BE RESPONSIBLE FOR OPERATION (APPLICANT) Station Manager, Heskett Station				APPLICATION DATE March 1, 1989
ADDRESS OF APPLICANT 400 North Fourth Street, Bismarck, ND 58501				TELEPHONE NUMBER (701) 222-7900
NAME OF SITE Heskett Ash Site	ADDRESS OF SITE Heskett Station, 2 Miles North of Mandan, ND			TELEPHONE NUMBER (701) 663-9576
PROPERTY OWNER Montana-Dakota Utilities	ADDRESS OF PROPERTY OWNER 400 North Fourth St., Bismarck, ND 58501			TELEPHONE NUMBER (701) 222-7900
LEGAL DESCRIPTION OF SITE A Portion of the SW $\frac{1}{4}$	SECTION 10	TOWNSHIP 139N	RANGE 81W	COUNTY Morton
PRESENT ZONING CLASSIFICATION OF SITE Industrial	DOES PRESENT ZONING ALLOW THIS PROPOSED USE? <input checked="" type="checkbox"/> YES <input type="checkbox"/> NO			EXPECTED LIFETIME OF SITE <u>28</u> YEARS

I hereby affirm all information in this application is true and accurate to the best of my knowledge and belief.

Bruce Finsdall

SIGNATURE OF APPLICANT

SEND COMPLETED APPLICATION TO:

NORTH DAKOTA STATE DEPARTMENT OF HEALTH
DIVISION OF HAZARDOUS WASTE MANAGEMENT AND SPECIAL STUDIES
1200 MISSOURI AVENUE, ROOM 302
BOX 5520
BISMARCK, ND 58502-5520

INSTRUCTIONS FOR COMPLETING AN APPLICATION FOR A
PERMIT TO CONSTRUCT AND/OR OPERATE A SPECIAL USE DISPOSAL SITE

**APPLICATION AND ALL ACCOMPANYING DOCUMENTS MUST
BE SUBMITTED IN QUADRUPPLICATE**

These instructions are considered to be general guidelines only. More or less data may be required by the Department depending on the waste and on conditions at the specific disposal sites. The information required for a specific site will be determined by a preliminary site evaluation by the Department. This may eliminate the expense of investigations at some sites which are obviously unacceptable. After the required site investigation has been completed by the applicant, further work may be required as deemed necessary by the results of the initial investigation.

Permit applications must be prepared and compiled as one cohesive document that logically presents all information necessary to review a permit. Any modifications or information submitted to the Department subsequent to the initial permit application should be in a format that can be physically incorporated into the formal permit application. The Department reserves the right to reject or return a permit application if it is not complete, or if the information is not presented in an orderly and logical format.

The instructions below address the following required information:

- I. Waste Information
 - II. Location Information
 - III. General Geographic Setting
 - IV. Site Specific Characteristics (Geology and Hydrology)
 - V. Construction Plans and Specifications
 - VI. Groundwater Monitoring
 - VII. Operation and Management Methods
 - VIII. Record Solid Waste Activity with County Registrar of Deeds
 - IX. Closure
-
- I. **WASTE INFORMATION:** For each type of solid waste to be managed, specify (a) amount in tons per day or cubic yards per day, or gallons per day; (b) physical description; and (c) qualitative and quantitative chemical analyses.
 - II. **LOCATION INFORMATION:** Show the facility location on a USGS 7 1/2 minute quadrangle map (scale not less than 1:24,000). Also include a current map or aerial photograph of the area showing existing land use. Aerial

photographs are often available from the Agricultural Stabilization and Conservation Service (ASCS). The map or aerial photograph shall be of sufficient scale to show those man-made and natural features of the area, such as water courses, flood plains, dry runs, wells, roads, and other appropriate details and the general topography of the area.

This section should also address the zoning within a quarter mile of the proposed location and any proposed changes in zoning required for waste disposal activities. The Department may request additional information from the applicant and/or the local zoning authorities regarding the zoning requirements for the site.

III. GENERAL GEOGRAPHIC SETTING: This narrative should be a general description of the site. It should include a general treatment of the geography, climate, soils, vegetation, geology, and groundwater to give an adequate background and foundation for effective presentation of the hydrogeology of the site and adjacent areas. The description should not be more elaborate than is necessary to accomplish this purpose.

IV. SITE SPECIFIC CHARACTERISTICS: (Geology and Hydrology) - This information shall be a detailed, integrated evaluation of the hydrogeologic conditions beneath and adjacent to the proposed site pertinent to the production and migration of refuse leachate, and to the capability for leachate containment and attenuation to acceptable quality before reaching a present or potential water source.

A qualitative and quantitative analysis of the effects of the emplacement of the refuse on the existing hydrologic regime must be addressed. Hydrogeologic data must be based on a systematic investigation utilizing data from borings, piezometers, water wells and other nearby water sources, the chemical characteristics of subsurface waters, and other available information.

After all pertinent information has been obtained, site investigation borings must be properly sealed or grouted in a manner that will prevent cross-contamination or interconnection of formations of strata.

A. TYPE AND EXTENT OF SUBSURFACE MATERIALS: A minimum of one boring is required for each ten (10) acres at the site. Regardless of minimum requirements, the degree of subsurface information obtained must be sufficiently comprehensive to allow the design hydrologist/geologist or engineer to make a detailed evaluation of the hydrologic and geologic properties of the subsurface materials, both at the site and laterally extrapolated, such that a reasonable estimate of the effects of these materials on the containment, migration, and attenuation of the leachate can be made. The site specific details must be incorporated into at least two or three cross-sections showing details on the site's geology, hydrology, and elevation. Any clay-rich soil to be used for compacted clay liners or cap must be accurately identified, located, and analyzed.

Borings used for the cross-sections must extend to a minimum depth of fifty (50) feet below the proposed elevation of the buried refuse, or if pertinent, a sufficient depth into bedrock to

determine its character and hydraulic characteristics. In-situ permeability tests may be necessary to determine the permeability of the formations surrounding and underlying the proposed facility. A lithologic and geophysical log may be required for each boring. The geophysical log may include a gamma-gamma and a gamma-density log.

The placement, construction and design of borings piezometer(s) and/or monitoring well(s) should be coordinated with an appropriate representative of the Department. The complete logs of each boring must be provided as well as the following information.

1. Date of boring
 2. Location of boring
 3. Method of drilling including the circulation technique (air, air-mist, water, mud)
 4. Method of sampling
 5. Diameter of borehole
 6. Elevation at surface of boring, referenced to mean sea level to the nearest 0.1 foot
 7. For monitoring wells, the elevations of the screened interval
 8. Depth and elevation of the water level in the borehole or piezometer
 9. Method of piezometer and/or monitor well completion or method used to seal and abandon borehole, whichever is applicable
- B. MATERIAL CLASSIFICATION AND ANALYSIS: Material samples should be taken by split spoon or shelly tube at depths in the boring operation where the type of material encountered differs from that immediately overlying, or in homogeneous materials, at regular intervals. These samples and any samples of clay-rich soil to be used for clay liners must be classified, tested, and analyzed in a materials testing laboratory and the following data reported:
1. Textural classification (USDA System or Unified System) plotted on the appropriate textural classification.
 2. Particle size distribution curves of representative samples.
 3. Coefficient of permeability - based on field (preferred) and/or laboratory tests.
 4. Ion-exchange capacity of samples and ability to adsorb and "fix" heavy metals. Results should be reported in millequivalents per 100 grams of sample. Most fine textured materials will favor ion-exchange because of their mineralogy,

low permeability and large surface area. Sands and gravels are less effective and hence will permit less attenuation of leachate per unit of flow path, and will allow more rapid rates of travel.

- C. **HYDROLOGY:** The hydrology of the site will dictate its ultimate suitability and the final design of the facility.

The design and operation, if soundly based on hydrogeologic principles, will incorporate one or more of the following: elevating the base of the disposal facility above any existing or potential zones of saturation; utilization of existing natural environment to contain and "treat" the leachate; modification of the natural environment to provide the desired hydrogeologic characteristics to either contain the leachate within the refuse, or to provide attenuation in the resulting hydrologic flow system and; isolate the refuse from the surrounding flow system by the use of a natural or artificially-installed liner, and thence collecting and treating the leachate by an engineered system.

Placement of refuse above the zone of saturation does not preclude all leachate production and resultant groundwater pollution, since precipitation during site operation as well as after site closure may generate leachate.

The hydrogeological factors which must be sufficiently considered include:

1. The permeability of the subsurface materials beneath and surrounding the area to be filled with waste;
2. The rate(s) and direction(s) of groundwater movement;
3. The spatial distribution of the potentiometric surface(s) at the time instrumentation is completed, as well as after the facility is constructed, including the water table and the potentiometric surfaces for aquifers in the vicinity of the site;
4. Any structural features which may affect the flow path for groundwater and/or leachate migration. Facilities proposed for areas underlain by significant lignite seams or for areas where lignite has been mined should include a structural contour map of the base of the lignite seam;
5. The effects of facility construction and the emplacement of the refuse on the existing hydrologic regimen, including consideration of flow-system changes as a result of site disruption, construction, or pumpage from present or potential water sources; and
6. The thickness, composition, and configuration of the final cover of the filled area, as well as the post-reclamation vegetation and its effect on surface water infiltration.

V. **CONSTRUCTION PLANS AND SPECIFICATIONS:** Submit a detailed narrative report with the following:

- A. A detailed topographic map of the existing site, (scale 1" = 200' or larger) using a contour interval of five (5) feet where the relief exceeds twenty (20) feet, and two (2) foot contour intervals where the relief is less than twenty (20) feet. The map should show all buildings, ponds, streams, ditches, utilities, roads, fences, location(s) of boreholes, and any other items of significance.
- B. A second topographic map, matched to the scale of the above map, prepared to completely describe the final construction of the proposed site. This should include the construction of disposal areas of trenches; the development of control features for surface water run-off, run-on, and drainage; any installation for the collection and treatment of leachate; access roads; buildings; utilities; fencing; monitoring wells; topsoil and subsoil stockpiles; cover material stockpiles; liner and clay cap material stockpiles; and all other features of the developed facility.
- C. A soil survey report with appropriate maps and a narrative. This section should describe the types of soils at the site and describe the thickness of the topsoil ("A" horizons) and the subsoil ("B" horizons). A description of how these horizons will be removed, handled, and stockpiled for later respreading during site reclamation must be included in detail. This stockpiled soil material (Suitable Plant Growth Material or SPGM) must be handled, stockpiled, and the piles revegetated in a manner that minimizes erosion and/or contamination of the material. The maps included in the construction plans should identify locations of SPGM stockpiles.
- D. Submit a series of cross-sections or profiles (scale 1" = 200' or larger) of the developed site. These sections should number no less than three (3), but in any case must be adequate to define the three dimensional distribution of materials to a depth of fifty (50) feet below the proposed elevation of refuse.

These profiles should clearly indicate the constructed pits, the geologic strata or lithology surrounding and underlying the disposal facility, the placement of any required side and/or bottom liners, the placement of any surface water sumps, the placement and screened interval of appropriate monitoring wells, the levels of the water table, groundwater flow directions, the proposed sequence of placement and total compacted thickness of each lift of waste, thickness of cover material for each lift, and the slope of the completed landfill with final cover in place. These cross-sections should be in a format that allows permit reviewers to obtain a quick and concise view of the proposed facility.

- E. The construction plans should address the Quality Control and Assurance Procedures to be used during site construction, liner

installation, groundwater monitoring, site operation, and site closure. The Department may require a routine report from the facility on the status of the operation and its construction (especially the liners) and its operation (especially surface water control and dust control). The description of the Quality Control Procedures for liner construction or any other appropriate construction (clay cap, etc.) should be signed by an independent registered engineer. A routine status report could be included with the quarterly groundwater monitoring report.

VI. GROUNDWATER MONITORING: The design of a groundwater monitoring system and the parameters for water analysis should be based on an assessment of the waste analysis, the site's geology and hydrology, the plans for construction, and the facility's method of operation. Items that should be discussed include:

- A. The water level in the boreholes immediately after boring completion and sufficient periodic measurements of the depth to water until stabilization has been attained.
- B. The vertical and horizontal components of the hydraulic gradients; a contour map for each potentiometric surface (data for which may be based on local domestic and industrial wells, and on-site piezometers and boreholes).
- C. The location of one or more up-gradient groundwater quality monitoring well nests and a minimum of two down-gradient groundwater quality monitoring piezometer nests to be located in the expected path(s) of the leachate migration. The location and construction of the piezometers should be in accordance with the hydrogeology of the site as determined by the exploratory program, subject to final approval by the Department.
- D. All monitoring wells must be cased and must be installed in compliance with Chapter 43-35 of the North Dakota Century Code and in compliance with Chapter 33-18-01 of the North Dakota Administrative Code governing water well construction. Monitoring wells must be completed in a manner that maintains the integrity of the borehole and precludes cross-contamination or interconnection of aquifers or geologic strata. The casing must be screened with an appropriately sized factory slotted pipe and packed with clean sand or gravel to allow collection of groundwater samples. The annular space between the well casing and borehole must be properly sealed to prevent contamination of samples and the groundwater.

At the surface, all wells must have a proper apron to prevent surface water infiltration and a protective outer casing to prevent physical damage to the well. The outer casing should include a cap and lock.

The monitoring piezometer should be constructed of non-metallic material, with a two (2) inch or greater inside diameter. Such piezometers will aid in evaluation of the effectiveness of the proposed facility design, and provide an early warning of design malfunction so that timely remedial measures can be initiated.

- E. Background analysis for the following chemical characteristics shall be mandatory for at least one groundwater sample taken from a piezometer installed in the expected flow path(s) of the leachate.

EPA standard procedure shall be used for obtaining, transporting, and analyzing samples. The results of the analysis shall be submitted to the Department before an operating permit can be issued.

CHEMICAL PARAMETERS FOR GROUNDWATER ANALYSIS

1. Total Alkalinity (CaCO_3)
2. Arsenic (AS*)
3. Bicarbonate (HCO_3)
4. Cadmium (Cd)*
5. Calcium (Ca)*
6. Carbonate (CO_3)
7. Chloride (Cl)
8. Total Chromium *
9. Fluoride (F-)
10. Hardness (as calcium carbonate)
11. Iron (Fe)*
12. Lead (pb)*
13. Magnesium (Mg)*
14. Manganese (Mn)*
15. Mercury (Hg)*
16. Nitrate (NO_3)
17. pH
18. Potassium (K)*
19. Sodium (Na)*
20. Specific Conductance**
21. Sulfate (SO_4)
22. Total Dissolved Solids
23. Selenium (Se)*
24. Barium (Ba)*
25. Silver (Ag)*
26. Molybdenum *

* Analyzed for "dissolved" metals. (i.e. samples filtered through an 0.45u membrane filter.

** Reported in micromhos at 25 degrees C.

Additional parameters may be assigned by the Department. These parameters will be determined by the detailed chemical analysis of the waste.

All constituents reported in milligrams per liter (mg/l).

Periodic groundwater samples shall be collected and analyzed by the applicant, or his designated representative, to monitor for alterations in groundwater quality. The frequency of samples and parameters required for analysis will be specified by the Department.

VII. OPERATION AND MANAGEMENT METHODS: The permit application must contain details on the facility's operation and maintenance. This should include in detail:

- A - Personnel
- B - Contingency and emergency plans
- C - Control of access to the site (fence, gates, signs, etc.)
- D - Roads (including maintenance)
- E - Confining disposal to as small an area as possible
- F - Dust control
- G - Spill prevention and cleanup
- H - Storage (if any)
- I - Source and thickness of cover
- J - Frequency of covering
- K - Methods of waste handling and haulage
- L - Leachate (including pit water) and surface water run-on/run-off control, handling, and disposal
- M - Recordkeeping
- N - Development Plans
- O - Quality Assurance and Quality Control

VIII. RECORD OF SOLID WASTE DISPOSAL ACTIVITY WITH THE COUNTY REGISTER OF DEEDS: Prior to onset of disposal activities, the permittee shall record a notarized affidavit with the County Register of Deeds to place a notation in the County's tract system specifying that this solid waste management site, as specified in the legal description, is permitted to accept solid wastes for disposal.

This affidavit shall specify that another affidavit must be recorded upon the facility's final closure.

Upon closure, an additional affidavit shall be recorded, as above, specifying any final details regarding the types of wastes disposed at the site, as well as any final details regarding the site's location, construction, management, etc.

The Department must be provided with a copy of both affidavits certified by the County Register of Deeds in the county in which the disposal site is located, within thirty (30) days of their recorded dates.

IX. CLOSURE: A closure plan must be included which describes in detail the procedures to be followed and the materials and manpower to be used in accomplishing final closure of the disposal facility. Generally, closed sites should have an adequate slope to promote surface water run-off without causing active erosion of the final cover.

The plan should include whatever maps, cross-sections, diagrams, and narrative is necessary to detail such things as:

- A. Schedule or timetable of closure.
- B. Final elevation of disposed wastes.

- C. Equipment necessary to accomplish closure.
- D. Type, volume, and source of cover material.
- E. Construction and placement of clay and/or synthetic cap and any drainage layers.
- F. Final grading/contouring of the facility.
- G. Topsoil replacement.
- H. Seed, fertilizer, and irrigation necessary to establish cover.
- I. Surface water run-off.
- J. Schedule for post-closure groundwater monitoring.
- K. Maintenance of leachate control or collection system.
- L. A short description of the utilization and maintenance of the disposal area after closure. The closed site should be managed in a careful manner that will prevent deterioration of the desired plant community and the low permeability final cover. The closure plan should provide for routine inspection and maintenance of the closed site, including the replanting of vegetation and the replacement of any eroded final cover.

9.0 SUMMARY

A permanent coal combustion ash disposal facility will be constructed north of Mandan, ND adjacent to the R. M. Heskett power station. The disposal site will be incrementally developed to minimize impact upon the landscape and reduce potential for fugitive dust emissions and waste leachate generation. Disposal trenches will be bi-annually constructed and equipped with an in situ clay liner sloping towards an in-pit leachate collection system. Collected leachate will be evaporatively treated in a clay-lined surface impoundment.

Earthen berms and tree plantings will provide visual and acoustical obstructions between facility operations and adjacent dwellings to the south. Additional landscaping may be performed as needed. Filled trenches will be covered with a compacted clay cap along with uncompacted overburden and plant growth materials to a total depth of eight feet. Reclamation will be performed with each disposal trench closure and produce a gently sloping grassland.

The groundwater immediately beneath the site is of poor quality and marginally useful as a domestic or agricultural resource. All waste will be emplaced above the historic water table. Facility operations should not effect local groundwater flow. A monitoring program will be established to characterize deviations in groundwater hydrology and chemistry. Contingencies have been identified in the event of site characterization errors, incompatible facility design, or operational difficulties as outlined in this permit application.

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SINGLE
FAMILY
RESIDENTIAL

SINGLE
FAMILY
RESIDENTIAL

INDUSTRIAL

PROPOSED

ASH

DISPOSAL

SITE

INDUSTRIAL

R.M. HESKETT STATION

AGRICULTURAL

MULTIPLE FAMILY RESIDENTIAL

INDUSTRIAL

EXHIBIT 3-C
HESKETT SITE
AERIAL PHOTO & ZONING

Scale: 1" = 200'
3-30-88

R. M. HESKETT STATION

SPECIAL USE DISPOSAL SITE

PERMIT APPLICATION

Montana-Dakota Utilities Co.
400 North 4th Street
Bismarck, ND 58501

March 1, 1989

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1.0 INTRODUCTION

This application describes hydrogeologic, constructional, and operational details relevant to the procurement of a Solid Waste Disposal Permit from the State of North Dakota. The characterization data and design specifications contained within this application are based upon results obtained from a 1986 investigation which focused upon selecting a waste disposal site that would be suitable for long-term disposal of coal combustion ash generated at the R.M. Heskett Station. The specific objective was to locate a site that would require minimal engineering design and allow the use of in-situ materials for leachate containment and chemical attenuation. Several localities were considered with one site being selected for a highly detailed geohydrologic evaluation. The proposed ash disposal site is located approximately one-quarter mile west of Heskett Station and 2 miles north of Mandan, ND.

A total of 27 monitoring wells were installed in and around the site. The monitoring of well water levels over a two year period has indicated the presence of a static water table (generally 30-40 feet below the ground surface) which flows in a north-northeasterly direction. Potentiometric levels indicated a substantial downward component of groundwater flow over the entire proposed disposal site.

During the operational phase of ash disposal primary objectives will include the minimization of fugitive dust production and preservation of the area landscape by continual reclamation of ash-filled "trenches". Frequent coverage of the trenches with low permeability earthen materials, in conjunction with in-pit water collection devices and an evaporative liquids treatment system, is expected to reduce highly mineralized leachate generation and its degradation potential to the poor-quality groundwater resource beneath

the facility. The suitability of the disposal setting is further assured by the placement of waste above the historic water table and the construction of a surface water drainage system adjacent to the site. Contingencies have also been identified which would hinder unanticipated increases in water table elevation.

2.0 WASTE INFORMATION

2.1 Sources of Waste

Montana-Dakota Utilities Co. currently operates two lignite-fired electrical generation units at its R. M. Heskett Station. Unit #1, operational since 1954, utilizes a spreader stoker-type steam generator in the production of up to 20,000 Kw/hr of electrical energy. Unit #2 became functional in 1963 with a boiler similar in design to Unit #1. In early 1987, Unit #2 was converted to an atmospheric fluidized bed combustor capable of supporting a turbine capacity of 73,000 Kw/hr. Units #1 and #2 have an anticipated remaining operational life of 20 years and 30 years, respectively. Both units produce fly ash and bottom ash as the mineral residue of lignite combustion.

2.2 Amounts of Waste Produced

Annual ash generation rates from Heskett Station are estimated in Table 2.1. The proposed disposal facility is designed to accommodate the combustion wastes that will be generated throughout the remaining operational life of Unit #1 (175,000 tons or 1.5×10^5 cy) and Unit #2 (1,569,000 tons or 1.4×10^6 cy).

TABLE 2-1

Annual Ash Generation from Units 1 and 2
at R. M. Heskett Station

	FLY ASH		BOTTOM ASH		SAND ¹	
	Tons	Cubic Yards	Tons	Cubic Yards	Tons	Cubic Yards
Unit 1	4035	4000	4737	3500	-----	-----
Unit 2	25877	25500	10569	7800	15854	11800
Total	29912	29500	15306	11300	15854	11800
Percent (by weight)	49	-----	25	-----	26	-----
Estimated total weight of ash (with sand) 61,070 tons						
Estimated total volume of ash (with sand) 52,600 cubic yards						

¹ Sand is only used within the fluidized bed of Unit #2.

2.3 Description of Waste

All lignite combustion waste produced at Heskett Station will be deposited within the disposal facility in a nonsegregated manner. The combined ash-types differ in color from a light brown to gray-black. Waste texture can vary from a fine, flour-like powder to a distinctly granular consistency. The fluidized bed combustor for Unit #2 utilizes significant amounts of inert sand as a bed matrix. During combustion this sand becomes coated and interspersed with bottom ash slag. Bed sand will be disposed of with the fly ash/bottom ash mixture. The fluidized bed material is visually obvious in the ash mixture due to its uniform granular appearance.

An analysis was performed on the leachate of representative samples of each type of ash waste intended for disposal at the proposed facility. Fly ash and bottom ash samples were collected from Unit #1 ash hoppers during normal operations. Unit #2 fly ash and bottom ash samples were obtained during a "test burn" of Beulah lignite in a scale model fluidized bed steam generation system.

Leachate was extracted from each ash sample using EPA Extraction Procedure Method 1310 (EP Toxicity Test) without pH adjustments (no acetic acid additions). Exhibit 2-A present results of the analytical analysis for both fly ash and bottom ash types. (Because Unit #2 fly ash and bottom ash were collected from a test burn, an EP Toxicity Test was later performed to characterize operational ash samples - these results also appear in Exhibit 2-A.)

The pH of all ash leachates appeared quite alkaline in nature. Fly ashes from Units #1 and #2 contained more alkali than their respective bottom

ashes. Leachate pH was considered an important factor in judging site suitability in that it controls the release of trace elements which are locked in the lattice structures of various mineral phases of lignite combustion residue (Groenewold et al., 1980). Sulfate and sodium concentrations were also higher in the fly ashes when compared to those of the bottom ashes.

Leachate from all ash samples, except Unit #1 bottom ash, contained detectable levels of arsenic, cadmium and lead. Selenium was detected only in the fly ash of both units. Fluoride, iron, magnesium, chloride and boron occurred in both the fly and bottom ash leachate at very low concentrations. Nitrates and other analyzed trace elements were near or below laboratory detection limits.

EXHIBIT 2-A

WASTE LEACHATE EXTRACTION ANALYSES



MINNESOTA VALLEY TESTING LABORATORIES, Inc.



PHONE (507) 354-8517

P.O. BOX 249, CENTER & GERMAN STREETS, NEW ULM, MINNESOTA 56073-0249

Report To: Montana Dakota Utilities
400 North 4th Street
Bismarck, ND 58501

Date: November 11, 1986

Work Order # CS-2251

Attn: John Verwey

Date Received: 9-25-86

Sample Identification: Coarse Ash Hopper, Precipitation Hopper Comp.

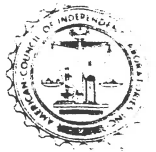
Analyses	Unit #1	
	Coarse Ash Hopper (Bottom Ash)	Precipitation Hopper Comp. (Fly Ash)
Total Alkalinity as CaCO ₃ ...mg/l..	414	1.472
Bicarbonate as CaCO ₃ ...mg/l.....	161	150
Calcium.....mg/l.....	77.5	95.0
Carbonate as CaCO ₃ ...mg/l.....	253	1,323
Chloride.....mg/l.....	19.0	23.0
Fluoride.....mg/l.....	0.11	0.22
Hardness as CaCO ₃ ...mg/l.....	194	238
Iron.....mg/l.....	0.2	0.2
Manganese.....mg/l.....	< 0.01	0.01
Magnesium.....mg/l.....	0.1	0.1
Nitrate.....mg/l.....	< 1.0	< 1.0
pH.....	11.5	12.6
Potassium.....mg/l.....	15.0	100
Sodium.....mg/l.....	380	2,200
Specific Conductance micromhos/cm	2,544	15,001
Sulfate.....mg/l.....	900	6,550
Total Dissolved Solids...mg/l....	1,357	10,389
Boron.....mg/l.....	0.91	1.18

EP Tox Extraction
no acid added.

BY Jerome Kolesky



MINNESOTA VALLEY TESTING LABORATORIES, Inc.



PHONE (507) 354-8517

P.O. BOX 249, CENTER & GERMAN STREETS, NEW ULM, MINNESOTA 56073-0249

Report To: Montana Dakota Utilities
400 North 4th Street
Bismarck, ND 58501

Attn: John Verwey

Date: November 11, 1986
Work Order # CS-2251
Date Received: 9-25-86

Sample Identification: Coarse Ash Hopper, Precipitation Hopper Comp.

Analyses	Unit #1 Coarse Ash Hopper	Unit #1 Precipitation Hopper Comp.
	Bottom Ash	Fly Ash
Arsenic.....mg/l.....	< 0.002	0.070
Barium.....mg/l.....	< 0.5	< 0.5
Cadmium.....mg/l.....	< 0.01	0.02
Chromium.....mg/l.....	< 0.05	< 0.05
Lead.....mg/l.....	< 0.10	0.40
Mercury.....mg/l.....	< 0.002	< 0.002
Selenium.....mg/l.....	< 0.003	0.003
Silver.....mg/l.....	< 0.05	< 0.05
Molybdenum....mg/l.....	< 0.50	< 0.50

EP-TOX Extraction
no acid added

BY Jerome Kotecky



MINNESOTA VALLEY TESTING LABORATORIES, Inc.



PHONE (507) 354-8517

P.O. BOX 249, CENTER & GERMAN STREETS, NEW ULM, MINNESOTA 56073-0249

Report To: Montana Dakota Utilities
400 North 4th Street
Bismarck, ND 58501

Date: November 11, 1986

Work Order # CS-2251

Attn: John Verwey

Date Received: 9-25-86

Sample Identification: Bed Ash, Bag House

*Unit #2
Bottom Ash*

*Unit #2
Fly Ash*

Analyses	Bed Ash	Bag House
Total Alkalinity as CaCO ₃ ...mg/l..	173	598
Bicarbonate as CaCO ₃ ...mg/l.....	69.0	80.5
Calcium.....mg/l.....	570	105
Carbonate as CaCO ₃ ...mg/l.....	103.5	517.5
Chloride.....mg/l.....	5.0	21.0
Fluoride.....mg/l.....	< 0.10	0.27
Hardness as CaCO ₃ ...mg/l.....	1,429	263
Iron.....mg/l.....	0.2	0.1
Manganese.....mg/l.....	< 0.01	< 0.01
Magnesium.....mg/l.....	1.4	0.1
Nitrate.....mg/l.....	< 1.0	< 1.0
pH.....	10.7	11.9
Potassium.....mg/l.....	40.0	100
Sodium.....mg/l.....	1,200	2,350
Specific Conductance micromhos/cm	7,066	10,870
Sulfate.....mg/l.....	4,300	6,160
Total Dissolved Solids...mg/l....	5,774	8,324
Boron.....mg/l.....	1.20	1.70

*EP TOX Extraction
no acid added*

BY *Jerome Kotecky*



MINNESOTA VALLEY TESTING LABORATORIES, Inc.



PHONE (507) 354-8517

P.O. BOX 249, CENTER & GERMAN STREETS, NEW ULM, MINNESOTA 56073-0249

Report To: Montana Dakota Utilities
400 North 4th Street
Bismarck, ND 58501

Attn: John Verwey

Date: November 11, 1986

Work Order # CS-2251

Date Received: 9-25-86

Sample Identification: Bed Ash, Bag House

*Unit #2
Bottom Ash*

*Unit #2
Fly Ash*

Analyses	Bed Ash	Bag House
Arsenic.....mg/l.....	0.155	0.045
Barium.....mg/l.....	< 0.5	< 0.5
Cadmium.....mg/l.....	0.02	0.03
Chromium.....mg/l.....	< 0.05	< 0.05
Lead.....mg/l.....	0.35	0.25
Mercury.....mg/l.....	< 0.002	< 0.002
Selenium.....mg/l.....	< 0.003	0.004
Silver.....mg/l.....	< 0.05	< 0.05
Molybdenum....mg/l.....	< 0.50	< 0.50

*EP TOX Extraction
no acid added.*

BY _____ *Jerome Kotecky*



*Sewer
ad - Utilization*

**MINNESOTA VALLEY
TESTING LABORATORIES, Inc.**



PHONE (507) 354-8517

P.O. BOX 249, CENTER & GERMAN STREETS, NEW ULM, MINNESOTA 56073-0249

*BIOB method
No X detection
1-20?*

**Report To: Montana Dakato Utilities Co.
Attn: Gene Brown
P.O. Box 40
Mandan, ND 58554**

Date: November 18, 1987

Work Order # 12-2237

Date Received: 9-29-87

Sample Identification: EPA Toxicity

Unit #2 bottom ad

<u>Analysis</u>	<u>4638</u>
Arsenic.....mg/L.....	0.004
Barium.....mg/L.....	< 0.1
Cadmium.....mg/L.....	< 0.05
Chromium.....mg/L.....	0.14
Lead.....mg/L.....	< 0.100
Mercury.....mg/L.....	0.0003
Selenium.....mg/L.....	< 0.003
Silver.....mg/L.....	0.04

A FULL SERVICE LABORATORY

BY David A. Diamond

MVTL guarantees the accuracy of the analysis done on the sample submitted for testing. It is not possible for MVTL to guarantee that a test result obtained on a particular sample will be the same on any other sample unless all conditions affecting the sample are the same, including sampling by MVTL. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

LABORATORY REPORT

To: Mineral Specialities (1)
Address: P.O. Box 1563
Billings, Montana 59103
ATTN: Jerry Vollmer

Lab No.: 87-7859
Date: 7/24/87 pjf

EP TOXICITY ANALYSIS - Fly Ash - Unit 2

Heskett Plant, North Dakota
Submitted 6/26/87

Extraction and analysis performed according to SW-846,
Test Methods for Evaluating Solid Waste.

<u>CONSTITUENT</u>	<u>mg/l in extract</u>
Arsenic	<0.5
Barium	<10
Cadmium	<0.1
Chromium	<0.5
Lead	<0.5
Mercury	<0.02
Selenium	0.2
Silver	<0.5

Post-it® Fax Note	7671	Date	4/3	# of pages	1
To	Alan Wette	From	Andrea		
Co./Dept.		Co.			
Phone #		Phone #			
Fax #		Fax #			

3.0 PROPOSED SPECIAL USE DISPOSAL SITE

3.1 Site Location

The R. M. Heskett Station is located in Morton County approximately two miles north of Mandan, ND. Disposal facility siting began by reviewing existing published geologic and hydrologic data to preliminarily identify potential sites within a 20 mile radius of Heskett Station. Five candidate sites were chosen and field evaluated. Two sites were determined as meriting further characterization and were comparatively examined in detail (Exhibit 3-A). Hydrologic, lithologic, aesthetic, economic, land use, and safety considerations indicated that the Heskett Site would prove best suited for the proposed disposal facility.

The Heskett Site is located east of Highway No. 1806 and approximately one-half mile west of Heskett Station. The site covers 47 acres of the SW1/4 of Section 10, Range 81 West, Township 139 North and is bound on the west and north by Rock Haven Creek, east by Heskett Station and the existing ash storage pile, and on the south by 43rd Street Northeast. Industrial property belonging to the Amoco Oil Refinery lies directly to the south of 43rd Street Northeast. Scattered residential housing lies adjacent to the north, west, and south of Heskett Site.

3.2 Land Use and Zoning

Heskett Site is currently owned by Montana-Dakota Utilities Co. and holds an industrial zoning designation. A plat of the site appears in Exhibit 3-B along with monitoring well location/elevation information. An examination

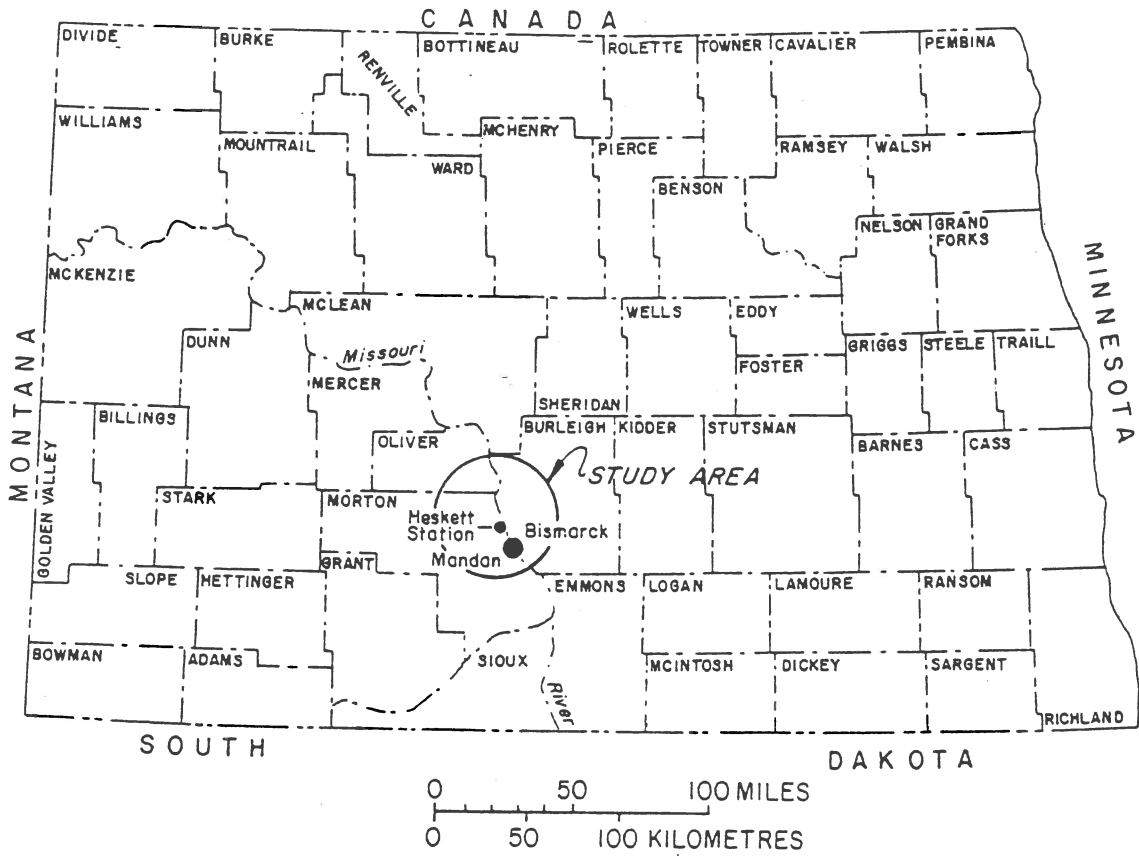
of Exhibits 3-B and 3-C indicates area land use to be primarily of an industrial and agricultural nature. The site itself is native grassland previously used for grazing livestock. Flat farmlands extend to the north while hilly pasture predominates to the west of Highway No. 1806. Level cropland and wildlife sanctuary exists on Amoco Refinery property south of 43rd Street Northeast.

Several family dwellings exist to the south and west of the Heskett Site. Other dwellings are scattered singly and in groups throughout the surrounding area. Because of the close proximity of some residences to the proposed facility, certain features will be incorporated into the design which will preserve the landscape by presenting line-of-site obstructions from the south and, if needed, west and north.

EXHIBIT 3-A

STUDY REVIEW AREA AND FINAL SITES

Study Review Area



Study Area - Final Sites

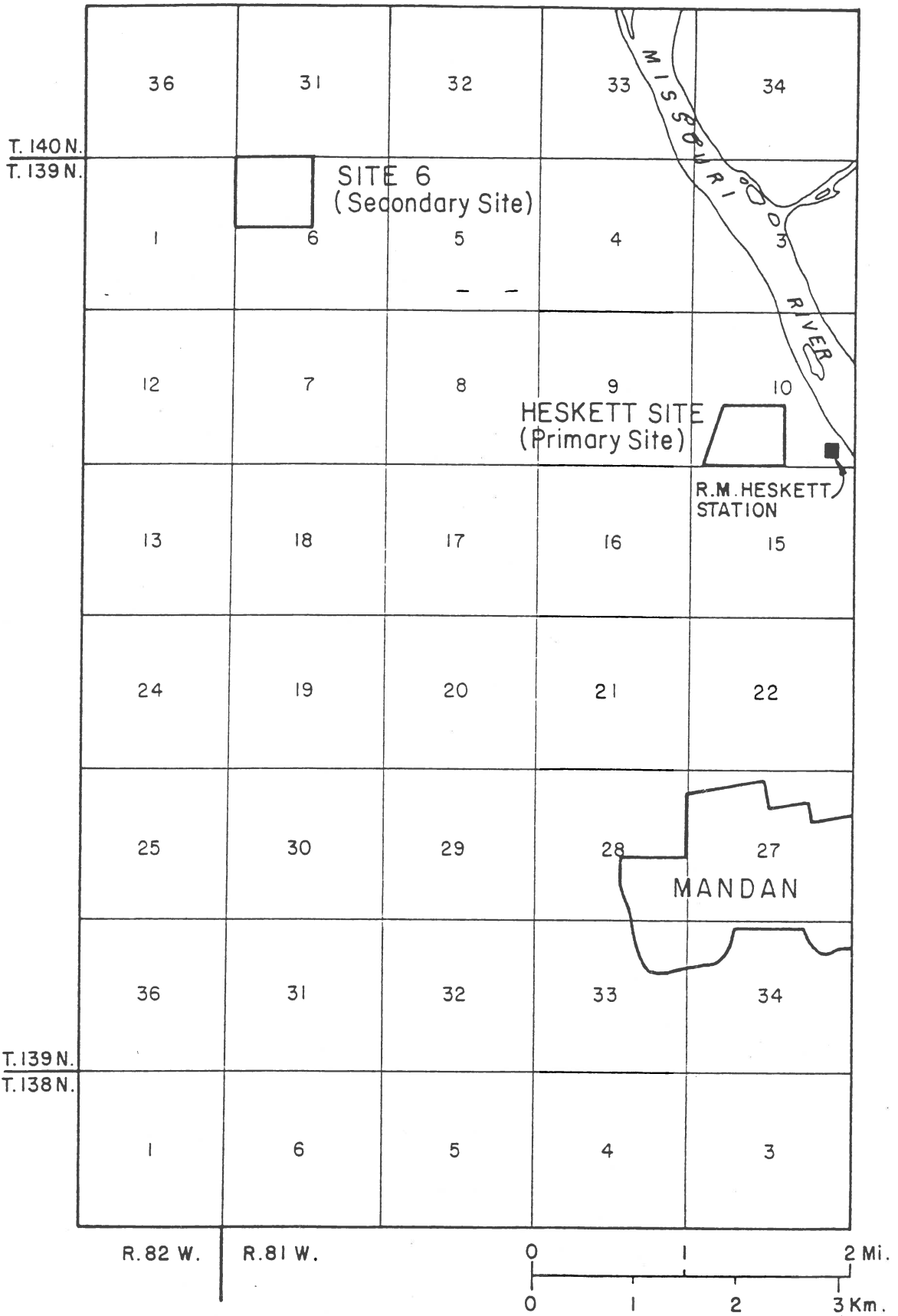


EXHIBIT 3-B

SITE PLAT/WELL SITINGS

EXHIBIT 3-C

AERIAL PHOTO AND ZONING

4.0 AREA DESCRIPTION

4.1 Geographical Setting

The disposal area is located entirely within the Missouri Plateau of the Great Plains Physiographic Province. Characterized by plains and gently sloping hills, the landscape is interrupted by isolated tablelands and river valleys entrenched 200 to 400 feet (Ackerman, 1980). Surface altitudes generally increase towards the west.

The Heskett site is a relatively flat area bounded on the west and north by an ephemeral stream (Rock Haven Creek) which supports a small shrub/woodlands community. Rock Haven Creek drains a small hilly area of approximately 2.4 square miles to the west of the site. Discharge is made directly into the Missouri River. No surface water flow gauging has ever been done at Rock Haven Creek. The North Dakota State Water Commission estimated annual flow of at least 50 acre-feet for every 80 years out of 100. One hundred acre feet of flow can be expected for 50 years out of 100.

4.2 Regional Geology

The Tertiary Cannonball Formation underlies the entire Heskett site and lies stratigraphically under several other regional formations (Exhibit 4-A). The Cannonball Formation crops out over a large portion of eastern Morton County. The bluffs along the Missouri River north of Mandan near Heskett Station are resultant from these outcrops.

The Cannonball Formation is characterized by deposits of sand, silt and clay. The beds within this formation are generally unconsolidated and tend to weather rapidly. Some of the sand units are partially cemented and are resistant to erosion. The resistant units often form benches along eroded

drainages (Carlson, 1983). Cvancara (1976) points out another characteristic of the Cannonball Formation; lack of persistent lithostratigraphic units or beds. The units are often truncated because most bedding within this formation is lenticular.

The Cretaceous and Tertiary rocks in this portion of North Dakota generally dip toward the center of the Williston Basin. Reported dips of the Cannonball Formation in the Bismarck-Mandan area are generally less than 1° and trend toward the northwest. Local irregularities in dip direction and magnitude are common in the Cannonball Formation. These minor variations are caused by small synclines and anticlines which are superimposed on the larger structure of the basin (Kume and Hansen, 1965). These small anomalies may often be responsible for local irregularities in groundwater flow direction and magnitude.

4.3 Regional Groundwater

The Cannonball Formation interfingers with its continental equivalent, the Ludlow Formation. The two formations are contemporary with deposition of the Cannonball occurring in a marine environment and deposition of the Ludlow occurring in a fresh water environment.

Aquifers within these formations are generally found in fine grained sandstones. Such units range from 5 to 129 feet thick and contain from 5 to 40 percent silt and clay. Lateral extensiveness is typically lacking. Core samples from these aquifers possess hydraulic conductivities ranging 2.9×10^{-3} cm sec⁻¹ to 1.5×10^{-5} cm sec⁻¹ (Ackerman, 1980). General groundwater movement is to the east or northeast with major discharge areas occurring in the valleys of the Missouri River, Heart River, and Big Muddy Creek.

Ackerman (1980) further states that the Cannonball and Ludlow Formation aquifers maybe in hydraulic connection with adjacent glacial drift aquifers. Area groundwater is generally of a sodium bicarbonate or sodium bicarbonate-sulfate type. Such waters are usually of poor quality for domestic usage because of high sulfate concentrations and excessive levels of total dissolved solids.

4.4 Climate

The climate of the Heskett site is semiarid with widely ranging seasonal temperatures. Summer temperatures may exceed 100°F (38°C) while winter temperatures may drop below -40°F (-40°C). The mean average annual temperature at Mandan, ND is 41.4°F (5.2°C) with average annual precipitation being 16.8 inches (42.6 cm). Approximately 60 percent of the annual precipitation (10 inches) occurs as rain during a four month period beginning in April and extending through July (U.S. Department of Commerce, 1973).

There are on the average about 125 frost-free days in this region of North Dakota. The mean depth of frost penetration is 4.5 feet (1.4 m). Extremely cold winters may occasionally allow frost to penetrate up to a depth of 7.0 feet (2.1 m) (Jensen, 1984).

The prevailing wind in the Bismarck-Mandan area is from the west-northwest with a mean velocity of 10 mph (16.1 km/hr). Winds are generally stronger in the spring and early summer as opposed to the fall and winter (Jensen, 1984).

4.5 Regional Soils

Regional near-surface materials are soils which have developed from climatic and biotic interactions with poorly consolidated sand, silt, and clay

of the Upper Cretaceous and Tertiary Formations. Glacial till appears preserved on some upland surfaces and lowland alluviums (Carlson, 1983).

Area hills have moderately steep slopes and typically have well entrenched dendritic drainageways. Patterson, et al. (1968) stated that the Bainville and Morton soil series dominate the smoothly rounded hills west of the proposed site. These soils appear on slopes of 2 to 30 percent and are well to excessively drained. Both soils, being derived from weathered medium-textured beds of the Tertiary period, tend to be loamy with high water holding capacities and somewhat limited permeabilities. Morton soils comprise 35 to 50 percent of the immediate area and are often used for cropland. Bainville soils cover 40 to 55 percent of area acreage and, being susceptible to water erosion hazards, are commonly used for pasturage.

Adjacent to the Heskett site lies the floodplain of the Missouri River. Alluvial Havre soils overlay medium-textured sediments and dominate 60 to 85 percent of the nearly level floodplain. Havre soils, with their moderate permeability and high water-holding capacities, are extensively utilized for croplands and pasturage. Well-drained Banks and Lohmiller soils each comprise 5 to 15 percent of the slightly elevated ridges and flats associated with the Missouri River floodplain (Patterson, et al., 1968).

4.6 Vegetation

The principle natural vegetative community in the study area is the mixed-grass prairie dominated by short grasses. Edwards and Ableiter (1936) stated that the smooth heavy soils of the uplands support substantial growths of western wheatgrass (Agropyron smithii) and needlegrass (Stipa comata). Little bluestem (Andropogon scoparius) commonly grows on exposed knobs and

steep slopes. Sedges, weeds, and cattails are typical of the poorly drained areas.

Natural forests are confined to bottomlands and along large streams and drainageways. Steep-sided gullies, especially those with northern exposures, contain ash (Fraxinus lanceolata), elm (Ulmus americana), aspen (Populus tremuloides), and oak (Quercus macrocarpa). The Missouri River floodplain contains significant natural stands of cottonwood trees (Populus deltoides). Also present are occasional occurrences of thicket-type woody vegetative communities dominated by buffaloberry (Shepherdia argentea). Such thickets are common in or near "woody draws" and bottomlands but seldom cover large surface expanses.

EXHIBIT 4-A

REGIONAL GEOLOGIC FORMATIONS

Regional Geologic Formations

ERA	SYSTEM	FORMATION OR GROUP	THICKNESS (FEET)	LITHOLOGY	
CENOZOIC	QUATERNARY	ALLUVIUM	0-30	SILT, SAND AND GRAVEL	
		COLEHARBOR	0-300	TILL, GRAVEL AND SAND	
	TERTIARY	FORT UNION GROUP	GOLDEN VALLEY	0-60	SILT, CLAY AND SANDSTONE
			SENTINEL BUTTE	0-700	SILT, CLAY, SAND AND LIGNITE
			BULLION CREEK	0-500	SILT, CLAY, SAND AND LIGNITE
			SLOPE	0-60	SILT, CLAY, SAND AND LIGNITE
			CANNONBALL	0-300	SILT, CLAY AND SAND
			LUDLOW	0-200	SILT, CLAY, SAND AND LIGNITE

5.0 SITE SPECIFIC CHARACTERISTICS

5.1 Site Investigation Methods

5.1.1 Site Selection Criteria

A primary concern involved the location and development of a site which would have near-surface (upper 30 feet) in-situ materials possessing characteristics similar to those of clay liner material. Relatively level near-surface sediments characterized by high clay and silt content were considered desirable. Because such materials typically transmit groundwater at slow rates, the migration of leachate into usable subsurface water supplies would be severely hindered. Another consideration was the chemical attenuation capabilities of the subsurface geologic materials. Clay and silt have been reported to generally have higher chemical attenuation capabilities than do other sediments, thereby making their presence desirable for many waste disposal settings. (Drever, 1982).

Selection of potential site areas larger than 1 square mile were based solely upon existing available data. A database was constructed which included published information from county geologic and groundwater investigative reports, soil survey reports, and water well drilling reports submitted to the North Dakota State Water Commission (NDSWC) by private contractors. Topographic maps and county zoning maps were also reviewed.

Five candidate sites were selected based upon geologic, geomorphic, and hydrologic data evaluations. Limited surficial investigations (including soil borings) were then conducted at each of the five sites. The position of the water table was very important in defining an acceptable site. Only those

sites with water tables more than 25 feet below a relatively level ground surface were considered.

Selection of two final sites were based on lithology, transport distance, road limitations, topography, and apparent depth to groundwater. Boreholes were drilled at each of the sites (maximum drilled depth was 120 feet) and lithologic/hydrologic/geophysical information recorded. Review of this information indicated that the final candidate sites had very similar geologic and hydrologic characteristics. Economics of site development, local zoning conditions, land use, transportation safety, facility access, and operational monitoring factors strongly suggested that the Heskett site was the most suitable disposal facility location.

5.1.2 Subsurface Borings

Boreholes were drilled by either a Portadrill 524 or a Denver-Gardner Heavy Duty 1000. All borings were air drilled (without the addition of drilling fluids) to reduce contaminations to groundwater. Drilling conditions for each bore hole are presented in Exhibit 5-C. Samples were collected at 5-foot intervals or at occurrences of lithologic change.

A total of 27 observation wells were installed at the Heskett site with twelve of the boreholes developed into water table monitoring wells and 15 developed as piezometers. The location of the various observation wells are shown in Exhibit 5-A. Additional information on area hydrogeochemistry was obtained from 9 wells (identified in this report as monitoring wells WS1, WS1A, WS1B, WS2, WS3, WS3A, WS4, WS4A, and WS4B) that were installed during a previous groundwater investigation which was conducted around the ash waste pile immediately east of the proposed facility (Armstrong and Schmid, 1986).

The observation wells were installed in nests of 2 to 4 single wells screened at differing elevations. Nine separate piezometer nests were installed over the Heskett study area. The deepest well in each nest was geophysically and lithologically logged (Exhibits 5-D and 5-E, respectively). A typical nest contained one water table monitoring well and two piezometers screened at different elevations.

5.1.3 Monitoring Well Construction

Monitoring wells were constructed of two-inch schedule 40 PVC pipe with screened lengths of either 4 or 20 feet. The 20-foot screened sections were installed to monitor the elevation of the water table and for water quality sampling. The 4-foot screened sections were primarily installed to monitor hydraulic head. A factory slotted size of 1 X .020 inches was used for all well screens.

A filter sand pack was placed around the screened portion of each well after the pipe was lowered into the bore hole. Washed quartz sand was packed with the use of packing poles to a height of two feet above the top of the screened interval. Before sampling was conducted each well was developed twice by backwash and mechanical surge methods.

After the sand pack was complete, sealing grout was slurried down the annulus between the bore hole and the PVC pipe. The grout seal was continued to the land surface where a two-foot diameter grout pad was constructed around each monitoring well. The monitoring wells were capped with threaded male PVC cap adapters and assigned unique well numbers.

The water level measuring reference point for the wells was the top of the PVC well pipe. Well locations and elevations can be seen on Exhibits 3-B and 5-A. Well construction data are presented in Exhibit 5-C.

5.1.4 Groundwater Monitoring

Water levels were monitored periodically during and after the course of the formal characterization study. Water level information, as determined with an electric-contact gauge tape, appears in Exhibit 5-G.

Each well was purged prior to sampling by removing at least 3 well volumes of standing water or until dry, whichever occurred first. The wells were purged with either a stainless steel and teflon mechanical two-inch submersible pump or a 1.25 inch hand bailer. All well groundwater samples were collected with a hand bailer in accordance with the Environmental Protection Agency's publication 600/4-82-029, "Handbook for Sampling and Sample Preservation of Water and Waste Water" (US EPA, 1982). Immediately after the samples were collected field pH, specific conductance and temperature were measured and recorded.

Samples were collected and preserved for major ion analysis and for trace element determinations. Other samples were collected from select wells for oil, grease, and phenol analyses. Site characterization study samples (collected in 1986) were transported to the University of North Dakota's Mining and Mineral Resources Research Institute's Fuels Analysis Laboratory for chemical analysis. Additional follow-up sampling and chemical analysis was performed in 1988 by Minnesota Valley Testing Labs of Bismarck, ND.

5.2 Site Investigation Results

5.2.1 Geology

Lithologic and geophysical logs of the wells drilled at this site indicated that at least the upper most 100 feet of subsurface material lies

within the Cannonball Formation. Consequently, the proposed Heskett waste disposal facility would be constructed completely within the Cannonball Formation. The Ludlow Formation may appear subsurface of the Heskett site study area below an elevation of 1605 feet above mean sea level (MSL). However, only the deepest bore holes penetrated to this elevation and geophysical logs from these wells do not provide any indication of contact between the two formations.

An existing topographic reference map (with well locations and cross-section locations) is provided in Exhibit 5-A. A series of eight geohydrologic cross-sections of the proposed Heskett disposal site are provided in Exhibit 5-B. Each cross-section includes topography (exaggerated 10 times), dominant lithologies, observation well locations, potentiometric levels and water table position as of October, 1986.

The Heskett Site consists of unconsolidated silt and clay with lesser amounts of very fine to medium-grained sand (lithologic log, Exhibit 5-E). The sand is generally found interspersed in a matrix of silt and clay; however, it sometimes occurs as distinct lenses which range in depth from 0.5 inches to 1 foot. The thin sand lenses are not horizontally persistent. Small gypsum crystals occur throughout the upper 30 feet of the site. These gypsum crystals are presumed to be the result of diagenetic processes which occur above the water table during alternate wetting and drying cycles (Groenewold et al., 1983).

The dominant lithology of the site is silt which commonly occurs in a clay-rich matrix. Above an elevation of 1695 feet MSL the clayey-silt is generally brownish-tan in color with grain coatings and mottling of iron-oxides. Below this elevation the color changes to steel-gray with the iron

compounds existing in the reduced state. The reduced/oxidized boundary is well defined over the site by the color change described above and corresponds with the elevation of the water table.

The uppermost indurated unit encountered beneath the proposed disposal area is a siltstone bed occurring between the elevations of 1625 feet and 1635 feet MSL. This is the most laterally continuous and persistent unit found at the Heskett site.

A thin veneer of till is present in small patches throughout the Heskett study area. This till, along with all glacial material in North Dakota, has been grouped within the Coleharbor Formation (Bluemle, 1971). The till of the Heskett study area is less than 2 feet thick and is of a pebble-loam nature. Other evidence of glaciation includes the presence of several large boulders, less than 3 feet in diameter, which were derived from the Canadian Shield.

The glacial sediments indicate that glacial ice covered the study area during the Pleistocene Epoch. Horizontal sheet fracturing may have developed within the surficial bedrock formations, including the Cannonball Formation, as this glacial ice ablated. The fracturing of these sediments might promote secondary porosity and be responsible for the relatively large groundwater flow volumes encountered within the silts and clays beneath the Heskett site study area.

The soils across the proposed Heskett ash disposal area (Exhibit 5-F) are generally well developed. Edwards and Ableiter (1936) classified upland soils of the site as Hall series silt-loam. The soil is very silty with abundant clay and minor amounts of fine-grained sand. Internal drainage is generally good and surface drainage is sufficient. Most site soils are

approximately 1 foot thick with the upper 6 to 8 inches appearing very dark due to abundant organic matter. The soil becomes lighter in color 8 inches below the soil surface. All soils at the Heskett site are calcareous and freely effervesces with dilute hydrochloric acid.

5.2.2 Geohydrology

Exhibit 5-H illustrates the water table elevation contour of the Heskett site as of October 16, 1986. Because periodic well measurements over two years indicated relatively static potentiometric levels, the described elevation of the water table is considered representative. Water levels of all of the Heskett Site wells are given in Exhibit 5-G. Hydrographs of select piezometer nests appear in Exhibit 5-I.

The shallow groundwater beneath the proposed facility is flowing generally towards the northeast. Local variations do exist and can be attributed to the heterogeneous nature of the lithologies of the Cannonball Formation along with the undulating surface topography of the site. Surface topography appears to exert the most profound effect on groundwater flow with water table elevation mimicking the surface topography. As the groundwater approaches Rock Haven Creek it begins to take a more easterly path following the down-cut gradient of this creek into the Missouri River.

The groundwater flow beneath the base of a small draw, which extends to the north and slightly west from the south-central border of Section 10 to its intersection with the Rock Haven Creek, is nearly directly north. This groundwater flow is strongly influenced by the surficial topography which also dips toward the north. Industrial surface water holding ponds located on Amoco

refinery property south of the proposed site occasionally provides surface discharge into this draw. Running and ponded water resultant from these discharges as well as area ground surface runoff are frequently evident on MDU property just north of 43rd Street Northeast.

Morton County often experiences a drop in the elevation of the water table during the winter months due to a lack of recharge (Groenewold, et al., 1979 and 1983). Hydrographs (Exhibit 5-I) developed from two years of accumulated site potentiometric data indicate little apparent seasonal effect. An overall potentiometric level drop can be noted during the drought year of 1988. The data also indicated that the groundwater is flowing strongly downward. Thus, it can be expected that water will not be entering the proposed disposal pit from beneath the site.

Six subsurface lithologic intervals were sampled from in and near the proposed ash disposal site and laboratory tested to determine certain physical/chemical properties. Table 5-1 summarizes the results of cation exchange capacity and hydraulic conductivity testing for these samples (See Exhibit 5-K for greater detail). Data obtained from such lab permeability testing should be considered representative only of the point of sampling. Samples are often modified, in terms of hydraulic conductivity, during well drilling and sample collection. Minor subsurface fracturing might not be preserved in the laboratory. However, these data are useful in estimating flow rates through interstices in the subsurface geologic media and in situations where in-situ sediments will be modified by compaction to reduce secondary permeability.

Single-well response tests performed on select Heskett site wells (wells 11, 20, 31, 41 and 43) show greater in-situ permeabilities than the falling-head lab permeabilities of wells screened in the same sediments.

TABLE 5-1

Hydraulic Conductivities and Cation Exchange Capacities

Well Number	60	WS2	WS2
Sample Depth (ft)	20-40	29-30	61-62
Type of Sample	Bag	Core	Core
Permeability			
K @ 20°C (cm/sec)	2.0×10^{-7}	2.7×10^{-9}	3.6×10^{-8}
K @ 20°C (ft/min)	4.0×10^{-7}	5.4×10^{-9}	7.1×10^{-8}
Cation Exchange Cap. (meq/100 grams)	-----	92.2	12.0
Well Number	WS1	WS1	WS1
Sample Depth (ft)	20-21	25-26	30-31
Type of Sample	Core	Core	Core
Permeability			
K @ 20°C (cm/sec)	2.6×10^{-8}	1.5×10^{-8}	1.7×10^{-8}
K @ 20°C (ft/min)	5.2×10^{-8}	2.9×10^{-8}	3.4×10^{-8}
Cation Exchange Cap. (meq/100 grams)	71.8	12.3	74.2

WS - Refers to wells installed and sampled during a previous groundwater investigation around the coal ash waste pile at Heskett Station. This study was conducted by Water Supply, Incorporated.

These slug tests provide estimates of permeability over the screened 4-foot interval. Results, which appear in Table 5-2, show that wells 11 and 31 have the lowest permeabilities of the wells tested with values on the order of $K = 10^{-5}$ cm sec⁻¹. Higher conductivities were encountered in wells 20, 41 and 43 with values approximating $K = 10^{-4}$ cm sec⁻¹.

TABLE 5-2

Single Well Response Tests

<u>Well</u>	<u>Permeability</u>	<u>Screen Depth (MSL)</u>
11	3.78×10^{-5} cm sec ⁻¹	1642.81 - 1646.81
20	6.57×10^{-4} cm sec ⁻¹	1627.48 - 1631.48
31	2.84×10^{-5} cm sec ⁻¹	1635.58 - 1639.58
41	4.12×10^{-4} cm sec ⁻¹	1626.77 - 1630.77
43	5.07×10^{-4} cm sec ⁻¹	1650.14 - 1654.14

Reference: Freeze, R. A., and Cherry, J. A., 1979., Groundwater: Chapter 8.5, pgs. 339-342, Prentice-Hall Inc., Englewood Cliffs, NJ.

5.2.3 Hydrogeochemistry

Results of the site groundwater characterizations are shown in Exhibit 5-J. Analysis of samples collected in 1986 from wells 10-70 were conducted by the Mining and Mineral Resources Research Institute's Fuels Analysis Laboratory at the University of North Dakota. Supplemental sampling was conducted in 1988 by Minnesota Valley Testing Labs of Bismarck, ND. All samples were analyzed in accordance with EPA publication 600/4-79-020, "Methods for Chemical Analysis of Water and Wastes" (U.S. EPA, 1979).

The quality of the shallow (less than 120 feet below the land surface) groundwater at the proposed Heskett disposal site was found to be quite poor. Similar groundwater quality has been reported in other shallow wells within the Cannonball Formation (Ackerman, 1977 and 1980). Large quantities of salts and soluble mineral phases were deposited along with the sediments of the Cannonball. These materials dissociate as undersaturated interstitial groundwater flows through the formation. The ultimate quality of the water depends on the solubility of the geologic media and saturation condition of the groundwater which flows through it. Soluble constituents of the shallow groundwater at the Heskett site, as is characteristic of other Cannonball Formation wells, are high or very high relative to water in other aquifers in the area. Without pretreatment such groundwater is generally considered to be unfit for consumption by humans and livestock. Most of the local domestic wells tap either the underlying Hell Creek or the Fox Hills aquifers which possess waters with qualities far superior to that of the Cannonball.

An examination of the 1986 data appearing in Exhibit 5-J shows that the specific conductance and pH of wells sampled at the Heskett site are within the range of what has been reported as characteristic of the Cannonball Formation. Well 70 is located upgradient from known industrial influences and

can be considered representative of background groundwater quality at the site. Chemical analyses indicate that water within wells 60 and 70 have the highest specific conductance of all monitored wells.

Total dissolved solids (TDS) concentrations show the shallow groundwater at the Heskett site to be highly mineralized, ranging from 1,286 mg/L in well 30 to 14,917 mg/L in well 60. Wells screened within the Cannonball Formation commonly have TDS concentrations ranging from 1,000 to 3,000 mg/L (Ackerman, 1980).

Wells finished within the Cannonball Formation typically have sodium concentrations ranging from 500 mg/L to 1000 mg/L (Ackerman, 1977 and 1980). Sodium levels of wells 10, 12, 55 and 70 were well above these levels. Sulfate concentrations were highest in wells 44, 55, 60 and 70 with observed maximum occurring in well 60 (11,632 mg/L). Sodium, TDS and sulfate concentrations indicated that extremely saline pockets of groundwater exist at the southwestern (near wells 70, 10-13, and 60-62) and east-central (near wells 55 and 56) borders of the Heskett study area.

Both magnesium and calcium concentrations were relatively high and variable over the Heskett site study area. Well 44 contained the highest levels of these two constituents with 648 mg/L of calcium and 1,322 mg/L of magnesium. Heskett site water would be considered quite hard with actual values (expressed as CaCO_3) ranging from 222 mg/L in well 30 to 7,040 mg/L in well 60.

Chloride, potassium, iron, and fluoride concentrations were generally within the expected range of concentrations for wells finished within the Cannonball Formation. However, potassium was slightly elevated in wells 44 and 60 where it reached concentrations of 51 mg/L and 41 mg/L, respectively.

Nitrate concentrations were found to be erratic over the Heskett site. Wells 55 and 60 contain the highest nitrate levels with 154 mg/L and 170 mg/L, respectively. The drinking water standard (provided in Exhibit 5-J for reference purposes) for nitrate (NO_3^-) is currently set at 45 mg/L. The elevated nitrate concentrations in wells 50, 52, 55 and 60 would tend to indicate contamination from biological sources. Domestic sewage drainfields are known to exist near the center of the south border of the proposed disposal site in the vicinity of wells 43 and 44. It is believed that these sources contribute at least a portion of the observed elevated nitrate concentrations.

Selenium is a common naturally-occurring element in sediments, especially in shale and clay (Freeze and Cherry, 1979). Wells 55 and 60 had the highest concentrations with 0.368 mg/L and 0.195 mg/L, respectively. The levels observed in these two wells are above levels common to groundwater systems which contain shale and dissolved selenium. Indeed, these levels approach 100 times the concentration observed in groundwater taken elsewhere from the Cannonball Formation (Ackerman, 1977).

Molybdenum was detected at reduced concentrations in wells 10, 32, 54 and 70. Water Supply Incorporated (WS), in their previous groundwater investigation concerning the currently operational Heskett ash pile, noted concentrations of molybdenum in well WS4 similar to those observed in this study in wells 10, 54 and 70. Well WS4 was at the time noted for increasing molybdenum levels with the greatest concentration reaching 0.11 mg/L on September 11, 1985 (Armstrong and Schmid, 1986). Further groundwater monitoring has shown that after this finding molybdenum levels then dropped below analytical detection limits. Minimum detection levels have only occasionally been exceeded in the ensuing years. With this study's addition

of background monitoring wells upgradient from the current ash pile it can be determined that concentrations of molybdenum in well WS4 were within the background range of groundwater at the Heskett site. The elevated molybdenum concentrations as noted by W.S. are therefore not believed caused by the migration of leachate from the existing ash pile.

The 1988 groundwater data characterized only the uppermost zone of saturation near the proposed site. Its review indicated that the same general relationship between water quality and heavy metal parameters still exists after two years. A general diminishing of nitrate concentrations can be noted. Boron, an untested analyte in 1986, appeared in concentrations ranging from 1.0 ppm to 2.8 ppm (wells 45 and 70, respectively). Molybdenum was not detected. Wells 60 and 70 continued to exhibit extremely poor overall quality.

5.2.4 Chemical Attenuation of Leachate in Soil

A major concern in developing a waste disposal landfill is the potential generation and migration of toxic leachate. If highly mineralized subsurface leachate moves beyond the disposal site degradation of valuable groundwater supplies might occur. The leachate from the fly ash and bottom ash samples were generally comparable, in terms of overall quality, to the chemical composition of naturally-occurring groundwater at the Heskett site. An examination of Exhibits 2-A and 5-J shows that several of the major ions actually occurred at lower concentrations in the leachate than in the groundwater. Unit 1 bottom ash leachate appeared to be of much better quality than any groundwater sampled. Fly ash samples produced more highly mineralized (higher TDS) leachate than did bottom ash samples.

The overall quality of the existing groundwater at the proposed Heskett ash disposal site is brackish to saline with an average TDS concentration of 8,000 mg/L. The ash leachate produced using the modified EP toxicity test had an average TDS concentration of 6,500 mg/L. Consequently it may be expected that Heskett ash leachate will not significantly affect the TDS content of contaminated underlying groundwater even if soil buffer and attenuation mechanisms would be discounted.

The heavy metal analytes of primary concern in the leachate appear to be arsenic, cadmium, and lead. Sorptive, precipitation and co-precipitation processes are the major attenuation mechanisms that effect the concentration of these dissolved elements. Hassett and Groenewold (1986) studied trace element attenuation capabilities of coal-bearing Tertiary overburden deposits of central and western North Dakota. They found that the pH of a given leachate and the alkaline buffering capacity of the geologic media were the most critical variables in trace element attenuation. Western fly ash leachates are typically very alkaline with pH values approaching 13. In order to buffer such a solution either protons (H^+) must be added or hydroxyls (OH^-) must be removed. Oxides tend to ~~lose~~ lose protons in strongly alkaline solutions. This H^+ source, along with other acid producing reactions such as pyrite oxidation and organic decomposition, are the main alkaline buffering reactions. The protons that are liberated during these reactions will tend to neutralize the hydroxyl ions, thereby lowering the pH of the solution. The pH of the leachate will be buffered until it reaches equilibrium with the groundwater. In central and western North Dakota this equilibrium is generally attained at a pH value of between 7 and 9 (Groenewold et al., 1983; Koob and Groenewold, 1984).

Direct precipitation of cadmium and lead occur at pH values above 6.5. The solubility product of lead carbonate ($PbCO_3$) at $18^\circ C$ is 3.3×10^{-14} . In groundwater systems which contain abundant carbonate lead will be precipitated as lead carbonate, thereby maintaining dissolved lead at low concentrations (Beaver, 1986 and 1987). The same type of reaction maintains cadmium at very low concentrations. Hassett and Groenewold (1986) found that cadmium was removed in excess of 99 percent during laboratory experiments with reduced and oxidized silts. Beaver (1986) confirmed the attenuation capabilities of similar geologic media during a coal ash field monitoring program near Center, North Dakota. He noted that several ions, including arsenic, cadmium and lead, were highly mobile under alkaline conditions within the ash itself. However, the alkaline leachate was buffered as soon as it came into contact with the surrounding clay and silt deposits. As the pH became lower the concentrations of cadmium and lead were greatly reduced (Beaver, 1986).

Arsenic attenuation is also controlled by solution pH. Laboratory experiments performed by Hassett and Groenewold (1986) have shown that arsenic, as As^{5+} , is significantly attenuated by the Tertiary sediments of western North Dakota. Arsenic appears to be most strongly attenuated in the pH range of 7-9. The mobility of selenium is similar to that of arsenic and the same attenuation processes control its concentration in groundwater systems. Sorptive processes appear responsible for arsenic attenuation in geologic media but the mechanisms of attenuation have not yet been well defined (Hassett and Groenewold, 1986). It does appear that cation and anion adsorption on clay particles and hydroxide coatings are important mechanisms in attenuating arsenic and other trace elements.

Hassett and Groenewold (1986) have shown that the clay, silt and sand sediments of central and western North Dakota have a strong capacity to buffer

highly alkaline leachates and attenuate trace elements such as arsenic and selenium. The ash pile at Heskett station has been subjected to continuous leaching for the past 30 years. When the quality of the shallow groundwater in the vicinity of the ash pile (data currently on file with the Health Department) was compared to the proposed disposal site it was apparent that upgradient groundwater quality was similar to or of poorer quality than the water near the ash pile. Consequently, groundwater sampling data around the existing ash pile may support the Hasset and Groenewold conclusions if buffered and attenuated leachate from the ash pile is infiltrating underlying groundwater.

EXHIBIT 5-A

TOPOGRAPHY AND BOREHOLE/CROSS-SECTION LOCATIONS

EXHIBIT 5-B

GEOHYDROLOGIC CROSS-SECTIONS

(PLATES A THROUGH H)

EXHIBIT 5-C

WELL COMPLETION REPORTS

Well Number: 10

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CCD

Elevation: Ground; 1722.06 ft. Casing top; 1725.01 ft.
Well Bottom; 1604.01 ft.

Completion: Date drilled; 8-12-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 120 ft.
Encountered water (below surface); 65 ft.
Geophysical log recorded

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.90-115.30 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 115.30-119.30 ft.
Elevation of interval; 1604.01-1608.01 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 114-120 ft.

Grout Seal: Depths (from ground); 0-114 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 51.97 ft. below top of casing
Elevation; 1673.04 ft.

Chemistry: Date; 8-21-86
pH; 7.75 Sp. cond; 11050 micromhos/cm
Temp; 8.9 oC

Well Number: 11

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CCD

Elevation: Ground; 1722.10 ft. Casing top; 1725.01 ft.
Well Bottom; 1642.81 ft.

Completion: Date drilled; 8-12-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 80 ft.
Encountered water (below surface); 65 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.90-78.20 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 78.20-82.20 ft.
Elevation of interval; 1642.81-1646.81 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 77-79 ft.

Grout Seal: Depths (from ground); 0-77 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 43.83 ft. below top of casing
Elevation; 1681.18 ft.

Chemistry: Date; 8-21-86
pH; 7.75 Sp. cond; 9840 micromhos/cm
Temp; 8.6 oC

Well Number: 12

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CCD

Elevation: Ground; 1721.88 ft. Casing top; 1724.90 ft.
Well Bottom; 1643.51 ft.

Completion: Date drilled; 8-12-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 80 ft.
Encountered water (below surface); 65 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +3.02-58.37 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 58.37-78.37 ft.
Elevation of interval; 1643.51-1663.51 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 57-79 ft.

Grout Seal: Depths (from ground); 0-57 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 43.60 ft. below top of casing
Elevation; 1681.30 ft.

Chemistry: Date; 8-21-86
pH; 7.60 Sp. cond; 11440 micromhos/cm
Temp; 8.5 oC

Well Number: 13

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CCD

Elevation: Ground; 1721.88 ft. Casing top; 1724.90 ft.
Well Bottom; 1681.88 ft.

Completion: Date drilled; 11-13-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry

Boring: Diameter; 5 5/8 in. Depth drilled; 40 ft.
Encountered water (below surface); ? ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +3.02-20.37 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC Depths (from
ground); 20.37-40.37 ft.
Elevation of interval; 1681.51-1701.51 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 19-41 ft.

Grout Seal: Depths (from ground); 0-19 ft.
Date sealed; 1-27-87

Additional Data:

Static Water Level: Date; 12-15-86
Depth; 30.09 ft. below top of casing
Elevation; 1694.81 ft.

Chemistry: Date; NA
pH; NA Sp. cond; NA
Temp; NA

Well Number: 20

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CAC

Elevation: Ground; 1707.04 ft. Casing top; 1709.48 ft.
Well Bottom; 1627.48 ft.

Completion: Date drilled; 8-12-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry

Boring: Diameter; 5 5/8 in. Depth drilled; 80 ft.
Encountered water (below surface); 45 ft.
Geophysical log recorded

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.44-75.56 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 75.56-79.56 ft.
Elevation of interval; 1627.48-1631.48 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 74-80 ft.

Grout Seal: Depths (from ground); 0-74 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 37.96 ft. below top of casing
Elevation; 1671.52 ft.

Chemistry: Date; 8-21-86
pH; 7.98 Sp. cond; 4970 micromhos/cm
Temp; 8.7 oC

Well Number: 21

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CAC

Elevation: Ground; 1707.22 ft. Casing top; 1709.40 ft.
Well Bottom; 1661.90 ft.

Completion: Date drilled; 8-12-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;

Boring: Diameter; 5 5/8 in. Depth drilled; 50 ft.
Encountered water (below surface); 45 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.66-21.32 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 21.32-45.32 ft.
Elevation of interval; 1661.90-1685.90 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 20-46 ft.

Grout Seal: Depths (from ground); 0-20 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 29.33 ft. below top of casing
Elevation; 1680.07 ft.

Chemistry: Date; 8-21-86
pH; 6.95 Sp. cond; 13920 micromhos/cm
Temp; 8.5 oC

Well Number: 30

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CBA

Elevation: Ground; 1715.55 ft. Casing top; 1717.64 ft.
Well Bottom; 1595.64 ft.

Completion: Date drilled; 8-12-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 120 ft.
Encountered water (below surface); 60 ft.
Geophysical log recorded

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.90-115.91 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 115.91-119.91 ft.
Elevation of interval; 1595.64-1599.64 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 114-120 ft.

Grout Seal: Depths (from ground); 0-114 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 49.41 ft. below top of casing
Elevation; 1668.23 ft.

Chemistry: Date; 8-21-86
pH; 7.95 Sp. cond; 1993 micromhos/cm
Temp; 8.6 oC

Well Number: 31

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CBA

Elevation: Ground; 1715.24 ft. Casing top; 1717.58 ft.
Well Bottom; 1635.58 ft.

Completion: Date drilled; 8-12-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 80 ft.
Encountered water (below surface); 60 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.34-75.66 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 75.66-79.66 ft.
Elevation of interval; 1635.58-1639.58 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 74-80 ft.

Grout Seal: Depths (from ground); 0-74 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 43.54 ft. below top of casing
Elevation; 1674.04 ft.

Chemistry: Date; 8-21-86
pH; 7.96 Sp. cond; 1993 micromhos/cm
Temp; 7.8 oC

Well Number: 32

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CBA

Elevation: Ground; 1715.34 ft. Casing top; 1717.79 ft.
Well Bottom; 1641.69 ft.

Completion: Date drilled; 8-12-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 80 ft.
Encountered water (below surface); 60 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.45-53.65 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 53.65-73.65 ft.
Elevation of interval; 1641.69-1661.69 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 52-75 ft.

Grout Seal: Depths (from ground); 0-52 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 42.03 ft. below top of casing
Elevation; 1675.76 ft.

Chemistry: Date; 8-21-86
pH; 7.22 Sp. cond; 3000 micromhos/cm
Temp; 8.0 oC

Well Number: 33

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CBA

Elevation: Ground; 1715.34 ft. Casing top; 1717.79 ft.
Well Bottom; 1672.79 ft.

Completion: Date drilled; 11-13-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry

Boring: Diameter; 5 5/8 in. Depth drilled; 45 ft.
Encountered water (below surface); ? ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.45-25.65 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 25.65-45.65 ft.
Elevation of interval; 1669.69-1689.69 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 24-45 ft.

Grout Seal: Depths (from ground); 0-24 ft.
Date sealed; 1-27-87

Additional Data:

Static Water Level: Date; 12-15-86
Depth; 40.68 ft. below top of casing
Elevation; 1677.11 ft.

Chemistry: Date; NA
pH; NA Sp. cond; NA
Temp; NA

Well Number: 40

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CDB

Elevation: Ground; 1708.02 ft. Casing top; 1710.15 ft.
Well Bottom; 1592.25 ft.

Completion: Date drilled; 8-13-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 120 ft.
Encountered water (below surface); 50 ft.
Geophysical log recorded

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.13-111.77 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 111.77-115.77 ft.
Elevation of interval; 1592.25-1596.25 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 110-117 ft.

Grout Seal: Depths (from ground); 0-117 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 63.72 ft. below top of casing
Elevation; 1646.43 ft.

Chemistry: Date; 8-21-86
pH; 7.58 Sp. cond; 6260 micromhos/cm
Temp; 8.2 oC

Well Number: 41

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CDB

Elevation: Ground; 1708.03 ft. Casing top; 1710.07 ft.
Well Bottom; 1626.77 ft.

Completion: Date drilled; 8-13-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 82 ft.
Encountered water (below surface); 50 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.04-77.26 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 77.26-81.26 ft.
Elevation of interval; 1626.77-1630.77 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 76-82 ft.

Grout Seal: Depths (from ground); 0-76 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 36.58 ft. below top of casing
Elevation; 1673.49 ft.

Chemistry: Date; 8-21-86
pH; 7.57 Sp. cond; 5480 micromhos/cm
Temp; 8.4 oC

Well Number: 42

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CDB

Elevation: Ground; 1708.12 ft. Casing top; 1710.31 ft.
Well Bottom; 1652.61 ft.

Completion: Date drilled; 8-13-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 60 ft.
Encountered water (below surface); 50 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.19-35.51 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 35.51-55.51 ft.
Elevation of interval; 1652.61-1672.61 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 34-56 ft.

Grout Seal: Depths (from ground); 0-34 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 32.88 ft. below top of casing
Elevation; 1677.43 ft.

Chemistry: Date; 8-21-86
pH; 7.22 Sp. cond; 5060 micromhos/cm
Temp; 8.6 oC

Well Number: 43

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CDD

Elevation: Ground; 1708.92 ft. Casing top; 1711.03 ft.
Well Bottom; 1650.14 ft.

Completion: Date drilled; 9-18-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry

Boring: Diameter; 5 5/8 in. Depth drilled; 60 ft.
Encountered water (below surface); 25 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.11-54.78 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 54.78-58.78 ft.
Elevation of interval; 1650.14-1654.14 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 53-59 ft.

Grout Seal: Depths (from ground); 0-53 ft.
Date sealed; 9-18-86

Additional Data:

Static Water Level: Date; 10-4-86
Depth; 25.85 ft. below top of casing
Elevation; 1685.18 ft.

Chemistry: Date; 10-4-86
pH; 6.70 Sp. cond; 6950 micromhos/cm
Temp; 8.5 oC

Well Number: 44

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CDD

Elevation: Ground; 1709.09 ft. Casing top; 1711.40 ft.
Well Bottom; 1685.88 ft.

Completion: Date drilled; 9-18-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry

Boring: Diameter; 5 5/8 in. Depth drilled; 25 ft.
Encountered water (below surface); 25 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.31-3.21 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 3.21-23.54 ft.
Elevation of interval; 1685.88-1705.88 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 2.5-24.0 ft.

Grout Seal: Depths (from ground); 0-2.5 ft.
Date sealed; 9-18-86

Additional Data:

Static Water Level: Date; 10-4-86
Depth; 21.92 ft. below top of casing
Elevation; 1689.48 ft.

Chemistry: Date; 10-4-86
pH; 6.72 Sp. cond; 10270 micromhos/cm
Temp; 9.1 oC

Well Number: 45

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CDB

Elevation: Ground; 1708.12 ft. Casing top; 1710.31 ft.
Well Bottom; 1668.12 ft.

Completion: Date drilled; 11-13-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;

Boring: Diameter; 5 5/8 in. Depth drilled; 40 ft.
Encountered water (below surface); ? ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.19-20.51 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 20.51-40.51 ft.
Elevation of interval; 1667.61-1687.61 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 19-41 ft.

Grout Seal: Depths (from ground); 0-19 ft.
Date sealed; 1-27-86

Additional Data:

Static Water Level: Date; 12-15-86
Depth; 28,71 ft. below top of casing
Elevation; 1681.60 ft.

Chemistry: Date; NA
pH; NA Sp. cond; NA
Temp; NA

Well Number: 50

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CAD

Elevation: Ground; 1674.58 ft. Casing top; 1677.01 ft.
Well Bottom; 1647.51 ft.

Completion: Date drilled; 8-13-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 30 ft.
Encountered water (below surface); 17 ft.
Geophysical log recorded

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.43-7.07 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 7.07-27.07 ft.
Elevation of interval; 1647.51-1667.51 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 6-29 ft.

Grout Seal: Depths (from ground); 0-6 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 5.45 ft. below top of casing
Elevation; 1671.56 ft.

Chemistry: Date; 8-21-86
pH; 7.56 Sp. cond; 6480 micromhos/cm
Temp; 10.8 oC

Well Number: 51

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CAD

Elevation: Ground; 1674.47 ft. Casing top; 1676.70 ft.
Well Bottom; 1637.33 ft.

Completion: Date drilled; 9-18-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 40 ft.
Encountered water (below surface); 18 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.23-32.14 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 32.14-37.14 ft.
Elevation of interval; 1637.33-1642.33 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 31-38 ft.

Grout Seal: Depths (from ground); 0-31 ft.
Date sealed; 9-18-86

Additional Data:

Static Water Level: Date; 10-4-86
Depth; 5.77 ft. below top of casing
Elevation; 1670.93 ft.

Chemistry: Date; 10-4-86
pH; 7.46 Sp. cond; 3700 micromhos/cm
Temp; 8.2 oC

Well Number: 52

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CAD

Elevation: Ground; 1674.45 ft. Casing top; 1676.71 ft.
Well Bottom; 1658.01 ft.

Completion: Date drilled; 9-18-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 20 ft.
Encountered water (below surface); 18 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.26-6.44 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 6.44-16.44 ft.
Elevation of interval; 1658.01-1668.01 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 5-18 ft.

Grout Seal: Depths (from ground); 0-5 ft.
Date sealed; 9-18-86

Additional Data:

Static Water Level: Date; 10-4-86
Depth; 4.13 ft. below top of casing
Elevation; 1672.58 ft.

Chemistry: Date; 10-4-86
pH; 7.29 Sp. cond; 6300 micromhos/cm
Temp; 9.4 oC

Well Number: 53

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10DCC

Elevation: Ground; 1685.71 ft. Casing top; 1688.17 ft.
Well Bottom; 1665.70 ft.

Completion: Date drilled; 9-18-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry

Boring: Diameter; 5 5/8 in. Depth drilled; 21 ft.
Encountered water (below surface); 15 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.46-5.01 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 5.01-20.01 ft.
Elevation of interval; 1665.70-1680.70 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 4-21 ft.

Grout Seal: Depths (from ground); 0-4 ft.
Date sealed; 9-18-86

Additional Data:

Static Water Level: Date; 10-4-86
Depth; 6.30 ft. below top of casing
Elevation; 1681.87 ft.

Chemistry: Date; 10-4-86
pH; NA Sp. cond; NA micromhos/cm
Temp; NA oC

Well Number: 54

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10DCC

Elevation: Ground; 1685.71 ft. Casing top; 1688.10 ft.
Well Bottom; 1633.11 ft.

Completion: Date drilled; 9-18-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry

Boring: Diameter; 5 5/8 in. Depth drilled; 60 ft.
Encountered water (below surface); 15 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.39-47.60 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 47.60-52.60 ft.
Elevation of interval; 1633.11-1638.11 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 46-54 ft.

Grout Seal: Depths (from ground); 0-46 ft.
Date sealed; 9-18-86

Additional Data:

Static Water Level: Date; 10-4-86
Depth; 15.16 ft. below top of casing
Elevation; 1672.94 ft.

Chemistry: Date; 10-4-86
pH; 9.55 Sp. cond; 1100 micromhos/cm
Temp; 9.8 oC

Well Number: 55

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10DCA

Elevation: Ground; 1693.86 ft. Casing top; 1696.10 ft.
Well Bottom; 1636.95 ft.

Completion: Date drilled; 9-18-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry

Boring: Diameter; 5 5/8 in. Depth drilled; 60 ft.
Encountered water (below surface); 45 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.24-31.91 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 31.91-56.91 ft.
Elevation of interval; 1636.95-1661.95 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 30-58 ft.

Grout Seal: Depths (from ground); 0-30 ft.
Date sealed; 9-18-86

Additional Data:

Static Water Level: Date; 10-4-86
Depth; 29.46 ft. below top of casing
Elevation; 1666.64 ft.

Chemistry: Date; 10-4-86
pH; 6.81 Sp. cond; 10840 micromhos/cm
Temp; 8.5 oC

Well Number: 56

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-80-10DCA

Elevation: Ground; 1693.86 ft. Casing top; 1696.42 ft.
Well Bottom; 1597.99 ft.

Completion: Date drilled; 9-18-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry

Boring: Diameter; 5 5/8 in. Depth drilled; 100 ft.
Encountered water (below surface); 45 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.56-91.87 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 91.87-96.87 ft.
Elevation of interval; 1597.99-1601.99 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 90-98 ft.

Grout Seal: Depths (from ground); 0-90 ft.
Date sealed; 9-18-86

Additional Data:

Static Water Level: Date; 10-4-86
Depth; 42.03 ft. below top of casing
Elevation; 1654.39 ft.

Chemistry: Date; 10-4-86
pH; 8.44 Sp. cond; 4160 micromhos/cm
Temp; 8.3 oC

Well Number: 60

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-18-10CDB

Elevation: Ground; 1714.23 ft. Casing top; 1716.42 ft.
Well Bottom; 1662.02 ft.

Completion: Date drilled; 8-13-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 60 ft.
Encountered water (below surface); 45 ft.
Geophysical log recorded

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.19-22.21 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 22.21-52.21 ft.
Elevation of interval; 1662.02-1692.02 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 21-54 ft.

Grout Seal: Depths (from ground); 0-21 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 31.01 ft. below top of casing
Elevation; 1685.41 ft.

Chemistry: Date; 8-21-86
pH; 6.94 Sp. cond; 15760 micromhos/cm
Temp; 8.5 oC

Well Number: 61

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CDA

Elevation: Ground; 1714.23 ft. Casing top; 1716.53 ft.
Well Bottom; 1670.89 ft.

Completion: Date drilled; 9-18-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry

Boring: Diameter; 5 5/8 in. Depth drilled; 46 ft.
Encountered water (below surface); 37 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.30-13.34 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 13.34-43.34 ft.
Elevation of interval; 1670.89-1700.89 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 12-45 ft.

Grout Seal: Depths (from ground); 0-12 ft.
Date sealed; 9-18-86

Additional Data:

Static Water Level: Date; 10-4-86
Depth; 32.58 ft. below top of casing
Elevation; 1683.95 ft.

Chemistry: Date; 10-4-86
pH; 6.83 Sp. cond; 12750 micromhos/cm
Temp; 8.4 oC

Well Number: 62

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10CDB

Elevation: Ground; 1714.32 ft. Casing top; 1716.67 ft.
Well Bottom; 1681.40 ft.

Completion: Date drilled; 9-18-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry

Boring: Diameter; 5 5/8 in. Depth drilled; 35 ft.
Encountered water (below surface); 35 ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.35-12.92 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 12.92-32.91 ft.
Elevation of interval; 1681.40-1701.40 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 11-34 ft.

Grout Seal: Depths (from ground); 0-11 ft.
Date sealed; 9-18-86

Additional Data:

Static Water Level: Date; 10-4-86
Depth; 32.74 ft. below top of casing
Elevation; 1683.93 ft.

Chemistry: Date; 10-4-86
pH; 6.71 Sp. cond; 13170 micromhos/cm
Temp; 9.3 oC

Well Number: 70

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-16ABA

Elevation: Ground; 1733.18 ft. Casing top; 1735.67 ft.
Well Bottom; 1634.57 ft.

Completion: Date drilled; 8-13-86
Driller; Mohl Drilling, Beulah, ND
Method of drilling; Air rotary, dry;
some air-mist

Boring: Diameter; 5 5/8 in. Depth drilled; 102 ft.
Encountered water (below surface); 45 ft.
Geophysical log recorded

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.49-94.61 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 94.61-98.61 ft.
Elevation of interval; 1634.57-1638.57 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 93-99 ft.

Grout Seal: Depths (from ground); 0-93 ft.
Date sealed; 8-13-86

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 54.20 ft. below top of casing
Elevation; 1681.47 ft.

Chemistry: Date; 8-21-86
pH; 7.85 Sp. cond; 13000 micromhos/cm
Temp; 10.1 oC

Well Number: (WS1)

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-DBB

Elevation: Ground; 1679.61 ft. Casing top; 1681.71 ft.
Well Bottom; 1606.73 ft.
Repaired casing top (1-13-86); 1683.67 ft.

Completion: Date drilled; 9-22-81
Driller; Water Supply, Inc.
Method of drilling; NA

Boring: Diameter; NA in. Depth drilled; 73 ft.
Encountered water (below surface); NA ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +2.7-40, 45-73 ft.
(as of 1-13-87); +4.7-40, 45-73 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 40-45 ft.
Elevation of interval; 1634.61-1639.61 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 37-47 ft.

Grout Seal: Depths (from ground); 0-37 ft.
Date sealed; NA

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 24.61 ft. below top of casing
Elevation; 1657.10 ft.

Chemistry: Date; 8-21-86
pH; 7.47 Sp. cond; 1899 micromhos/cm
Temp 7.0 oC

Well Number: (WS1A)

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-DBB

Elevation: Ground; 1679.10 ft. Casing top; 1682.23 ft.
Well Bottom; 1657.10 ft.

Completion: Date drilled; 8-5-85
Driller; Water Supply, Inc.
Method of drilling; NA

Boring: Diameter; NA in. Depth drilled; 23 ft.
Encountered water (below surface); NA ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +3.2-17 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 17-22 ft.
Elevation of interval; 1657.10-1662.10 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 15-23 ft.

Grout Seal: Depths (from ground); 0-15 ft.
Date sealed; NA

Additional Data:

Static Water Level: Date; 8-21-86
Depth; DRY ft. below top of casing
Elevation; ft.

Chemistry: Date: 8-21-86
pH; NA Sp. cond; NA micromhos/cm
Temp; NA oC

Well Number: (WS1B)

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10DBB

Elevation: Ground; 1678.80 ft. Casing top; 1682.07 ft.
Well Bottom; 1648.80 ft.

Completion: Date drilled; 8-6-85
Driller; Water Supply, Inc.
Method of drilling; NA

Boring: Diameter; NA in. Depth drilled; 30 ft.
Encountered water (below surface); NA ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +3.3-25 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 25-30 ft.
Elevation of interval; 1648.80-1653.80 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 23-30 ft.

Grout Seal: Depths (from ground); 0-22 ft.
Date sealed; NA

Additional Data:

Static Water Level: Date; 8-21-86
Depth; 24.48 ft. below top of casing
Elevation; 1657.59 ft.

Chemistry: Date; 8-21-86
pH; 7.07 Sp. cond; 3940 micromhos/cm
Temp; 8.5 oC

Well Number: (WS2)

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10DCC

Elevation: Ground; 1696.00 ft. Casing top; 1698.64 ft.
Well Bottom; 1607.00 ft.

Completion: Date drilled; 9-23-81
Driller; Water Supply, Inc.
Method of drilling; NA

Boring: Diameter; NA in. Depth drilled; 90 ft.
Encountered water (below surface); NA ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +3-56, 61-89 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 56-61 ft.
Elevation of interval; 1635.00-1640.00 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 53-62 ft.

Grout Seal: Depths (from ground); 0-52 ft.
Date sealed; NA

Additional Data:

Static Water Level: Date; 10-4-86
Depth; 33.86 ft. below top of casing
Elevation; 1664.78 ft.

Chemistry: Date; 8-21-86
pH; 7.04 Sp. cond; 3760 micromhos/cm
Temp; 8.6 oC

Well Number: (WS3)

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10DBA

Elevation: Ground; 1658.00 ft. Casing top; 1661.00 ft.
Well Bottom; 1608.00 ft.

Completion: Date drilled; 9-21-81
Driller; Water Supply, Inc.
Method of drilling; NA

Boring: Diameter; NA in. Depth drilled; 50 ft.
Encountered water (below surface); NA ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +3-25, 30-50 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 25-30 ft.
Elevation of interval; 1628.00-1633.00 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 24-32 ft.

Grout Seal: Depths (from ground); 0-23 ft.
Date sealed; NA

Additional Data:

Static Water Level: Date; 9-4-86
Depth; 14.67 ft. below top of casing
Elevation; 1646.33 ft.

Chemistry: Date; NA
pH; NA Sp. cond; NA micromhos/cm
Temp; NA oC

Well Number: (WS3A)

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10DBA

Elevation: Ground; 1657.70 ft. Casing top; 1660.81 ft.
Well Bottom; 1645.31 ft.

Completion: Date drilled; 8-5-85
Driller; Water Supply, Inc.
Method of drilling; NA

Boring: Diameter; NA in. Depth drilled; 13 ft.
Encountered water (below surface); NA ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +3.1-7.5 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 7.5-12.5 ft.
Elevation of interval; 1645.31-1650.31 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 6-13 ft.

Grout Seal: Depths (from ground); 0-6 ft.
Date sealed; NA

Additional Data:

Static Water Level: Date; 10-4-86
Depth; 8.37 ft. below top of casing
Elevation; 1652.44 ft.

Chemistry: Date; NA
pH; NA Sp. cond; NA micromhos/cm
Temp; NA oC

Well Number: (WS4)

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10DBA

Elevation: Ground; 1659.61 ft. Casing top; 1662.61 ft.
Well Bottom; 1607.60 ft.

Completion: Date drilled; 9-24-81
Driller; Water Supply, Inc.
Method of drilling; NA

Boring: Diameter; NA in. Depth drilled; 52 ft.
Encountered water (below surface); NA ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +3-30, 35-52 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 30-35 ft.
Elevation of interval; 1624.60-1629.60 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 27-36 ft.

Grout Seal: Depths (from ground); 0-26 ft.
Date sealed; NA

Additional Data:

Static Water Level: Date; 9-4-86
Depth; 19.62 ft. below top of casing
Elevation; 1642.99 ft.

Chemistry: Date; NA
pH; NA Sp. cond; NA micromhos/cm
Temp; NA oC

Well Number: (WS4A)

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10DBA

Elevation: Ground; 1659.49 ft. Casing top; 1662.49 ft.
Well Bottom; 1641.50 ft.

Completion: Date drilled; 9-24-81
Driller; Water Supply, Inc.
Method of drilling; NA

Boring: Diameter; NA in. Depth drilled; 18 ft.
Encountered water (below surface); NA ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +3-13 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 13-18 ft.
Elevation of interval; 1641.50-1646.50 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 11-18 ft.

Grout Seal: Depths (from ground); 0-11 ft.
Date sealed; NA

Additional Data:

Static Water Level: Date; 9-4-86
Depth; 17.29 ft. below top of casing
Elevation; 1645.20 ft.

Chemistry: Date; NA
pH; NA Sp. cond; NA micromhos/cm
Temp; NA oC

Well Number: (WS4B)

Project: MDU Ash Disposal Program

Construction Data:

Location: 139-81-10DBA

Elevation: Ground; 1659.75 ft. Casing top; 1662.75 ft.
Well Bottom; 1635.80 ft.

Completion: Date drilled; 8-5-85
Driller; Water Supply, Inc.
Method of drilling; NA

Boring: Diameter; NA in. Depth drilled; 25 ft.
Encountered water (below surface); NA ft.

Casing: Diameter; 2 in. Material; Sch. 40 PVC
Depths (from ground); +3.1-19.0 ft.

Screen: Diameter; 2 in. Slot size; 20
Material; Factory slotted PVC
Depths (from ground); 19-24 ft.
Elevation of interval; 1635.80-1640.80 ft.

Sand Pack: Type of sand; Washed sand
Depths (from ground); 18-25 ft.

Grout Seal: Depths (from ground); 0-18 ft.
Date sealed; NA

Additional Data:

Static Water Level: Date; 9-4-86
Depth; 17.39 ft. below top of casing
Elevation; 1645.36 ft.

Chemistry: Date; NA
pH; NA Sp. cond; NA micromhos/cm
Temp; NA oC

EXHIBIT 5-D

GEOPHYSICAL LOGS

EXHIBIT 5-E

LITHOLOGIC LOGS

Wells 10, 11, 12 and 13

- 0-1 Top soil, silty, clayey, sandy, brown, calcareous; with some limestone pebbles.
- 1-11 Silt, clayey, brownish-tan, slightly indurated, very dry, calcareous; with thin coarse-grained, clean silt lenses and a few small (less than .5 in.) iron oxide concretions. Abundant small gypsum crystals (less than .13 in. long). Some small, black flakes of organic plant material. Cannonball-Ludlow Formations.
- 11-14 Silt, as above, with some (less than 20%) very fine- to fine-grained sand interspersed.
- 14-30 Silt, as above, clayey, less sand than above interval, oxidized; with very fine-grained silty sand lenses and very few gypsum crystals.
- 30-41 Silt, very clayey, with some (less than 20%) very fine-grained sand interspersed, steel-gray (color change), moderately indurated; with fewer small gypsum crystals than above intervals.
- 41-59 Silt, as above, very clayey, with some (less than 20%) fine- to medium-grained sand interspersed in a silt and clay matrix.
- 59-65 Silt, as above, with abundant (more than 20%) fine- to medium-grained sand interspersed.
- 65-81 Silt, clayey, steel-gray to bluish, moderately indurated; with thin coarse-grained silt to very fine-grained sand lenses in an otherwise fine silt to clay matrix.
- 81-84 Clay, silty, steel-gray to bluish, moderately indurated, dense.
- 84-91 Siltstone, sandy, clayey, steel-gray to bluish, slightly indurated; with small fine-grained sand lenses and abundant (more than 20%) sand interspersed in the matrix.
- 91-110 Silt, clayey, bluish-gray, moderately indurated; with thin (less than 1 foot) mudstone lenses.
- 110-120 Silt, very clayey, steel-gray to bluish, moderately indurated, very dense. Cannonball-Ludlow Formations.

Wells 20 and 21

- 0-1 Top soil, silty, sandy, clayey, dark-brown, calcareous; with some limestone and granite pebbles.
- 1-21 Silt, clayey, with minor amounts (less than 10%) of very fine-grained sand interspersed, brownish-tan, slightly indurated, calcareous, oxidized; with small iron oxide concretions and abundant small gypsum crystals.
Cannonball-Ludlow Formations.
- 21-26 Silt, as above, steel-gray (color change).
- 26-49 Silt, clayey, with some (less than 20%) very fine- to medium-grained sand interspersed, steel-gray to bluish, slightly indurated; with very few small gypsum crystals and some thin (less than 1 foot) siltstone lenses.
- 49-53 Silt, as above, with abundant (more than 20%) fine- to medium-grained sand interspersed.
- 53-63 Silt, as above, clayey, less sand, with thin (less than 1 foot) siltstone to mudstone lenses.
- 63-80 Silt, very clayey, steel-gray to bluish, moderately indurated, very dense.
Cannonball-Ludlow Formations.

Wells 30, 31, 32 and 33

- 0-1 Top soil, silty, sandy, brownish, calcareous; with some granite and limestone pebbles.
- 1-2 Pebble-loam (glacial till), silty, sandy, clayey, yellowish-brown, dry, calcareous.
- 2-31 Silt, clayey, with minor amounts (less than 10%) of very fine-grained sand interspersed, brownish-tan, slightly indurated, calcareous, oxidized; with small iron oxide concretions. Some small, black flakes organic plant material.
Cannonball-Ludlow Formations.
- 31-44 Silt, clayey, steel-gray (color change), slightly indurated, calcareous; with small iron oxide concretions, thin coarse silt lenses, small gypsum crystals and gray to reddish-brown mottling.

- 44-61 Silt, as above, with some (less than 20%) fine- to medium-grained sand interspersed.
- 61-65 Silt, as above, with abundant (more than 20%) fine- to medium-grained sand interspersed, dense.
- 65-76 Silt, as above, clayey, less sand, some thin (less than 1 foot) lenses of siltstone to mudstone.
- 76-80 Siltstone, sandy, clayey, steel-gray to bluish, slightly indurated; with small fine-grained sand lenses and abundant (more than 20%) fine-grained sand interspersed in the matrix.
- 80-92 Silt, clayey, steel-gray to bluish, moderately indurated, with some (less than 20%) very fine- to fine grained sand interspersed.
- 92-120 Silt, very clayey, steel-gray to bluish, moderately indurated, very dense.
Cannonball-Ludlow Formations.

Well 40

- 0-1 Top soil, sandy, silty, brownish-tan, calcareous; with some granite and limestone pebbles.
- 1-5 Pebble-loam (glacial till), sandy, silty, with detrital lignite and organic matter, yellowish-brown, very dry, calcareous.
- 5-22 Sand, very fine- to medium-grained, unconsolidated, with thin lenses of clay and detrital lignite, brownish-yellow, calcareous.
- 22-40 Silt, clayey, with minor amounts (less than 10%) very fine-grained sand interspersed, brownish-tan, slightly indurated, calcareous, oxidized; with small iron oxide concretions and small gypsum crystals; Cannonball-Ludlow Formations.
- 40-51 Silt, clayey, with minor amounts (less than 10%) of very fine-grained sand interspersed, steel-gray (color change), moderately indurated; with some reddish-brown mottling and some very thin (less than 6 inches) mudstone lenses.
- 51-58 Silt, as above, with abundant (more than 20%) fine-grained sand and thin silty-clay lenses.

- 58-62 Siltstone, sandy, clayey, steel-gray to bluish, moderately indurated; with small fine-grained sand lenses and abundant (more than 20%) sand interspersed in the matrix.
- 62-70 Silt, clayey, with some (less than 20%) fine- to medium-grained sand interspersed, steel-gray to bluish, moderately indurated; with thin (less than 2 feet) sandy lenses.
- 70-80 Silt, as above, very clayey, some (less than 10%) fine-grained sand interspersed; less sand than above interval.
- 80-120 Silt, as above, dark-steel-gray.
Cannonball-Ludlow Formations.

Wells 41, 42 and 43

- 0-1 Top soil, sandy, silty, dark-brown, calcareous; with some granite and limestone pebbles.
- 1-4 Pebble-loam (glacial till), sandy, silty, clayey, yellowish-brown, very dry, calcareous.
- 4-40 Silt, clayey, with some (less than 20%) very fine-grained sand interspersed, brownish-tan, unconsolidated, noncompacted, calcareous to 25 feet, oxidized; with small iron oxide concretions and abundant small gypsum crystals.
Cannonball-Ludlow Formations.
- 40-51 Silt, clayey, with minor amounts (less than 10%) of very fine-grained sand interspersed, steel-gray (color change), moderately indurated; with some reddish-brown mottling and some very thin (less than 6 inches) mudstone lenses.
- 51-58 Silt, as above, with abundant (more than 20%) fine-grained sand and thin silty-clay lenses.
- 58-62 Siltstone, sandy, clayey, steel-gray to bluish, moderately indurated; with small fine-grained sand lenses and abundant (more than 20%) sand interspersed in the matrix.
- 62-70 Silt, clayey, with some (less than 20%) fine- to medium-grained sand interspersed, steel-gray to bluish, moderately indurated; with thin (less than 2 feet) sandy lenses.

30-40 Silt, as above, very clayey, less sand than above interval, dark-steel-gray.
Cannonball-Ludlow Formations.

Wells 53 and 54

- 0-4 Top soil, clayey, silty, very dark-brown, wet, sticky.
- 4-15 Clay, silty, with some (less than 20%) fine- to medium-grained sand interspersed, brownish-tan, slightly indurated, dry, calcareous; with small iron oxide concretions, small gypsum crystals and occasional reddish-brown mottling;
Cannonball-Ludlow Formations.
- 15-20 Sand, very fine-grained to medium-grained, silty, clayey, unconsolidated, yellowish-brown, oxidized.
- 20-30 Silt, clayey, with some (less than 20%) fine-grained sand interspersed, steel-gray (color change), slightly indurated; with clay and sand lenses, some small concretions and some small gypsum crystals.
- 30-45 Silt, as above, very clayey.
- 45-60 Silt, as above, clayey, brownish-gray, moderately indurated, some reddish-brown mottling.
Cannonball-Ludlow Formations.

Wells 55 and 56

- 0-5 Sandy-loam (glacial), with fine- to medium-grained sand, silty, calcareous; with small granite and limestone pebbles.
- 5-26 Clay, silty, with minor amounts (less than 10%) of very fine-grained sand, dark-brownish-tan, moderately indurated, brittle, very dry, calcareous; with small iron oxide concretions, small gypsum crystals and occasional thin sandstone laminae. Some small, black flakes of organic plant material.
Cannonball-Ludlow Formations.
- 26-35 Clay, as above, very silty, sandy, brownish-tan, oxidized.

- 35-40 Silt, clayey, with some (less than 20%) very fine- to fine-grained sand interspersed, steel-gray (color change) moderately indurated; with small gypsum crystals and occasional clay lenses.
- 40-60 Silt, as above, with minor amounts (less than 10%) of fine-grained sand interspersed.
- 60-85 Silt, as above, clayey, less sand than above interval.
- 85-100 Silt, as above, very clayey, with minor amounts (less than 10%) of sand interspersed, light-gray. Cannonball-Ludlow Formations.

Wells 60, 61 and 62

- 0-2 Top soil, silty, clayey, dark-brown to tanish-brown, calcareous.
- 2-25 Silt, very clayey, with some minor amounts (less than 10%) of very fine- to fine-grained sand interspersed, brownish-tan, slightly indurated, dry, calcareous; with abundant small gypsum crystals and thin silt and sand lenses; Cannonball-Ludlow Formations.
- 25-29 Silt, as above, with abundant (more than 20%) fine- to medium-grained sand interspersed.
- 29-36 Silt, as above, clayey, less sand than above interval, dark-brownish-tan, oxidized.
- 36-60 Silt, very clayey, with some (less than 20%) very fine-grained sand interspersed, steel-gray (color change), moderately indurated; with thin (less than 1 foot) sandy-silt lenses. Cannonball-Ludlow Formations.

Well 70 0-2 Pebble-loam (glacial till), clayey, sandy, yellowish-brown, unconsolidated, damp, calcareous.

- 2-21 Silty, clayey, with some (less than 20%) fine-grained sand interspersed, brownish-tan, moderately indurated, very dry, calcareous, oxidized; with small iron oxide concretions and abundant small gypsum crystals. Cannonball-Ludlow Formations.

- 21-24 Shale, silty, steel- to dark-gray (color change), indurated, fissile, very dry; with occasional thin silt and sand lenses.
- 24-31 Silt, clayey, with abundant (more than 30%) sand, steel-gray, moderately indurated.
- 31-62 Silt, clayey, with some (less than 20%) very fine- to fine- grained sand interspersed, steel-gray, moderately indurated; with some small gypsum crystals and small iron oxide concretions.
- 62-76 Silt, as above, with some (less than 20%) fine-grained sand interspersed.
- 76-82 Silt, as above, with abundant (more than 20%) fine- to medium-grained sand.
- 82-100 Silt, as above, clayey, with some (less than 20%) fine-grained sand interspersed, dark-gray.
Cannonball-Ludlow Formations.

EXHIBIT 5-F

SITE SOILS CLASSIFICATION MAP

EXHIBIT 5-G

WATER LEVEL DATA

HESKETT SWL INFORMATION

WELL DATA

WELL NO.	TOP OF CASE	GROUND SURFACE	SCREENED	INTERVAL	CASING HEIGHT
10	1725.01	1722.06	1604.01	to 1608.01	2.95
11	1725.01	1722.10	1642.81	to 1646.81	2.91
12	1724.90	1721.88	1643.51	to 1663.51	3.02
13	1724.98	1721.80	1681.51	to 1701.51	3.18
20	1709.48	1707.04	1627.48	to 1631.48	2.44
21	1709.40	1707.22	1661.90	to 1685.90	2.18
30	1717.64	1715.55	1595.64	to 1599.64	2.09
31	1717.58	1715.24	1635.58	to 1639.58	2.34
32	1717.79	1715.34	1641.69	to 1661.69	2.45
33	1717.91	1715.48	1669.69	to 1689.69	2.43
40	1710.15	1708.02	1592.25	to 1596.25	2.13
41	1710.07	1708.03	1626.77	to 1630.77	2.04
42	1710.31	1708.12	1652.61	to 1672.61	2.19
43	1711.03	1708.92	1650.14	to 1654.14	2.11
44	1711.40	1709.09	1685.88	to 1705.88	2.31
45	1710.17	1708.34	1667.61	to 1687.61	1.83
50	1677.01	1674.58	1647.51	to 1667.51	2.43
51	1676.70	1674.47	1637.33	to 1642.33	2.23
52	1676.71	1674.45	1658.01	to 1668.01	2.26
53	1688.17	1685.71	1665.70	to 1680.70	2.46
54	1688.10	1685.71	1633.11	to 1638.11	2.39
55	1696.10	1693.86	1636.95	to 1661.95	2.24
56	1696.42	1693.86	1597.99	to 1601.99	2.56
60	1716.42	1714.23	1662.02	to 1692.02	2.19
61	1716.53	1714.23	1670.89	to 1700.89	2.30
62	1716.67	1714.32	1681.40	to 1701.40	2.35
70	1735.67	1733.18	1634.57	to 1638.57	2.49
WS2	1698.64	1696.00	1635.00	to 1640.00	2.64
WS1	1681.71	1679.61	1634.61	to 1639.61	2.10
WS1	1683.67	as of 1-3-87			4.06
WS1A	1682.23	1679.10	1657.10	to 1662.10	3.13
WS1B	1682.07	1678.80	1648.80	to 1653.80	3.27
WS4	1662.61	1659.61	1624.60	to 1629.60	3.00
WS4A	1662.49	1659.49	1641.50	to 1646.50	3.00
WS4B	1662.75	1659.75	1635.80	to 1640.80	3.00
WS3	1661.00	1658.00	1628.00	to 1633.00	3.00
WS3A	1660.81	1657.70	1645.31	to 1650.31	3.11

CASING ON WELL WS1 WAS REPAIRED IN JANUARY, 1987

ALL VALUES ARE IN FEET ABOVE MEAN SEA LEVEL

SWL-TOP = STATIC WATER LEVEL (in feet) FROM TOP OF CASING
 SWL-MSL = STATIC WATER LEVEL (in feet) AT MEAN SEA LEVEL
 SWL-BLS = STATIC WATER LEVEL (in feet) BELOW LAND SURFACE

HESKETT SWL INFORMATION

WELL NO.	DATE	SWL-TOP	SWL-MSL	SWL-BLS
10	9-11-86	51.64	1673.37	48.69
	10-16-86	53.32	1671.69	50.37
	11-21-86	53.58	1671.43	50.63
	1-13-87	53.71	1671.30	50.76
	3-6-87	53.61	1671.40	50.66
	4-21-87	53.45	1671.56	50.50
	6-3-87	53.48	1671.53	50.53
	5-11-88	54.79	1670.22	51.84
	9-12-88	55.05	1669.96	52.10
1-4-89	56.33	1668.68	53.38	
11	9-11-86	42.42	1682.59	39.51
	10-16-86	41.47	1683.54	38.56
	11-21-86	40.88	1684.13	37.97
	1-13-87	40.72	1684.29	37.81
	3-6-87	40.59	1684.42	37.68
	4-21-87	40.72	1684.29	37.81
	6-3-87	40.65	1684.36	37.74
	5-11-88	42.62	1682.39	39.71
	9-12-88	43.67	1681.34	40.76
1-4-89	44.10	1680.91	41.19	
12	9-11-86	42.42	1682.48	39.40
	10-16-86	40.55	1684.35	37.53
	11-21-86	40.00	1684.90	36.98
	1-13-87	39.86	1685.04	36.84
	3-6-87	39.77	1685.13	36.75
	4-21-87	39.83	1685.07	36.81
	6-3-87	39.90	1685.00	36.88
	5-11-88	41.90	1683.00	38.88
	9-12-88	43.21	1681.69	40.19
1-4-89	43.37	1681.53	40.35	
13	12-15-86	30.09	1694.89	26.91
	1-13-87	29.99	1694.99	26.81
	3-6-87	30.15	1694.83	26.97
	4-21-87	29.92	1695.06	26.74
	6-3-87	29.86	1695.12	26.68
	5-11-88	31.27	1693.71	28.09
	9-12-88	31.53	1693.45	28.35
	1-4-89	31.69	1693.29	28.51

HESKETT SWL INFORMATION

WELL NO.	DATE	SWL-TOP	SWL-MSL	SWL-BLS
20	9-11-86	37.17	1672.31	34.73
	10-16-86	36.85	1672.63	34.41
	11-21-86	36.75	1672.73	34.31
	1-13-87	36.68	1672.80	34.24
	3-6-87	35.09	1674.39	32.65
	4-21-87	35.73	1673.75	33.29
	6-3-87	35.93	1673.55	33.49
	5-11-88	37.93	1671.55	35.49
	9-12-88	39.80	1669.68	37.36
	1-4-89	40.16	1669.32	37.72
21	9-11-86	29.17	1680.23	26.99
	10-16-86	28.94	1680.46	26.76
	11-21-86	28.61	1680.79	26.43
	1-13-87	28.51	1680.89	26.33
	3-6-87	28.41	1680.99	26.23
	4-21-87	27.95	1681.45	25.77
	6-3-87	28.12	1681.28	25.94
	5-11-88	30.77	1678.63	28.59
	9-12-88	32.22	1677.18	30.04
	1-4-89	33.07	1676.33	30.89

HESKETT SWL INFORMATION

WELL NO.	DATE	SWL-TOP	SWL-MSL	SWL-BLS
30	9-11-86	49.38	1668.26	47.29
	10-16-86	49.35	1668.29	47.26
	11-21-86	49.28	1668.36	47.19
	1-13-87	49.15	1668.49	47.06
	3-6-87	48.53	1669.11	46.44
	4-21-87	48.10	1669.54	46.01
	6-3-87	48.36	1669.28	46.27
	5-11-88	50.36	1667.28	48.27
	9-12-88	51.97	1665.67	49.88
	1-4-89	52.40	1665.24	50.31
31	9-11-86	43.21	1674.37	40.87
	10-16-86	43.74	1673.84	41.40
	11-21-86	43.74	1673.84	41.40
	1-13-87	43.41	1674.17	41.07
	3-6-87	42.59	1674.99	40.25
	4-21-87	42.26	1675.32	39.92
	6-3-87	42.59	1674.99	40.25
	5-11-88	45.01	1672.57	42.67
	9-12-88	46.88	1670.70	44.54
	1-4-89	47.31	1670.27	44.97
32	9-11-86	42.52	1675.27	40.07
	10-16-86	42.03	1675.76	39.58
	11-21-86	41.87	1675.92	39.42
	1-13-87	41.18	1676.61	38.73
	3-6-87	40.29	1677.50	37.84
	4-21-87	40.00	1677.79	37.55
	6-3-87	40.39	1677.40	37.94
	5-11-88	43.18	1674.61	40.73
	9-12-88	45.18	1672.61	42.73
	1-4-89	45.65	1672.14	43.20
33	12-15-86	40.68	1677.23	38.25
	1-13-87	40.72	1677.19	38.29
	3-6-87	39.73	1678.18	37.30
	4-21-87	39.01	1678.90	36.58
	6-3-87	39.54	1678.37	37.11
	5-11-88	42.06	1675.85	39.63
	9-12-88	43.57	1674.34	41.14
	1-4-89	44.03	1673.88	41.60

HESKETT SWL INFORMATION

WELL NO.	DATE	SWL-TOP	SWL-MSL	SWL-BLS
40	9-11-86	63.82	1646.33	61.69
	10-16-86	63.68	1646.47	61.55
	11-21-86	63.29	1646.86	61.16
	1-13-87	63.39	1646.76	61.26
	3-6-87	63.06	1647.09	60.93
	4-21-87	63.16	1646.99	61.03
	6-3-87	63.26	1646.89	61.13
	5-11-88	63.36	1646.79	61.23
	9-12-88	63.72	1646.43	61.59
	1-4-89	63.89	1646.26	61.76
41	9-11-86	36.29	1673.78	34.25
	10-16-86	36.09	1673.98	34.05
	11-21-86	35.93	1674.14	33.89
	1-13-87	36.16	1673.91	34.12
	3-6-87	35.83	1674.24	33.79
	4-21-87	35.43	1674.64	33.39
	6-3-87	35.63	1674.44	33.59
	5-11-88	37.40	1672.67	35.36
	9-12-88	39.21	1670.86	37.17
	1-4-89	39.70	1670.37	37.66
42	9-11-86	33.30	1677.01	31.11
	10-16-86	32.74	1677.57	30.55
	11-21-86	31.43	1678.88	29.24
	1-13-87	31.46	1678.85	29.27
	3-6-87	31.27	1679.04	29.08
	4-21-87	31.20	1679.11	29.01
	6-3-87	31.30	1679.01	29.11
	5-11-88	32.61	1677.70	30.42
	9-12-88	33.96	1676.35	31.77
	1-4-89	34.12	1676.19	31.93
45	12-15-86	28.71	1681.46	26.88
	1-13-87	28.58	1681.59	26.75
	3-6-87	28.48	1681.69	26.65
	4-21-87	28.58	1681.59	26.75
	6-3-87	28.71	1681.46	26.88
	5-11-88	29.89	1680.28	28.06
	9-12-88	30.84	1679.33	29.01
	1-4-89	30.97	1679.20	29.14

HESKETT SWL INFORMATION

WELL NO	DATE	SWL-TOP	SWL-MSL	SWL-BLS
43	10-16-86	26.02	1685.01	23.91
	11-21-86	25.82	1685.21	23.71
	1-13-87	26.08	1684.95	23.97
	3-6-87	25.89	1685.14	23.78
	4-21-87	26.12	1684.91	24.01
	6-3-87	26.58	1684.45	24.47
	5-11-88	27.56	1683.47	25.45
	9-12-88	29.92	1681.11	27.81
	1-4-89	29.20	1681.83	27.09
44	10-16-86	21.98	1689.42	19.67
	11-21-86	21.85	1689.55	19.54
	1-13-87	22.15	1689.25	19.84
	3-6-87	22.05	1689.35	19.74
	4-21-87	21.72	1689.68	19.41
	6-3-87	22.21	1689.19	19.90
	5-11-88	23.46	1687.94	21.15
	9-12-88	dry		
	1-4-89	24.87	1686.53	22.56

HESKETT SWL INFORMATION

WELL NO.	DATE	SWL-TOP	SWL-MSL	SWL-BLS
50	9-11-86	5.45	1671.56	3.02
	10-16-86	4.53	1672.48	2.10
	11-21-86	4.17	1672.84	1.74
	1-13-87	4.76	1672.25	2.33
	3-6-87	not taken		
	4-21-87	3.74	1673.27	1.31
	6-3-87	4.33	1672.68	1.90
	5-11-88	5.41	1671.60	2.98
	9-12-88	7.87	1669.14	5.44
	1-4-89	7.97	1669.04	5.54
51	10-16-86	6.43	1670.27	4.20
	11-21-86	6.07	1670.63	3.84
	1-13-87	6.30	1670.40	4.07
	3-6-87	5.94	1670.76	3.71
	4-21-87	5.45	1671.25	3.22
	6-3-87	5.74	1670.96	3.51
	5-11-88	7.35	1669.35	5.12
	9-12-88	9.61	1667.09	7.38
	1-4-89	9.81	1666.89	7.58
52	10-16-86	4.43	1672.28	2.17
	11-21-86	4.07	1672.64	1.81
	1-13-87	4.56	1672.15	2.30
	3-6-87	3.81	1672.90	1.55
	4-21-87	3.61	1673.10	1.35
	6-3-87	4.20	1672.51	1.94
	5-11-88	4.99	1671.72	2.73
	9-12-88	7.81	1668.90	5.55
	1-4-89	7.89	1668.82	5.63

HESKETT SWL INFORMATION

WELL NO.	DATE	SWL-TOP	SWL-MSL	SWL-BLS
53	10-16-86	6.66	1681.51	4.20
	11-21-86	6.46	1681.71	4.00
	1-13-87	6.92	1681.25	4.46
	3-6-87	7.55	1680.62	5.09
	4-21-87	6.17	1682.00	3.71
	6-3-87	7.32	1680.85	4.86
	5-11-88	7.51	1680.66	5.05
	9-12-88	11.25	1676.92	8.79
	1-4-89	10.93	1677.24	8.47
54	10-16-86	21.36	1666.74	18.97
	11-21-86	20.97	1667.13	18.58
	1-13-87	20.87	1667.23	18.48
	3-6-87	21.00	1667.10	18.61
	4-21-87	20.70	1667.40	18.31
	6-3-87	20.54	1667.56	18.15
	5-11-88	22.28	1665.82	19.89
	9-12-88	23.13	1664.97	20.74
	1-4-89	23.62	1664.48	21.23
55	10-16-86	29.46	1666.64	27.22
	11-21-86	29.50	1666.60	27.26
	1-13-87	29.56	1666.54	27.32
	3-6-87	29.30	1666.80	27.06
	4-21-87	29.30	1666.80	27.06
	6-3-87	29.13	1666.97	26.89
	5-11-88	29.86	1666.24	27.62
	9-12-88	30.35	1665.75	28.11
	1-4-89	29.66	1666.44	27.42
56	10-16-86	42.52	1653.90	39.96
	11-21-86	39.93	1656.49	37.37
	1-13-87	39.96	1656.46	37.40
	3-6-87	39.83	1656.59	37.27
	4-21-87	39.40	1657.02	36.84
	6-3-87	39.54	1656.88	36.98
	5-11-88	41.08	1655.34	38.52
	9-12-88	42.06	1654.36	39.50
	1-4-89	42.88	1653.54	40.32

HESKETT SWL INFORMATION

WELL NO.	DATE	SWL-TOP	SWL-MSL	SWL-BLS
60	9-11-86	32.58	1683.84	30.39
	10-16-86	32.51	1683.91	30.32
	11-21-86	32.35	1684.07	30.16
	1-13-87	32.35	1684.07	30.16
	3-6-87	32.51	1683.91	30.32
	4-21-87	32.29	1684.13	30.10
	6-3-87	32.25	1684.17	30.06
	5-11-88	34.61	1681.81	32.42
	9-12-88	35.47	1680.95	33.28
	1-4-89	35.92	1680.50	33.73
	61	10-16-86	32.55	1683.98
11-21-86		32.38	1684.15	30.08
1-13-87		32.38	1684.15	30.08
3-6-87		32.55	1683.98	30.25
4-21-87		32.32	1684.21	30.02
6-3-87		32.32	1684.21	30.02
5-11-88		34.65	1681.88	32.35
9-12-88		35.47	1681.06	33.17
1-4-89		35.96	1680.57	33.66
62		10-16-86	32.74	1683.93
	11-21-86	32.55	1684.12	30.20
	1-13-87	32.51	1684.16	30.16
	3-6-87	32.71	1683.96	30.36
	4-21-87	32.48	1684.19	30.13
	6-3-87	32.48	1684.19	30.13
	5-11-88	34.81	1681.86	32.46
	9-12-88	dry		
	1-4-89	dry		
	70	9-11-86	55.02	1680.65
10-16-86		54.99	1680.68	52.50
11-21-86		54.56	1681.11	52.07
1-13-87		54.46	1681.21	51.97
3-6-87		54.40	1681.27	51.91
4-21-87		54.53	1681.14	52.04
6-3-87		54.43	1681.24	51.94
5-11-88		54.56	1681.11	52.07
9-12-88		54.82	1680.85	52.33
1-4-89		54.92	1680.75	52.43

HESKETT SWL INFORMATION

WELL NO.	DATE	SWL-TOP	SWL-MSL	SWL-BLS
WS1	9-4-86	25.00	1656.71	22.90
	10-16-86	25.13	1656.58	23.03
	11-21-86	25.56	1656.15	23.46
	1-13-87*	28.15	1655.52	24.09
	3-6-87	26.77	1656.90	22.71
	4-21-87	24.97	1658.70	20.91
	6-3-87	25.36	1658.31	21.30
	5-11-88	29.00	1654.67	24.94
	9-12-88	30.32	1653.35	26.26
	1-4-89	29.86	1653.81	25.80
	* = WELL CASING REPAIRED			
WS1A	9-4-86	dry		
	10-16-86	dry		
	11-21-86	dry		
	1-13-87	dry		
	3-6-87	24.31	1657.92	21.18
	4-21-87	22.18	1660.05	19.05
	6-3-87	22.38	1659.85	19.25
	5-11-88	dry		
	9-12-88	dry		
1-4-89	dry			
WS1B	9-4-86	25.33	1656.74	22.06
	10-16-86	25.53	1656.54	22.26
	11-21-86	26.08	1655.99	22.81
	1-13-87	27.07	1655.00	23.80
	3-6-87	24.35	1657.72	21.08
	4-21-87	21.82	1660.25	18.55
	6-3-87	22.77	1659.30	19.50
	5-11-88	28.22	1653.85	24.95
	9-12-88	30.18	1651.89	26.91
	1-4-89	29.92	1652.15	26.65
WS2	9-4-86	33.96	1664.68	31.32
	10-16-86	33.66	1664.98	31.02
	11-21-86	33.47	1665.17	30.83
	1-13-87	33.79	1664.85	31.15
	3-6-87	33.73	1664.91	31.09
	4-21-87	32.91	1665.73	30.27
	6-3-87	33.04	1665.60	30.40
	5-11-88	35.33	1663.31	32.69
	9-12-88	36.68	1661.96	34.04
	1-4-89	37.17	1661.47	34.53

HESKETT SWL INFORMATION

WELL NO.	DATE	SWL-TOP	SWL-MSL	SWL-BLS
WS3	9-4-86	14.67	1646.33	11.67
	10-16-86	14.44	1646.56	11.44
	11-21-86	14.40	1646.60	11.40
	1-13-87	13.98	1647.02	10.98
	3-6-87	14.80	1646.20	11.80
	4-21-87	13.94	1647.06	10.94
	6-3-87	14.60	1646.40	11.60
	5-11-88	17.52	1643.48	14.52
	9-12-88	17.88	1643.12	14.88
	1-4-89	17.68	1643.32	14.68
WS3A	10-16-86	8.30	1652.51	5.19
	11-21-86	8.43	1652.38	5.32
	1-13-87	9.55	1651.26	6.44
	3-6-87	10.17	1650.64	7.06
	4-21-87	6.82	1653.99	3.71
	6-3-87	8.73	1652.08	5.62
	5-11-88	13.71	1647.10	10.60
	9-12-88	13.81	1647.00	10.70
	1-4-89	14.73	1646.08	11.62
	WS4	9-4-86	19.62	1642.99
10-16-86		19.52	1643.09	16.52
11-21-86		19.42	1643.19	16.42
1-13-87		18.83	1643.78	15.83
3-6-87		19.16	1643.45	16.16
4-21-87		19.00	1643.61	16.00
6-3-87		19.39	1643.22	16.39
5-11-88		21.46	1641.15	18.46
9-12-88		21.95	1640.66	18.95
1-4-89		21.23	1641.38	18.23
WS4A	9-4-86	17.29	1645.20	14.29
	10-16-86	17.16	1645.33	14.16
	11-21-86	17.13	1645.36	14.13
	1-13-87	17.39	1645.10	14.39
	3-6-87	17.62	1644.87	14.62
	4-21-87	15.81	1646.68	12.81
	6-3-87	16.93	1645.56	13.93
	5-11-88	19.36	1643.13	16.36
	9-12-88	20.11	1642.38	17.11
	1-4-89	19.75	1642.74	16.75
WS4B	9-4-86	17.39	1645.36	14.39
	10-16-86	17.23	1645.52	14.23
	11-21-86	17.16	1645.59	14.16
	1-13-87	17.42	1645.33	14.42
	3-6-87	17.65	1645.10	14.65
	4-21-87	15.81	1646.94	12.81
	6-3-87	17.06	1645.69	14.06
	5-11-88	19.55	1643.20	16.55
	9-12-88	20.28	1642.47	17.28
	1-4-89	19.92	1642.83	16.92

EXHIBIT 5-H

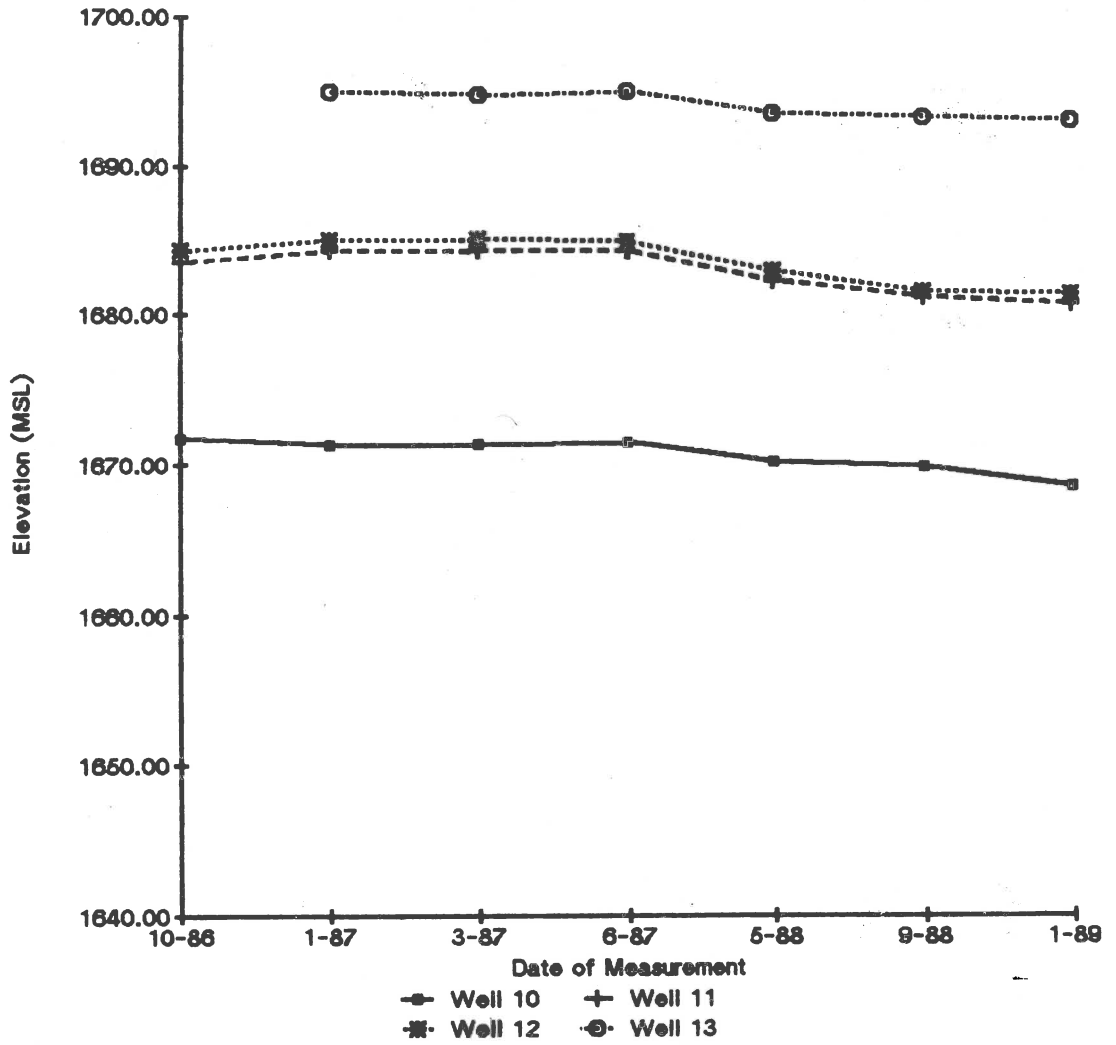
WATER TABLE ELEVATION CONTOUR MAP

EXHIBIT 5-I

SITE HYDROGRAPHS

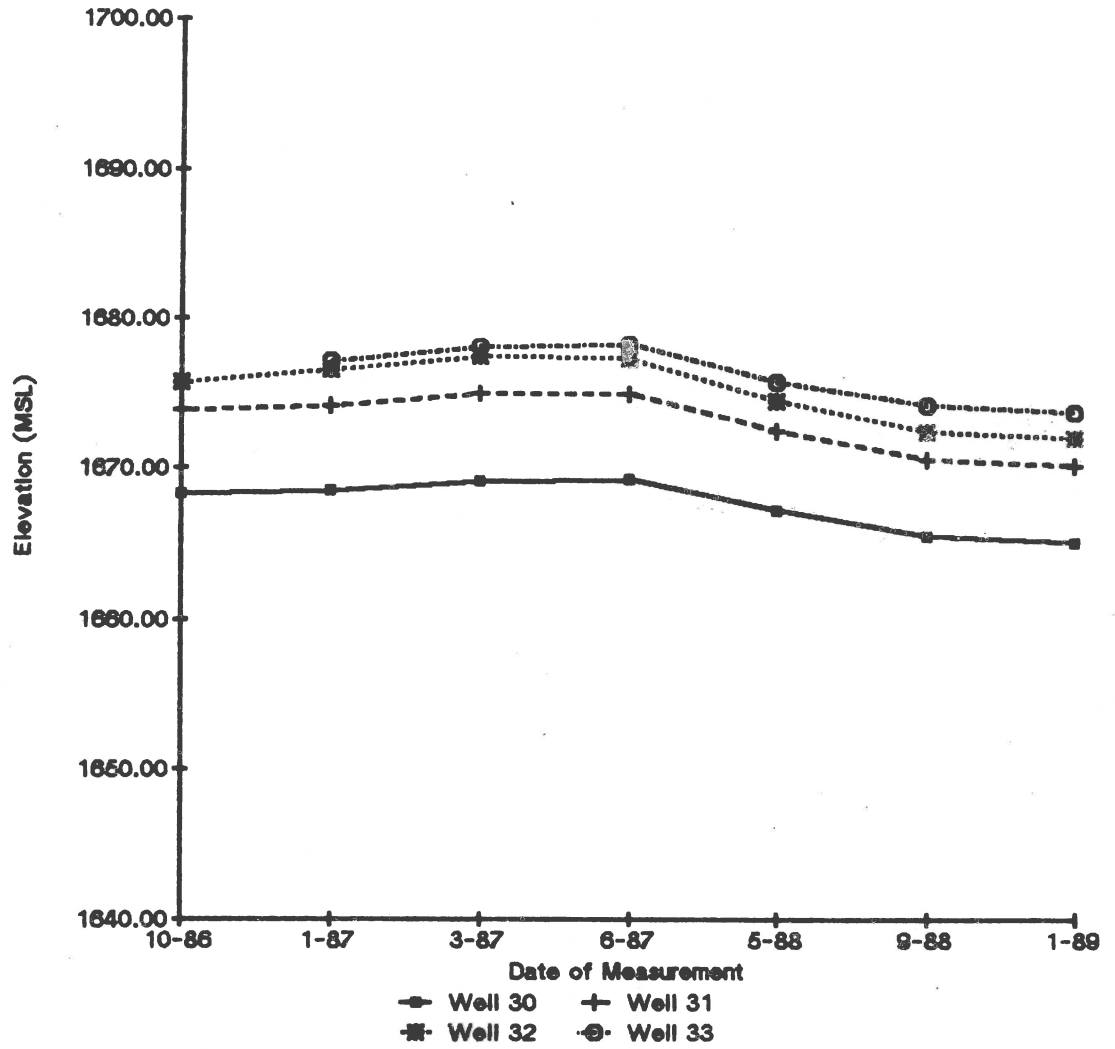
HYDROGRAPH

Wells 10, 11, 12, 13



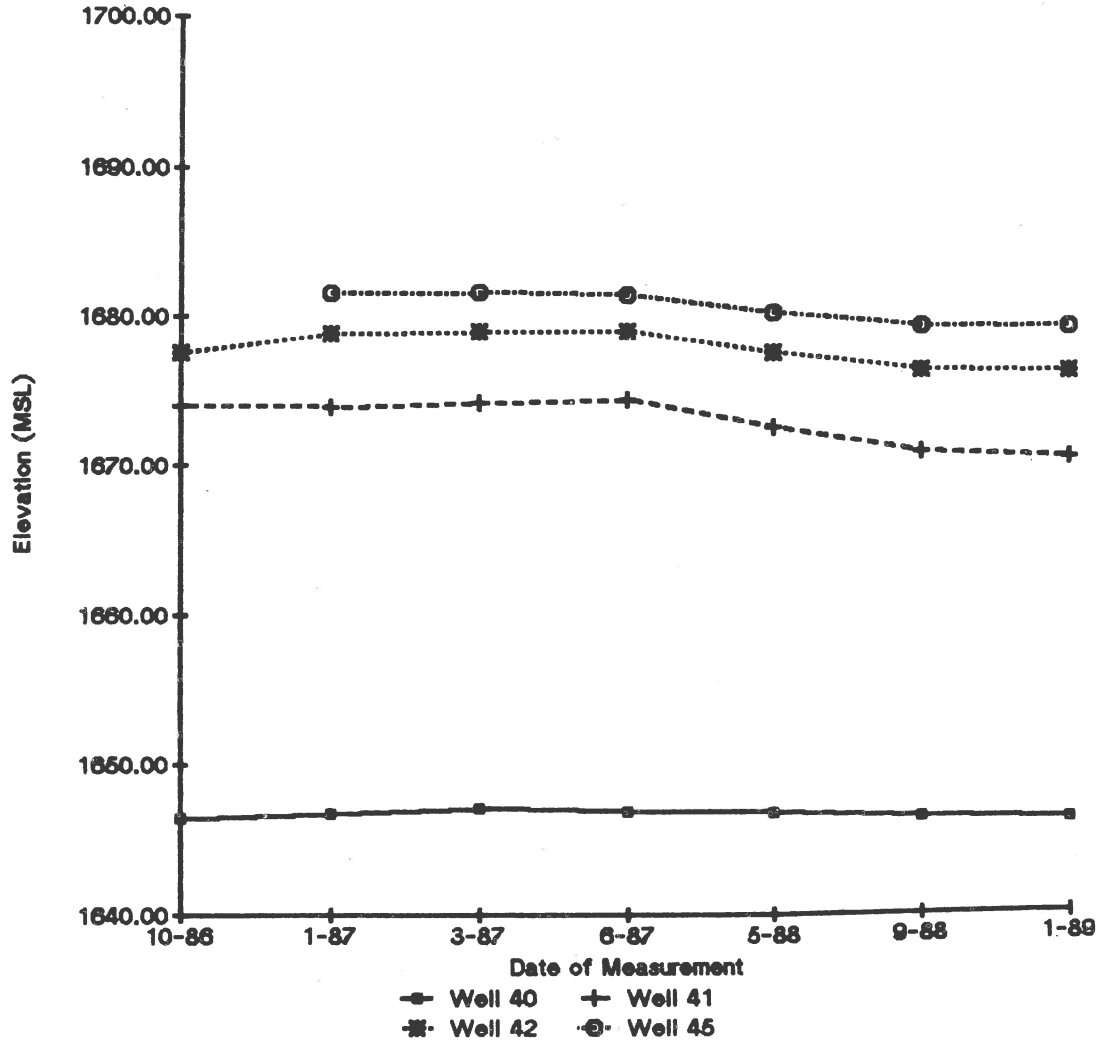
HYDROGRAPH

Wells 30, 31, 32, 33



HYDROGRAPH

Wells 40, 41, 42, 45



HYDROGRAPH

Wells 50, 51, 52

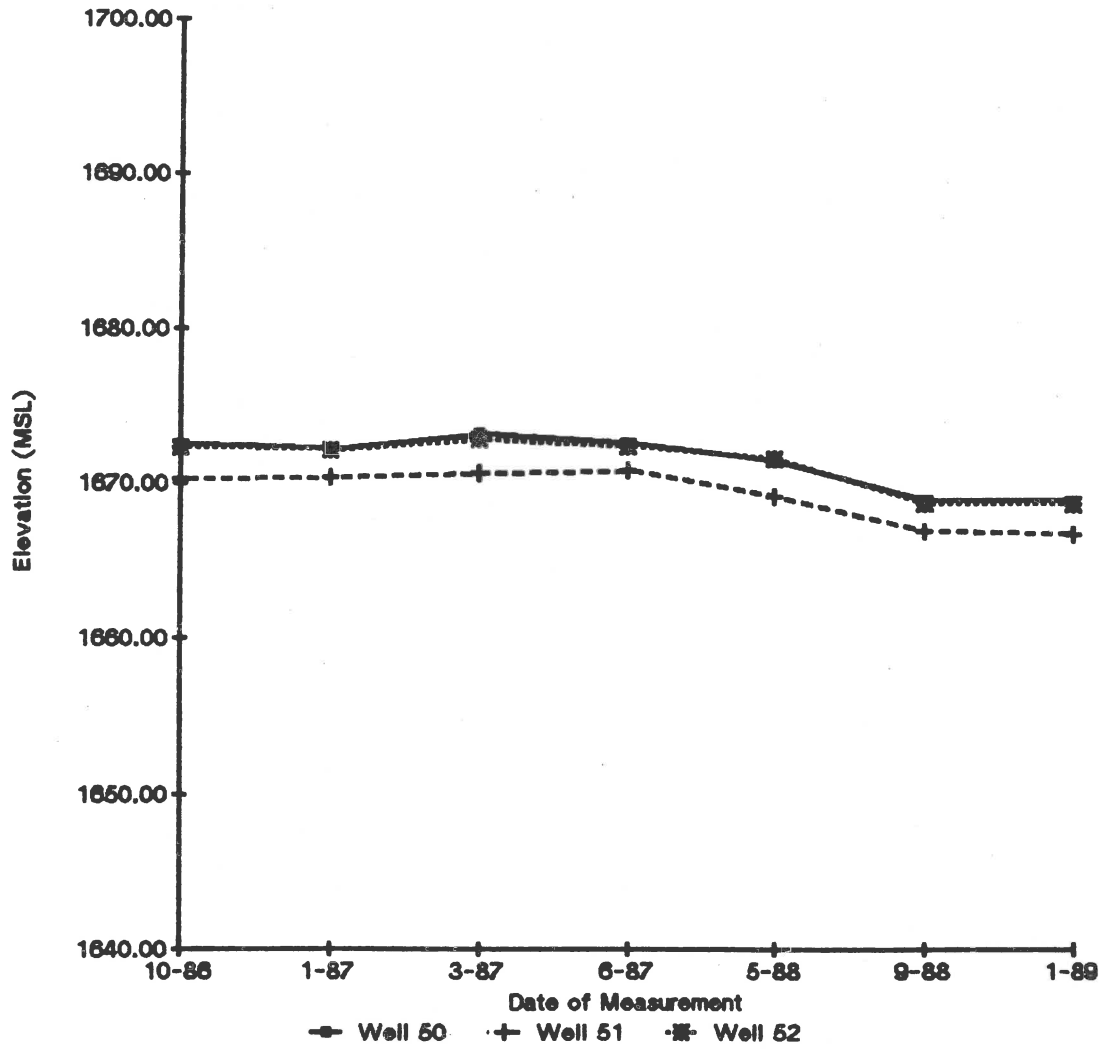


EXHIBIT 5-J

GROUNDWATER CHEMICAL ANALYSIS

Drinking Water Standards

Constituent	Recommended Concentration Limit ¹	
Total Dissolved Solids	(mg/L)	500
Sulfate (SO ₄)	(mg/L)	250
Chloride (Cl)	(mg/L)	250
Nitrate (NO ₃)	(mg/L)	45
Iron (Fe)	(mg/L)	0.3
Manganese (Mn)	(mg/L)	0.05
Copper (Cu)	(mg/L)	1.0
Zinc (Zn)	(mg/L)	5.0
Boron (B)	(mg/L)	1.0
Hydrogen Sulfide (H ₂ S)	(mg/L)	0.05
	Maximum Permissible Concentration ²	
Arsenic (As)	(mg/L)	0.05
Antimony (Sb)	(mg/L)	0.01
Barium (Ba)	(mg/L)	1.0
Cadmium (Cd)	(mg/L)	0.01
Chromium (Cr)	(mg/L)	0.05
Lead (Pb)	(mg/L)	0.050
Mercury (Hg)	(mg/L)	0.002
Selenium (Se)	(mg/L)	0.01
Silver (Ag)	(mg/L)	0.050
Fluoride (F)	(mg/L)	1.4-2.41 ³
Organics:		
Cyanide	(mg/L)	0.05
Phenol	(mg/L)	0.001
Synthetic Detergents	(mg/L)	0.5

¹Recommended concentration limits for these constituents are mainly to provide esthetic and taste characteristics.

²Maximum permissible limits are set according to health criteria.

³Limit depends on average air temperature of the region; fluoride is toxic at about 5-10 mg/L if water is consumed over a long period of time.

Chemical Analyses of Selected Wells

Parameter	Well 10	Well 12	Well 30
Sample Collection Date	9-11-86	9-11-86	9-11-86
Water Level ¹ (ft)	51.6	42.4	49.4
Elevation; Screen Center (ft)	1606.0	1653.5	1597.6
Field Water Temp (°C)	8.0	8.4	8.0
Field pH (standard units)	7.6	7.2	8.1
Field Sp.Cond. (µmhos/cm)	7370.0	8070.0	1350.0
Total Dissolved Solids ² (mg/L)	9736.0	10396.0	1286.0
Total Alkalinity as CaCO ₃ (mg/L)	674.0	645.0	425.0
Bicarbonate (HCO ₃) (mg/L)	825.0	789.0	520.0
Boron (B) (mg/L)			
Calcium (Ca) (mg/L)	339.0	422.0	33.0
Chloride (Cl) (mg/L)	20.8	20.7	2.1
Fluoride (F) (mg/L)	0.3	<.2	0.4
Iron (Fe) (mg/L)	<.2	0.6	<.2
Potassium (K) (mg/L)	16.0	13.0	5.8
Magnesium (Mg) (mg/L)	302.0	318.0	34.0
Nitrate (NO ₃) (mg/L)	<1	<1	<1
Sodium (Na) ³ (mg/L)	2232.0	2438.0	352.0
Sulfate (SO ₄) (mg/L)	6443.0	6818.0	606.0

TRACE ELEMENTS:

Arsenic (Ar) (mg/L)	<.002	.0025	<.002
Barium (Ba) (mg/L)	0.090	0.157	0.030
Cadmium (Cd) (mg/L)	0.0020	0.0012	<.001
Chromium (Cr) (mg/L)	<.002	<.002	<.002
Lead (Pb) (mg/L)	<.002	<.002	<.002
Manganese (Mn) (mg/L)	0.986	2.130	0.124
Mercury (Hg) (mg/L)	<.0003	<.0003	<.0003
Molybdenum (Mo) (mg/L)	0.018	<.010	<.010
Selenium (Se) (mg/L)	<.002	<.002	<.002
Silver (Ag) (mg/L)	<.001	<.001	<.001

¹From top of PCV casing.

²TDS is calculated.

Chemical Analyses of Selected Wells

Parameter		Well 32	Well 40	Well 42
Sample Collection Date		9-11-86	9-11-86	9-11-86
Water Level ¹	(ft)	42.5	63.8	33.3
Elevation; Screen Center	(ft)	1651.7	1594.3	1662.6
Field Water Temp	(°C)	8.3	8.6	8.5
Field pH	(standard units)	6.9	7.5	7.0
Field Sp.Cond.	(umhos/cm)	3150.0	4290.0	3700.0
Total Dissolved Solids ²	(mg/L)	3927.0	5333.0	4658.0
Total Alkalinity as CaCO ₃	(mg/L)	467.0	565.0	424.0
Bicarbonate (HCO ₃)	(mg/L)	571.0	691.0	519.0
Boron (B)	(mg/L)			
Calcium (Ca)	(mg/L)	313.0	422.0	432.0
Chloride (Cl)	(mg/L)	10.0	15.2	46.8
Fluoride (F)	(mg/L)	0.3	0.2	0.3
Iron (Fe)	(mg/L)	<.2	<.2	0.3
Potassium (K)	(mg/L)	14.0	12.0	15.0
Magnesium (Mg)	(mg/L)	318.0	136.0	250.0
Nitrate (NO ₃)	(mg/L)	<1	<1	4.3
Sodium (Na) ³	(mg/L)	464.0	1047.0	648.0
Sulfate (SO ₄)	(mg/L)	2538.0	3378.0	3058.0
TRACE ELEMENTS:				
Arsenic (Ar)	(mg/L)	<.002	<.002	<.002
Barium (Ba)	(mg/L)	0.093	0.083	0.198
Cadmium (Cd)	(mg/L)	<.001	<.001	<.001
Chromium (Cr)	(mg/L)	<.002	<.002	<.002
Lead (Pb)	(mg/L)	<.002	<.002	<.002
Manganese (Mn)	(mg/L)	0.462	0.037	0.670
Mercury (Hg)	(mg/L)	<.0003	<.0003	<.0003
Molybdenum (Mo)	(mg/L)	0.014	<.010	<.010
Selenium (Se)	(mg/L)	<.002	0.005	0.032
Silver (Ag)	(mg/L)	<.001	<.001	<.001

¹From top of PCV casing.

²TDS is calculated.

Chemical Analyses of Selected Wells

Parameter	Well 44	Well 50	Well 50
Sample Collection Date	11-21-86	9-11-86	11-21-86
Water Level ¹ (ft)	21.85	5.5	4.17
Elevation; Screen Center (ft)	1687.9	1657.5	1657.5
Field Water Temp (°C)	6.5	9.7	8.5
Field pH (standard units)	6.76	7.5	7.37
Field Sp. Cond. (umhos/cm)	7580.0	4310.0	3620.0
Total Dissolved Solids ² (mg/L)	11240.0	4999.0	5196.0
Total Alkalinity as CaCO ₃ (mg/L)	401.0	418.0	416.0
Bicarbonate (HCO ₃) (mg/L)	491.0	511.0	509.2
Boron (B) (mg/L)			
Calcium (Ca) (mg/L)	648.0	313.0	391.0
Chloride (Cl) (mg/L)	558.0	34.8	33.0
Fluoride (F) (mg/L)	0.5	0.3	<0.2
Iron (Fe) (mg/L)	<0.2	<.2	<0.2
Potassium (K) (mg/L)	51.0	12.0	13.0
Magnesium (Mg) (mg/L)	1322.0	250.0	257.0
Nitrate (NO ₃) (mg/L)	30.0	23.5	112.0
Sodium (Na) (mg/L)	1589.0	871.0	902.0
Sulfate (SO ₄) (mg/L)	7390.0	3302.0	3384.0

TRACE ELEMENTS:

Arsenic (Ar) (mg/L)	<.002	<.002	<.002
Barium (Ba) (mg/L)	0.156	0.084	0.128
Cadmium (Cd) (mg/L)	<.001	<.001	<.001
Chromium (Cr) (mg/L)	<0.001	<.002	0.003
Lead (Pb) (mg/L)	<.005	<.002	<.005
Manganese (Mn) (mg/L)	0.218	0.010	0.005
Mercury (Hg) (mg/L)	<.0003	<.0003	<.0003
Molybdenum (Mo) (mg/L)	<.010	<.010	<.010
Selenium (Se) (mg/L)	0.086	0.055	0.076
Silver (Ag) (mg/L)	<.002	<.001	<.002
Phenol (mg/L)	<1.0	<1.0	<1.0
Oil & Grease (mg/L)	<3.0	<3.0	<3.0

¹From top of PCV casing.

²TDS is calculated.

Chemical Analyses of Selected Wells

Parameter	Well 52	Well 54	Well 55
Sample Collection Date	11-21-86	11-21-86	11-21-86
Water Level ¹	(ft) 4.07	20.97	29.50
Elevation; Screen Center	(ft) 1663.0	1635.1	1648.9
Field Water Temp	(oC) 8.7	6.9	7.5
Field pH (standard units)	7.38	8.03	6.81
Field Sp.Cond.	(umhos/cm) 4650.0	4570.0	9007.0
Total Dissolved Solids ²	(mg/L) 6072.0	7223.0	13081.0
Total Alkalinity as CaCO ₃	(mg/L) 424.0	616.0	528.0
Bicarbonate (HCO ₃)	(mg/L) 519.0	754.0	646.3
Boron (B)	(mg/L)		
Calcium (Ca)	(mg/L) 392.0	295.0	445.0
Chloride (Cl)	(mg/L) 45.0	92.0	81.0
Fluoride (F)	(mg/L) <0.2	0.3	0.7
Iron (Fe)	(mg/L) <0.2	<0.2	<0.2
Potassium (K)	(mg/L) 15.0	13.0	28.0
Magnesium (Mg)	(mg/L) 305.0	439.0	862.0
Nitrate (NO ₃)	(mg/L) 148.0	6.0	154.0
Sodium (Na)	(mg/L) 1115.0	1490.0	2423.0
Sulfate (SO ₄)	(mg/L) 3991.0	4617.0	9007.0

TRACE ELEMENTS:

Arsenic (Ar)	(mg/L) <.002	<.002	<.002
Barium (Ba)	(mg/L) 0.125	0.105	0.133
Cadmium (Cd)	(mg/L) <.001	<.001	<.001
Chromium (Cr)	(mg/L) 0.003	0.003	0.003
Lead (Pb)	(mg/L) <.005	<.005	<.005
Manganese (Mn)	(mg/L) 0.004	1.080	0.045
Mercury (Hg)	(mg/L) <.0003	<.0003	<.0003
Molybdenum (Mo)	(mg/L) <.010	0.041	<.010
Selenium (Se)	(mg/L) 0.088	0.025	0.386
Silver (Ag)	(mg/L) <.002	<.002	<.002
Phenol	(mg/L)	<1.0	
Oil & Grease	(mg/L)	<3.0	

¹From top of PCV casing.

²TDS is calculated.

Chemical Analyses of Selected Wells

Parameter	Well 60	Well 70
Sample Collection Date	11-21-86	9-11-86
Water Level ¹	(ft) 32.35	55.0
Elevation; Screen Center	(ft) 1677.0	1636.4
Field Water Temp	(°C) 7.6	8.6
Field pH (standard units)	6.83	8.3
Field Sp. Cond.	(umhos/cm) 10440.0	10370.0
Total Dissolved Solids ²	(mg/L) 14917.0	13129.0
Total Alkalinity as CaCO ₃	(mg/L) 540.0	491.0
Bicarbonate (HCO ₃)	(mg/L) 661.0	600.0
Boron (B)	(mg/L)	
Calcium (Ca)	(mg/L) 417.0	192.0
Chloride (Cl)	(mg/L) 208.0	10.9
Fluoride (F)	(mg/L) 0.5	0.3
Iron (Fe)	(mg/L) <0.2	<.2
Potassium (K)	(mg/L) 41.0	22.0
Magnesium (Mg)	(mg/L) 1355.0	121.0
Nitrate (NO ₃)	(mg/L) 170.0	<1
Sodium (Na)	(mg/L) 1148.0	3682.0
Sulfate (SO ₄)	(mg/L) 11632.0	8818.0

TRACE ELEMENTS:

Arsenic (Ar)	(mg/L) <.002	.0032
Barium (Ba)	(mg/L) 0.151	0.080
Cadmium (Cd)	(mg/L) <.001	0.0010
Chromium (Cr)	(mg/L) 0.004	<.002
Lead (Pb)	(mg/L) <.005	<.002
Manganese (Mn)	(mg/L) 0.033	0.110
Mercury (Hg)	(mg/L) <.0003	<.0003
Molybdenum (Mo)	(mg/L) <.010	0.017
Selenium (Se)	(mg/L) 0.195	<.002
Silver (Ag)	(mg/L) <.002	<.001
Phenol	(mg/L) <1.0	
Oil & Grease	(mg/L) <3.0	

¹From top of PCV casing.

²TDS is calculated.

GENERAL INFORMATION

Sample Location/I.D. 52 60 33 70
 Casing Diameter 2" PVC 2" PVC 2" PVC 2" PVC
 Total Well Depth 17' ? 48' ? 38' ? 40' ?
 Past Static Water Level 7.7' 35.8' 36.8' 31.9'
 Approximate Volume of Water 1.5 gal 2 gal .25 gal 1.5 gal 7.5 gal

STATIC LEVEL MEASUREMENT

Date 12/19/88 12/19/88 12/19/88 12/19/88 12/19/88
 Time 14:20 14:45 15:00 15:25 16:35
 Datum PVC Top PVC Top PVC Top PVC Top PVC Top
 Measurement Equipment SteelTape SteelTape SteelTape SteelTape SteelTape
 Static Water Level 30.60 7.65 35.80 36.80 31.92 54.85

PRE-SAMPLING PREPARATION

Pre-Sample Technique/Equip. PVCbailer PVCbailer PVCbailer PVCbailer PVCbailer
 Volume Removed 1.5 gal 1 gal 2 gal .5 gal 1.5 gal 6 gal
 (dirty) (dirty)

SAMPLING

Date 12/20/88 12/20/88 12/20/88 12/20/88 12/21/88 12/21/88
 Time 10:15 10:45 11:25 12:00 15:50 16:22
 Measurement Equipment SteelTape SteelTape SteelTape SteelTape SteelTape SteelTape
 Static Water Level 31.05 7.95 35.86 36.92 31.85 54.90
 Sampling Technique/Equip. PVCbailer PVCbailer PVCbailer PVCbailer PVCbailer PVCbailer
 Field Temperature (C) 6 5 5 4 7 6
 Field pH 5.60 5.80 5.50 5.60 5.90 6.40
 Field Conductivity 3800 7200 1400 5900 1190 1380

Samples Collected
 Raw-Unfiltered 2 liters 2 liters 2 liters 2 liters 2 liters 2 liters
 Unfiltered/Sulfuric Acid 2 125ml 2 125ml 2 125ml 2 125ml 2 125ml 2 125ml
 Filtered/Nitric Acid 1 125ml 1 125ml 1 125ml 1 125ml 1 125ml 1 125ml
 Other (unfiltered/untreat) 1 125ml 1 125ml 1 125ml 1 125ml 1 125ml 1 125ml

DELIVERY

Date 12/20/88 - 12/22/88
 Time 4:30 - 10:30
 Delivered To Minnesota Valley Testing Laboratories, Inc.
 Via Hand Delivered
 Delivery Container Cooler with Ice

COMMENTS

* Well 33 had insufficient water for any samples - field parameters taken
 Well 45 - samples were dirty



PHONE (701) 258-9720

MINNESOTA VALLEY TESTING LABORATORIES, Inc.

1411 SOUTH 12TH STREET • P.O. BOX 1873
BISMARCK, NORTH DAKOTA 58502-1873



WATER ANALYSIS REPORT

Montana-Dakota Utilities
400 North Fourth
Bismarck, ND 58501

Date: January 27, 1989

W.O. #: 82-045

Attention: John Verwey

Lab. #: M- 156

Sample MDU - Heskett
Identification: #13 15:50 CST
12/20/88

P.O. #: M04548

Date Received: 12/22/88

PHYSICAL PARAMETERS:

Color units of apparent color	_____
Conductivity micromhos/cm @ 25°C	<u>12078</u>
pH	<u>7.2</u>
Solids (Total) mg/l	_____
Solids (Total Dissolved) mg/l	<u>11967</u>
Solids (Total Suspended) mg/l	_____
Solids (Total Volatile) mg/l	_____
Turbidity — NTU	_____
COMMON IONS:	
Calcium mg/l	<u>366.0</u>
Magnesium mg/l	<u>642.0</u>
Sodium mg/l	<u>1965.0</u>
Potassium mg/l	<u>27.0</u>
Acidity as CaCO ₃ mg/l	_____
Alkalinity (Total) as CaCO ₃ mg/l	<u>600</u>
Bicarbonate as CaCO ₃ mg/l	<u>600</u>
Bicarbonate as HCO ₃ mg/l	_____
Carbonate as CaCO ₃ mg/l	<u>0</u>
P-Alkalinity as CaCO ₃ mg/l	_____
Sulfate mg/l	<u>6774.9</u>
Chloride mg/l	<u>327.6</u>
Total Hardness as CaCO ₃ mg/l	<u>3556</u>
Sodium Adsorption Ratio	<u>14.37</u>
Cations	<u>157.9</u>
Anions	<u>164.2</u>
% Error	<u>2.0</u>

NUTRIENTS:

Ammonia-Nitrogen mg/l	_____
Nitrite-Nitrogen as N mg/l	_____
Nitrate-Nitrogen as N mg/l	<u>25.8</u>
Organic-Nitrogen mg/l	_____
Total - Kjeldahl Nitrogen mg/l	_____
Ortho-phosphate as P mg/l	_____
Phosphorus (Total) as P mg/l	_____
Phosphorus (Dissolved) as P mg/l	_____

METALS:

Copper (Total) mg/l	_____
Iron (Total) mg/l	_____
Manganese (Total) mg/l	_____

MISCELLANEOUS:

ADA g/l	_____
Biochemical Oxygen Demand mg/l	_____
Chemical Oxygen Demand mg/l	_____
Cyanide mg/l	_____
Fecal Coliform Count — Millipore filter/100 ml	_____
Fluoride mg/l	<u>0.62</u>
Iron Bacteria	_____
Oil & Grease mg/l	_____
Phenols mg/l	_____
Total Organic Carbon mg/l	_____
Total Plate Count per 100ml	_____

TRACE ELEMENTS:

Aluminum mg/l	_____	Cobalt mg/l	_____	Silver mg/l	<u>0.034</u>
Antimony mg/l	_____	Copper mg/l	_____	Strontium mg/l	_____
Arsenic mg/l	<u>0.007</u>	Iron mg/l	<u>0.11</u>	Thallium mg/l	_____
Barium mg/l	<u><0.100</u>	Lead mg/l	<u><0.001</u>	Thorium mg/l	_____
Beryllium mg/l	_____	Manganese mg/l	<u><0.05</u>	Tin mg/l	_____
Boron mg/l	<u>1.500</u>	Mercury mg/l	<u>0.0011</u>	Titanium mg/l	_____
Bromide mg/l	_____	Molybdenum mg/l	<u><0.100</u>	Vanadium mg/l	_____
Cadmium mg/l	<u><0.001</u>	Nickel mg/l	_____	Zinc mg/l	_____
Chromium mg/l	<u><0.050</u>	Selenium mg/l	<u><0.002</u>		

***** Metals are reported as dissolved, unless otherwise indicated. *****

FIELD DATA:

Flow	-	T ° C	<u>7.0°C</u>
E. C.	<u>1190</u>	pH	<u>5.90</u>
Static Water Level			<u>31.85</u>

Catherine A. Phelps, Chemist



PHONE (701) 258-9720

MINNESOTA VALLEY TESTING LABORATORIES, Inc.



1411 SOUTH 12TH STREET • P.O. BOX 1873
BISMARCK, NORTH DAKOTA 58502-1873

WATER ANALYSIS REPORT

Montana-Dakota Utilities
400 North Fourth
Bismarck, ND 58501

Date: January 24, 1989

W.O. #: 82-041

Attention: John Verwey

Lab. #: M-145

Sample Identification: MDU - Heskett
#45 10:15 CST
12-20-88

P.O. #: M04548

Date Received: 12-21-88

PHYSICAL PARAMETERS:

Color	units of apparent color	_____
Conductivity	micromhos/cm @ 25°C	<u>3937</u>
pH		<u>7.5</u>
Solids (Total)	mg/l	_____
Solids (Total Dissolved)	mg/l	<u>3611</u>
Solids (Total Suspended)	mg/l	_____
Solids (Total Volatile)	mg/l	_____
Turbidity - NTU		_____

COMMON IONS:

Calcium	mg/l	<u>465.0</u>
Magnesium	mg/l	<u>171.0</u>
Sodium	mg/l	<u>247.0</u>
Potassium	mg/l	<u>11.7</u>
Acidity as CaCO ₃	mg/l	_____
Alkalinity (Total) as CaCO ₃	mg/l	<u>340</u>
Bicarbonate as CaCO ₃	mg/l	<u>340</u>
Bicarbonate as HCO ₃	mg/l	_____
Carbonate as CaCO ₃	mg/l	<u>0</u>
P-Alkalinity as CaCO ₃	mg/l	_____
Sulfate	mg/l	<u>1840.0</u>
Chloride	mg/l	<u>124.1</u>
Total Hardness as CaCO ₃	mg/l	<u>1865</u>
Sodium Adsorption Ratio		<u>2.50</u>
Cations		<u>48.5</u>
Anions		<u>49.0</u>
% Error		<u>0.5</u>

TRACE ELEMENTS:

Aluminum	mg/l	_____	Cobalt	mg/l	_____	Silver	mg/l	<u>0.019</u>
Antimony	mg/l	_____	Copper	mg/l	_____	Strontium	mg/l	_____
Arsenic	mg/l	<u>0.005</u>	Iron	mg/l	<u><0.10</u>	Thallium	mg/l	_____
Barium	mg/l	<u><0.10</u>	Lead	mg/l	<u><0.001</u>	Thorium	mg/l	_____
Beryllium	mg/l	_____	Manganese	mg/l	<u><0.05</u>	Tin	mg/l	_____
Boron	mg/l	<u>1.000</u>	Mercury	mg/l	<u>0.0008</u>	Titanium	mg/l	_____
Bromide	mg/l	_____	Molybdenum	mg/l	<u><0.10</u>	Vanadium	mg/l	_____
Cadmium	mg/l	<u><0.001*</u>	Nickel	mg/l	_____	Zinc	mg/l	_____
Chromium	mg/l	<u><0.05</u>	Selenium	mg/l	<u><0.002</u>			

***** Metals are reported as dissolved, unless otherwise indicated. ***** *CEP

FIELD DATA:

Flow	-	T ° C	<u>6.0° C</u>
E. C.	<u>3800</u>	pH	<u>5.6</u>
Static Water Level			<u>31.05</u>

*Analysis completed by Controls for Environmental Pollution; Santa Fe, New Mexico

Catherine Anne Phelps

Catherine A. Phelps, Chemist



PHONE (701) 258-9720

MINNESOTA VALLEY TESTING LABORATORIES, Inc.

1411 SOUTH 12TH STREET • P.O. BOX 1873
BISMARCK, NORTH DAKOTA 58502-1873



WATER ANALYSIS REPORT

Montana-Dakota Utilities
400 North Fourth
Bismarck, ND 58501

Date: January 24, 1989

W.O. #: 82-041

Attention: John Verwey

Lab. #: M-146

Sample MDU - Heskett
Identification: #52 10:45 CST
12-20-88

P.O. #: M04548

Date Received: 12-21-88

PHYSICAL PARAMETERS:

Color	units of apparent color	_____
Conductivity	micromhos/cm @ 25°C	7300
pH		7.6
Solids (Total)	mg/l	_____
Solids (Total Dissolved)	mg/l	6724
Solids (Total Suspended)	mg/l	_____
Solids (Total Volatile)	mg/l	_____
Turbidity — NTU		_____
COMMON IONS:		
Calcium	mg/l	421.0
Magnesium	mg/l	285.0
Sodium	mg/l	1060.0
Potassium	mg/l	14.3
Acidity as CaCO ₃	mg/l	_____
Alkalinity (Total) as CaCO ₃	mg/l	438
Bicarbonate as CaCO ₃	mg/l	438
Bicarbonate as HCO ₃	mg/l	_____
Carbonate as CaCO ₃	mg/l	0
P-Alkalinity as CaCO ₃	mg/l	_____
Sulfate	mg/l	3535.6
Chloride	mg/l	99.3
Total Hardness as CaCO ₃	mg/l	2224
Sodium Adsorption Ratio		9.80
Cations		91.3
Anions		87.2
% Error		2.3

NUTRIENTS:

Ammonia-Nitrogen	mg/l	_____
Nitrite-Nitrogen as N	mg/l	_____
Nitrate-Nitrogen as N	mg/l	27.8
Organic-Nitrogen	mg/l	_____
Total - Kjeldahl Nitrogen	mg/l	_____
Ortho-phosphate as P	mg/l	_____
Phosphorus (Total) as P	mg/l	_____
Phosphorus (Dissolved) as P	mg/l	_____

METALS:

Copper (Total)	mg/l	_____
Iron (Total)	mg/l	_____
Manganese (Total)	mg/l	_____

MISCELLANEOUS:

ADA	g/l	_____
Biochemical Oxygen Demand	mg/l	_____
Chemical Oxygen Demand	mg/l	_____
Cyanide	mg/l	_____
Fecal Coliform Count — Millipore	filter/100 ml	_____
Fluoride	mg/l	0.29
Iron Bacteria		_____
Oil & Grease	mg/l	_____
Phenols	mg/l	_____
Total Organic Carbon	mg/l	_____
Total Plate Count per 100ml		_____

TRACE ELEMENTS:

Aluminum	mg/l	_____	Cobalt	mg/l	_____	Silver	mg/l	0.02
Antimony	mg/l	_____	Copper	mg/l	_____	Strontium	mg/l	_____
Arsenic	mg/l	0.004	Iron	mg/l	<0.10	Thallium	mg/l	_____
Barium	mg/l	<0.10	Lead	mg/l	<0.001	Thorium	mg/l	_____
Beryllium	mg/l	_____	Manganese	mg/l	0.06	Tin	mg/l	_____
Boron	mg/l	1.200	Mercury	mg/l	0.001	Titanium	mg/l	_____
Bromide	mg/l	_____	Molybdenum	mg/l	<0.10	Vanadium	mg/l	_____
Cadmium	mg/l	<0.001*	Nickel	mg/l	_____	Zinc	mg/l	_____
Chromium	mg/l	<0.05	Selenium	mg/l	0.005	*CEP		

***** Metals are reported as dissolved, unless otherwise indicated. *****

FIELD DATA:

Flow	_____	T° C	5.0° C
E. C.	7200	pH	5.8
Static Water Level	_____		7.95

*Analysis completed by Controls for Environmental Pollution; Santa Fe, New Mexico

Catherine A. Phelps, Chemist



PHONE (701) 258-9720

MINNESOTA VALLEY TESTING LABORATORIES, Inc.



1411 SOUTH 12TH STREET • P.O. BOX 1873
BISMARCK, NORTH DAKOTA 58502-1873

WATER ANALYSIS REPORT

• Montana-Dakota Utilities
400 North Fourth
Bismarck, ND 58501

Date: January 24, 1989

W.O. #: 82-041

Attention: John Verwey

Lab. #: M- 147

Sample Identification: MDU - Heskett
60 11:25 CST
12-20-88

P.O. #: M04548

Date Received: 12-21-88

PHYSICAL PARAMETERS:

Color	units of apparent color	_____
Conductivity	micromhos/cm @ 25°C	<u>15,166</u>
pH		<u>7.0</u>
Solids (Total)	mg/l	_____
Solids (Total Dissolved)	mg/l	<u>17,634**</u>
Solids (Total Suspended)	mg/l	_____
Solids (Total Volatile)	mg/l	_____
Turbidity — NTU		_____

COMMON IONS:

Calcium	mg/l	<u>415.0</u>
Magnesium	mg/l	<u>1,340.0</u>
Sodium	mg/l	<u>2,245.0</u>
Potassium	mg/l	<u>33.8</u>
Acidity as CaCO ₃	mg/l	_____
Alkalinity (Total) as CaCO ₃	mg/l	<u>524</u>
Bicarbonate as CaCO ₃	mg/l	<u>524</u>
Bicarbonate as HCO ₃	mg/l	_____
Carbonate as CaCO ₃	mg/l	<u>0</u>
P-Alkalinity as CaCO ₃	mg/l	_____
Sulfate	mg/l	<u>10,779.8</u>
Chloride	mg/l	<u>273.0</u>

Total Hardness as CaCO ₃	mg/l	<u>6,552</u>
Sodium Adsorption Ratio		<u>12.09</u>
Cations		<u>230.4</u>
Anions		<u>244.2</u>
% Error		<u>2.9</u>

TRACE ELEMENTS:

Aluminum	mg/l	_____
Antimony	mg/l	_____
Arsenic	mg/l	<u><0.002</u>
Barium	mg/l	<u><0.10</u>
Beryllium	mg/l	_____
Boron	mg/l	<u>1.800</u>
Bromide	mg/l	_____
Cadmium	mg/l	<u><0.001*</u>
Chromium	mg/l	<u><0.05</u>

Cobalt	mg/l	_____
Copper	mg/l	_____
Iron	mg/l	<u>0.20</u>
Lead	mg/l	<u><0.001</u>
Manganese	mg/l	<u>0.08</u>
Mercury	mg/l	<u>0.001</u>
Molybdenum	mg/l	<u><0.10</u>
Nickel	mg/l	_____
Selenium	mg/l	<u><0.002</u>

Silver	mg/l	<u>0.04</u>
Strontium	mg/l	_____
Thallium	mg/l	_____
Thorium	mg/l	_____
Tin	mg/l	_____
Titanium	mg/l	_____
Vanadium	mg/l	_____
Zinc	mg/l	_____

***** Metals are reported as dissolved, unless otherwise indicated. *****

NUTRIENTS:

Ammonia-Nitrogen	mg/l	_____
Nitrite-Nitrogen as N	mg/l	_____
Nitrate-Nitrogen as N	mg/l	<u>19.4</u>
Organic-Nitrogen	mg/l	_____
Total - Kjeldahl Nitrogen	mg/l	_____
Ortho-phosphate as P	mg/l	_____
Phosphorus (Total) as P	mg/l	_____
Phosphorus (Dissolved) as P	mg/l	_____

METALS:

Copper (Total)	mg/l	_____
Iron (Total)	mg/l	_____
Manganese (Total)	mg/l	_____

MISCELLANEOUS:

ADA	g/l	_____
Biochemical Oxygen Demand	mg/l	_____
Chemical Oxygen Demand	mg/l	_____
Cyanide	mg/l	_____
Fecal Coliform Count — Millipore filter/100 ml		_____
Fluoride	mg/l	<u>0.64</u>
Iron Bacteria		_____
Oil & Grease	mg/l	_____
Phenols	mg/l	_____
Total Organic Carbon	mg/l	_____
Total Plate Count per 100ml		_____

**High TDS due to hygroscopic nature of cations and anions.

FIELD DATA:

Flow	-	T° C	<u>5.0° C</u>
E. C.	<u>1400</u>	pH	<u>5.5</u>
Static Water Level	_____		<u>35.86</u>

*Analysis completed by Controls for Environmental Pollution; Santa Fe, New Mexico

Catherine A. Phelps, Chemist



PHONE (701) 258-9720

MINNESOTA VALLEY TESTING LABORATORIES, Inc.

1411 SOUTH 12TH STREET • P.O. BOX 1873
BISMARCK, NORTH DAKOTA 58502-1873



WATER ANALYSIS REPORT

Montana-Dakota Utilities
400 North Fourth
Bismarck, ND 58501

Date: January 27, 1989

W.O. #: 82-045

Attention: John Verwey

Lab. #: M- 157

Sample Identification: MDU - Heskett
#70 16:22 CST
12/20/88

P.O. #: M04548

Date Received: 12/22/88

PHYSICAL PARAMETERS:

Color units of apparent color	_____
Conductivity micromhos/cm @ 25°C	<u>14841</u>
pH	<u>8.0</u>
Solids (Total) mg/l	_____
Solids (Total Dissolved) mg/l	<u>13393</u>
Solids (Total Suspended) mg/l	_____
Solids (Total Volatile) mg/l	_____
Turbidity — NTU	_____

COMMON IONS:

Calcium mg/l	<u>212.5</u>
Magnesium mg/l	<u>117.0</u>
Sodium mg/l	<u>3880.0</u>
Potassium mg/l	<u>26.5</u>
Acidity as CaCO ₃ mg/l	_____
Alkalinity (Total) as CaCO ₃ mg/l	<u>510</u>
Bicarbonate as CaCO ₃ mg/l	<u>510</u>
Bicarbonate as HCO ₃ mg/l	_____
Carbonate as CaCO ₃ mg/l	<u>0</u>
P-Alkalinity as CaCO ₃ mg/l	_____
Sulfate mg/l	<u>8334.9</u>
Chloride mg/l	<u>19.9</u>
Total Hardness as CaCO ₃ mg/l	<u>1012</u>
Sodium Adsorption Ratio	<u>53.19</u>
Cations	<u>190.4</u>
Anions	<u>184.4</u>
% Error	<u>1.6</u>

NUTRIENTS:

Ammonia-Nitrogen mg/l	_____
Nitrite-Nitrogen as N mg/l	_____
Nitrate-Nitrogen as N mg/l	<u><1.0</u>
Organic-Nitrogen mg/l	_____
Total - Kjeldahl Nitrogen mg/l	_____
Ortho-phosphate as P mg/l	_____
Phosphorus (Total) as P mg/l	_____
Phosphorus (Dissolved) as P mg/l	_____

METALS:

Copper (Total) mg/l	_____
Iron (Total) mg/l	_____
Manganese (Total) mg/l	_____

MISCELLANEOUS:

ADA g/l	_____
Biochemical Oxygen Demand mg/l	_____
Chemical Oxygen Demand mg/l	_____
Cyanide mg/l	_____
Fecal Coliform Count — Millipore filter/100 ml	_____
Fluoride mg/l	<u>0.27</u>
Iron Bacteria	_____
Oil & Grease mg/l	_____
Phenols mg/l	_____
Total Organic Carbon mg/l	_____
Total Plate Count per 100ml	_____

TRACE ELEMENTS:

Aluminum mg/l	_____	Cobalt mg/l	_____	Silver mg/l	<u>0.030</u>
Antimony mg/l	_____	Copper mg/l	_____	Strontium mg/l	_____
Arsenic mg/l	<u>0.002</u>	Iron mg/l	<u>0.14</u>	Thallium mg/l	_____
Barium mg/l	<u><0.100</u>	Lead mg/l	<u><0.001</u>	Thorium mg/l	_____
Beryllium mg/l	_____	Manganese mg/l	<u>0.28</u>	Tin mg/l	_____
Boron mg/l	<u>2.800</u>	Mercury mg/l	<u>0.0010</u>	Titanium mg/l	_____
Bromide mg/l	_____	Molybdenum mg/l	<u><0.100</u>	Vanadium mg/l	_____
Cadmium mg/l	<u><0.001</u>	Nickel mg/l	_____	Zinc mg/l	_____
Chromium mg/l	<u><0.050</u>	Selenium mg/l	<u><0.002</u>		

***** Metals are reported as dissolved, unless otherwise indicated. *****

FIELD DATA:	
Flow _____	T ° C <u>6.0°C</u>
E. C. <u>1380</u>	pH <u>6.40</u>
Static Water Level _____	<u>54.90</u>

Catherine Anne Phelps

Catherine A. Phelps, Chemist

EXHIBIT 5-K

HYDRAULIC CONDUCTIVITIES, CATION EXCHANGE CAPACITIES,

AND PARTICLE SIZE ANALYSES

(WELLS 60, WS1, WS2, WS3, AND WS4)



3100 EAST BROADWAY
P.O. BOX 1114
BISMARCK, ND 58502
PHONE 701/223-6149

LABORATORY TEST RESULTS
PROPOSED ASH PIT HESKETT STATION
MANDAN, NORTH DAKOTA

PROJECT:

Montana-Dakota Utilities

DATE: September 18, 1986

REPORTED TO:

Attn: John Verwey
400 North 4th Street
Bismarck, ND 58501

FURNISHED BY:

COPIES TO:

LABORATORY No. 5200-86-454

INTRODUCTION

A sample of fat clay was submitted to Twin City Testing Corporation on August 14, 1986. We were authorized by you to perform an Atterberg limit test, standard proctor test and permeability test. We are transmitting two (2) copies of this report.

RESULTS

The test results can be found on the attached drafts. The permeability test was performed with the falling head method on a sample remolded to 14.5% of the maximum dry density at a moisture content of 32.4%, or 0.1% above the optimum moisture content. The maximum dry density and optimum moisture content were determined in accordance with ASTM:D698.

The test results indicate that the coefficient of permeability is 2.0×10^{-7} centimeters per second on the remolded sample.

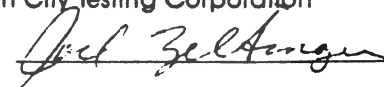
CLOSURE

If you desire to test the coefficient of permeability at a higher remolded compaction level and/or higher moisture content, please contact us. Also contact us if you have any questions in regards to this report or if we can be of further service to you.

AS A MUTUAL PROTECTION TO CLIENTS, THE PUBLIC AND OURSELVES, ALL REPORTS ARE SUBMITTED AS THE CONFIDENTIAL PROPERTY OF CLIENTS, AND AUTHORIZATION FOR PUBLICATION OF STATEMENTS, CONCLUSIONS OR EXTRACTS FROM OR REGARDING OUR REPORTS IS RESERVED PENDING OUR WRITTEN APPROVAL.

Twin City Testing Corporation

By





MOISTURE - DENSITY CURVE

SAMPLE NO. 1 - Hole 60, 20'-40'

PROJECT: PROPOSED ASH PIT HESKETT STATION
 MANDAN, NORTH DAKOTA

REPORTED TO: Montana-Dakota Utilities Company
 Attn: John Verwey

LABORATORY NO. 5200-86-454

DATE: August 21, 1986

COPIES TO:

*LIQUID LIMIT: 59.4

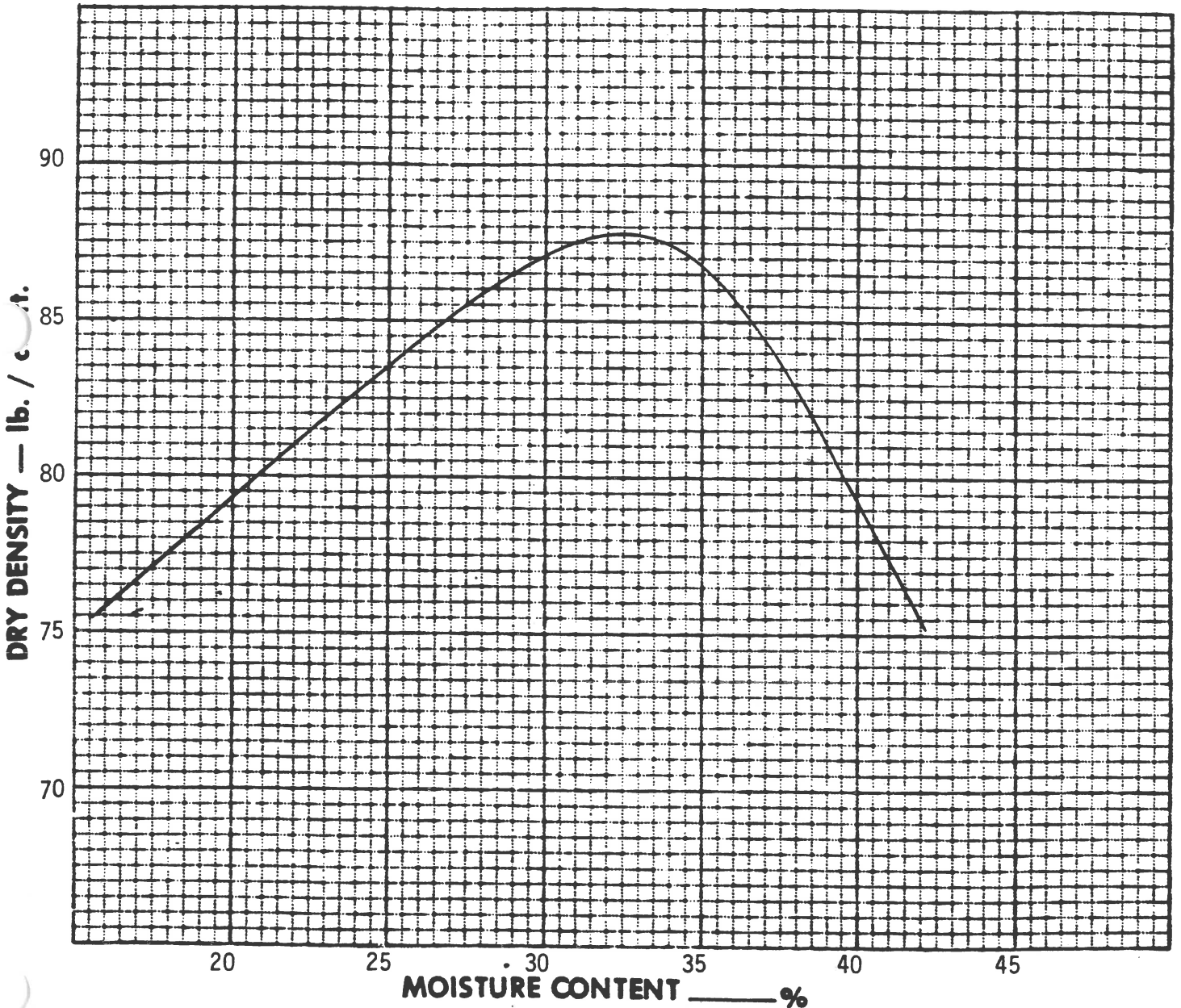
*PLASTIC LIMIT: 23.9

METHOD OF TEST: ASTM:D698-78, Method "A"

TYPE OF MATERIAL: Fat Clay, brown (CH)

MAXIMUM DENSITY: 87.8 lb./cu. ft.

OPTIMUM MOISTURE 32.3 %



Twin City Testing and Engineering Laboratory, Inc.

By David P. Johnson

LABORATORY TEST DATA

PROJECT: PROPOSED ASH PIT-HESKETT STATION-MANDAN, NORTH DAKOTA

REPORTED TO: Montana-Dakota Utilities Company
Attn: John Verwey

JOB NO.: 5200-86-454

Boring No.				
Sample No. Sample Designation	Hole 60			
Depth (ft)	20-40			
Type of Sample	Bag			
Soil Classification (ASTM:D2487)	Fat Clay (CH)			
In-Place Moisture Content (%)	-			
Moisture-Density Relation of Soil (ASTM:D698)				
Max. Dry Density (PCF)	87.8			
Optimum Moisture Content (%)	32.3			
Permeability Test				
Trial No.	6.8			
Type of Test	Falling Head			
Type of Specimen	Compacted			
Specimen Height (inches)	3.00			
Specimen Diameter (inches)	2.82			
Dry Density (PCF)	82.9			
Percent of Max. Density	94.5			
Moisture Content (%)	32.4			
Max. Head Differential (ft)	5.0			
Confining Pressure (effective - PSI)	2.0			
Water Temperature (°C)	21			
Coefficient of Permeability K @ 20°C (cm/sec)	2×10^{-7}			
K @ 20°C (ft/min)	4×10^{-7}			
Atterberg Limits				
Liquid Limit (%)	59.4			
Plastic Limit (%)	23.9			
Plasticity Index	35.5			

December 14, 1981

Water Supply, Inc
PO Box 1191
Bismarck, ND 58502

Attn: Roger Schmid

Gentlemen

Subj: Soil Testing for MDU Heskett Power Plant
Mandan, North Dakota
Invoice #52-0688

Attached herewith, please find our laboratory test results for permeability tests, cation exchange capacity, particle size distribution curves and U.S.D.A. textural classification charts.

If you have any questions or need any additional information, please contact us at the Bismarck office.

Very truly yours,



Gary L. Arman, P.E.
Operations Manager
Western North Dakota

GLA:djs

Encs

LABORATORY TEST DATA

PROJECT: SOIL TESTING FOR MDU HESKETT POWER PLANT - MANDAN, ND

DATE: December 14, 1981

REPORTED TO: Water Supply, Inc

JOB NO.: 52-0688

Boring No.	MDU Heskett 1	MDU Heskett 1	MDU Heskett 1	MDU Heskett 2
Sample No. Sample Designation				
Depth (ft)	20-21	25-26	30-31	29-30
Type of Sample	Core	Core	Core	Core
Soil Classification (ASTM:D2487)	SILTY CLAY & FAT CLAY (CL & CH)	SILTY CLAY & FAT CLAY (CL & CH)	SILTY CLAY & FAT CLAY (CL & CH)	SHALE, (Tex- tural Classi- fication: Fat Clay) (CH)
In-Place Moisture Content (%)				
Moisture-Density Relation of Soil (ASTM:D698)				
Max. Dry Density (PCF)				
Optimum Moisture Content (%)				
Permeability Test				
Trial No.	1	1	1	1
Type of Test	Falling Head	Falling Head	Falling Head	Falling Head
Type of Specimen	Natural	Natural	Natural	Natural
Specimen Height (inches)	4.36	3.49	3.76	2.08
Specimen Diameter (inches)	4.00	2.86	4.00	1.98
Dry Density (PCF)				
Percent of Max. Density				
Moisture Content (%)				
Max. Head Differential (ft)	5.0	5.0	5.0	5.0
Confining Pressure (effective - PSI)	2.0	2.0	2.0	2.0
Water Temperature (°C)	21	21	20	21
Coefficient of Permeability K @ 20°C (cm/sec)	2.6×10^{-8}	1.5×10^{-8}	1.7×10^{-8}	2.7×10^{-9}
K @ 20°C (ft/min)	5.2×10^{-8}	2.9×10^{-8}	3.4×10^{-8}	5.4×10^{-9}
Atterberg Limits				
Liquid Limit (%)				
Plastic Limit (%)				
Plasticity Index				

TWIN CITY TESTING LAB

LABORATORY TEST DATA

PROJECT: SOIL TESTING FOR MDU HESKETT POWER PLANT - MANDAN, ND

DATE: December 14, 1981

REPORTED TO: Water Supply, Inc

JOB NO.: 52-0688

Boring No.	MDU Heskett 2	MDU Heskett 2	MDU Heskett 3	MDU Heskett 3
Sample No. Sample Designation				
Depth (ft)	61-62	73-74	15-16	19-20
Type of Sample	Core	Core	Core	Core
Soil Classification (ASTM:D2487)	SHALE, (Textural Classification: Fat Clay) (CH)	SHALE, (Textural Classification: Fat Clay) (CH)	SILTY CLAY (CL-ML)	FAT CLAY & SILTY CLAY (CH & CL)
In-Place Moisture Content (%)				
Moisture-Density Relation of Soil (ASTM:D698)				
Max. Dry Density (PCF)				
Optimum Moisture Content (%)				
Permeability Test				
Trial No.	1	1	1	1
Type of Test	Falling Head	Falling Head	Falling Head	Falling Head
Type of Specimen	Natural	Natural	Natural	Natural
Specimen Height (inches)	1.96	0.80	2.93	3.29
Specimen Diameter (inches)	1.99	1.98	4.00	4.00
Dry Density (PCF)				
Percent of Max. Density				
Moisture Content (%)				
Max. Head Differential (ft)	5.0	5.0	5.0	50.0
Confining Pressure (effective - PSI)	2.0	2.0	2.0	2.0
Water Temperature (°C)	21	19	22	22
Coefficient of Permeability K @ 20°C (cm/sec)	3.6×10^{-8}	1.8×10^{-8}	8.5×10^{-8}	1.8×10^{-9}
K @ 20°C (ft/min)	7.1×10^{-8}	3.6×10^{-8}	1.7×10^{-7}	3.5×10^{-9}
Atterberg Limits				
Liquid Limit (%)				
Plastic Limit (%)				
Plasticity Index				

TWIN CITY TESTING LAB

LABORATORY TEST DATA

PROJECT: SOIL TESTING FOR MDU HESKETT POWER PLANT - MANDAN, ND

DATE: December 14, 1981

REPORTED TO: Water Supply, Inc

JOB NO.: 52-0688

Boring No.	MDU Heskett 3	MDU Heskett 4	MDU Heskett 4	MDU Heskett 4
Sample No. Sample Designation				
Depth (ft)	31-32	9-10	41-42	51-52
Type of Sample	Core	Core	Core	Core
Soil Classification (ASTM:D2487)	SILTY CLAY & FAT CLAY (CL & CH)	FAT CLAY & SILTY CLAY (CH & CL)	SHALE, (Tex- tural Classi- fication: Organic Fat Clay (CH-OH))	SHALE, (Tex- tural Classi- fication: Silty Clay (CL))
In-Place Moisture Content (%)				
Moisture-Density Relation of Soil (ASTM:D698)				
Max. Dry Density (PCF)				
Optimum Moisture Content (%)				
Permeability Test				
Trial No.	1	1	1	1
Type of Test	Falling Head	Falling Head	Falling Head	Falling Head
Type of Specimen	Natural	Natural	Natural	Natural
Specimen Height (inches)	2.20	3.63	2.31	2.31
Specimen Diameter (inches)	4.00	4.00	1.98	1.45
Dry Density (PCF)				
Percent of Max. Density				
Moisture Content (%)				
Max. Head Differential (ft)	30.0	50.0	5.0	5.0
Confining Pressure (effective - PSI)	2.0	2.0	2.0	2.0
Water Temperature (°C)	21	22	20	21
Coefficient of Permeability K @ 20°C (cm/sec)	9.1×10^{-9}	7.2×10^{-9}	7.6×10^{-9}	1.9×10^{-7}
K @ 20°C (ft/min)	1.8×10^{-8}	1.4×10^{-8}	1.5×10^{-8}	3.7×10^{-7}
Atterberg Limits				
Liquid Limit (%)				
Plastic Limit (%)				
Plasticity Index				

TWIN CITY TESTING LAB



REPORT OF: CATION EXCHANGE CAPACITY

SOIL TESTING FOR MDU HESKETT POWER

PLANT - MANDAN, NORTH DAKOTA

DATE: December 14, 1981

PROJECT:

REPORTED TO:

Water Supply, Inc
PO Box 1191
Bismarck, ND 58502
Attn: Roger Schmid

LABORATORY No. 52-0688

<u>SAMPLE NUMBER</u>	<u>DEPTHS</u>	<u>CATION EXCHANGE CAPACITY (meq/100g) (milliequivalents/100 gr)</u>
MDU Heskett #1	20'-21'	71.8
#1	25'-26'	12.3
#1	30'-31'	74.2
#1	40'-41'	27.4
MDU Heskett #2	29'-30'	92.2
#2	56'-57'	69.7
#2	61'-62'	12.0
#2	73'-74'	48.4
MDU Heskett #3	15'-16'	70.1
#3	19'-20'	58.1
#3	31'-32'	35.6
MDU Heskett #4	9'-10'	40.4
#4	15'-16'	60.9
#4	31'-32'	26.1
#4	41'-42'	51.3
#4	51'-52'	56.4



twin city testing
and engineering laboratory, inc.
662 CROWWELL AVENUE
ST PAUL, MN 55114
PHONE 612-645-3601

Job No. 52-0688

Sample No. MDU Heskett #1 Depth: 20'-21'

Classification (ASTM:D2487) CL & CH

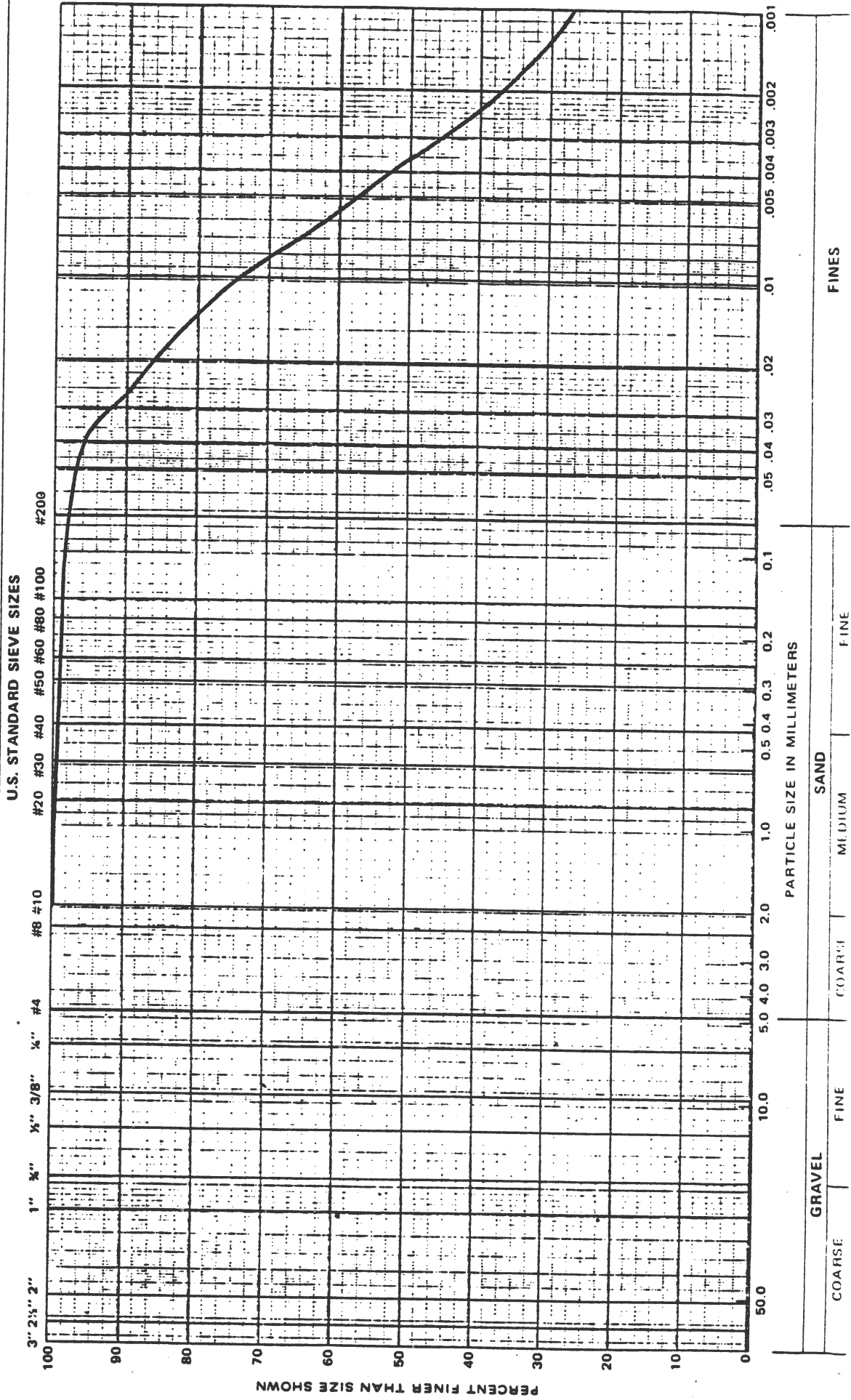
Description SILTY CLAY & FAT CLAY

Project: SOIL TESTING FOR MDU HESKETT

POWER PLANT - MANDAN, NORTH DAKOTA

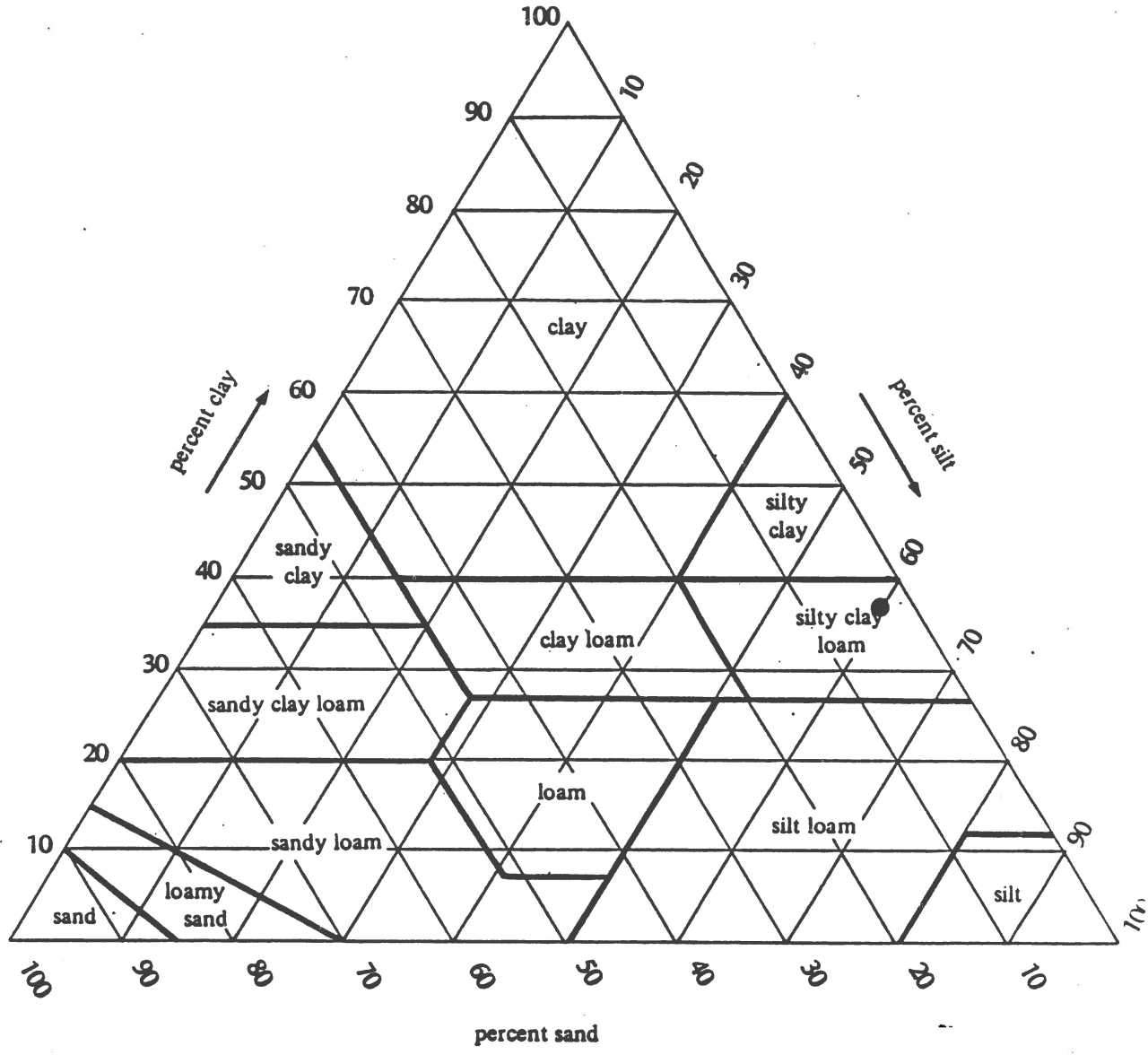
Reported To: Water Supply, Inc.

GRAIN SIZE DISTRIBUTION CURVE



USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #1, 20'-21'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

Size Range in Millimeters (Mean Diameter)												
75	2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008	
GRAVEL	SAND					SILT			CLAY			
	Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine	
	10	18	35	60	140	300						
U.S. Standard Sieve Numbers												

TWIN CITY TESTING LAB



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ST. PAUL, MN 55114
PHONE 612/645-3601

Job No. 52-0688

Sample No. MDU Heskett #1 Depth: 25' -26'

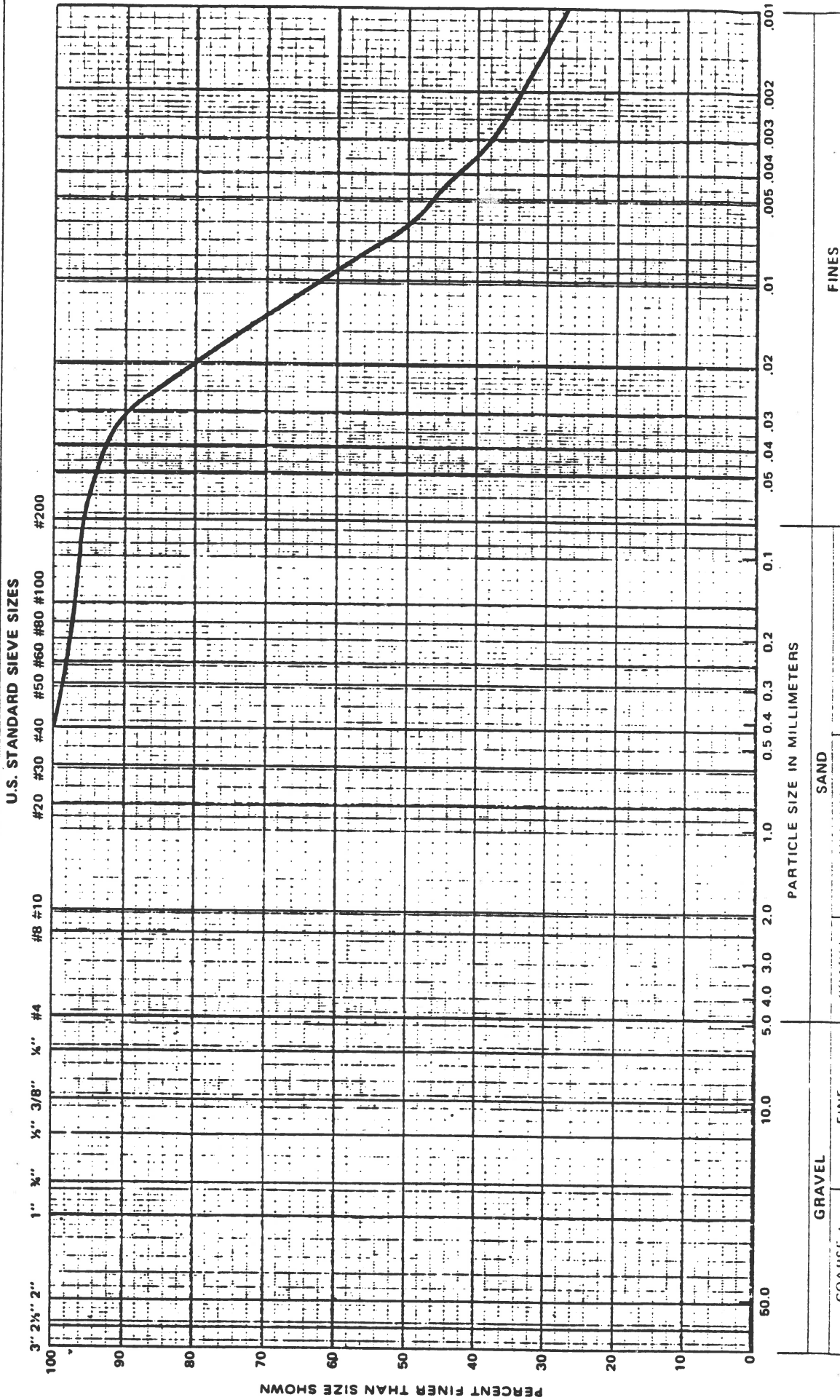
Classification (ASTM:D2487) CL & CH

Description SILTY CLAY & FAT CLAY

Project: SOIL TESTING FOR MDU HESKETT
POWER PLANT - MANDAN, NORTH DAKOTA

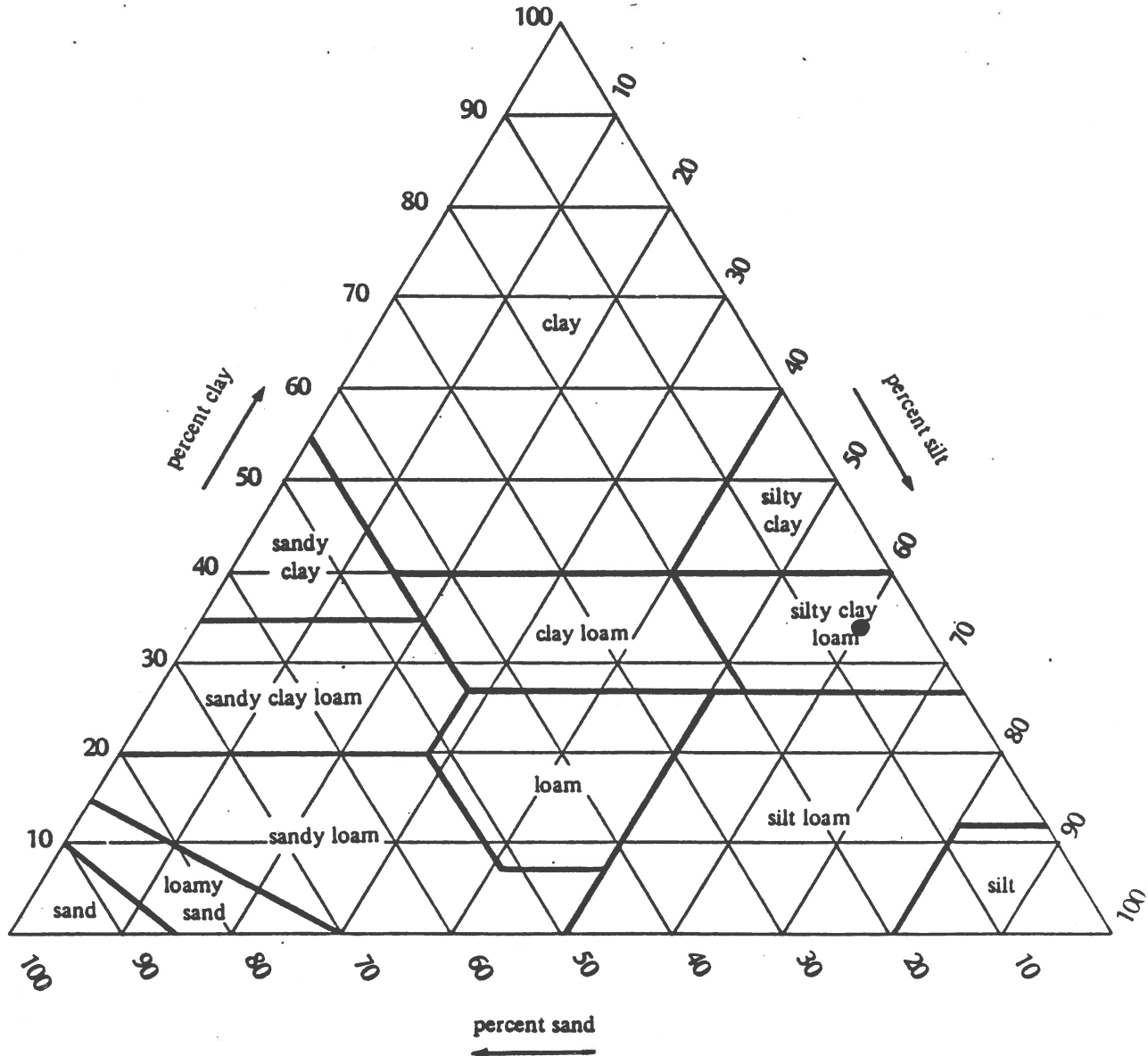
Reported To: Water Supply, Inc.

GRAIN SIZE DISTRIBUTION CURVE



USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #1, 25'-26'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

Size Range in Millimeters (Mean Diameter)												
75	2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008	
GRAVEL	SAND					SILT			CLAY			
	Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine	
	10	18	35	60	140	300						
U.S. Standard Sieve Numbers												

TWIN CITY TESTING LAB



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PHONE 612/645-3601

Job No. 52-0688

Sample No. MDU Heskett #1 Depth: 30' -31'

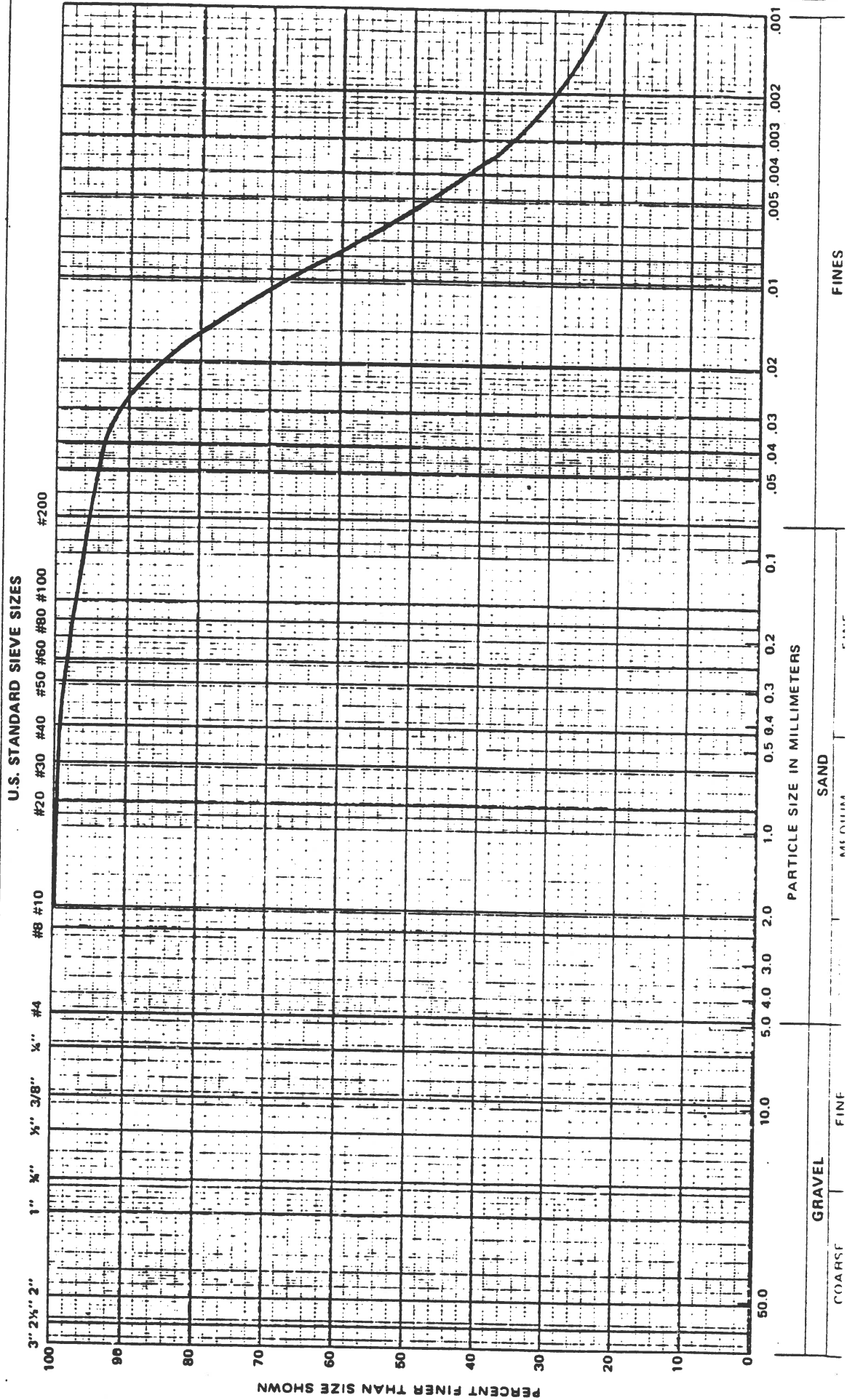
Classification (ASTM:D2487) CL & CH

Description SILTY CLAY & FAT CLAY

Project: SOIL TESTING FOR MDU HESKETT
POWER PLANT - MANDAN, NORTH DAKOTA

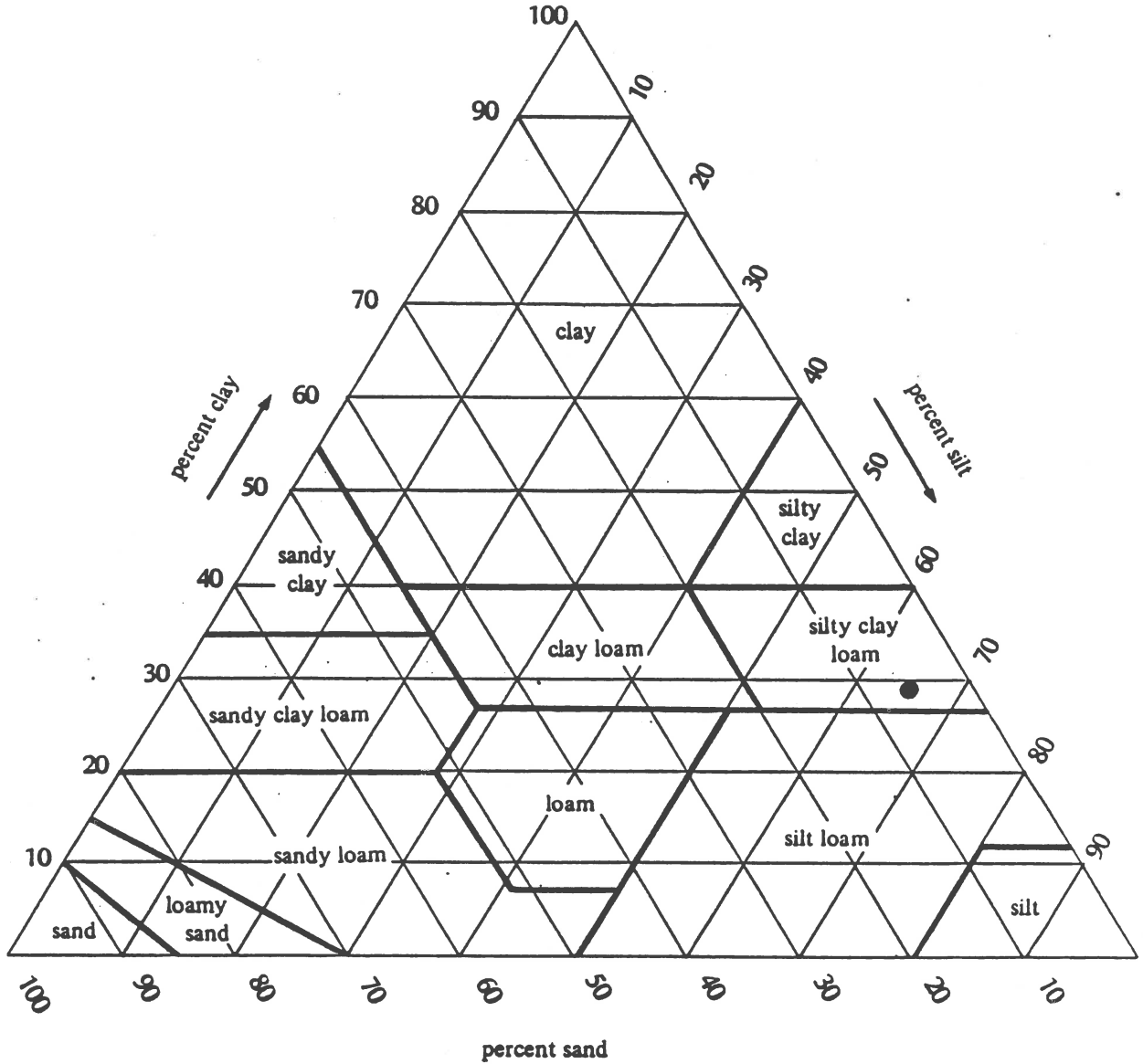
Reported To: Water Supply, Inc.

GRAIN SIZE DISTRIBUTION CURVE



USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #1, 30'-31'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

Size Range in Millimeters (Mean Diameter)											
75	2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008
GRAVEL	SAND					SILT			CLAY		
	Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine
	10	18	35	60	140	300					
U.S. Standard Sieve Numbers											

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PHONE 612-645-3601

Job No. 52-0688

Sample No. MDU Heskett #2 Deptl.: 29' - 30'

Classification (ASTM: D2487) CH

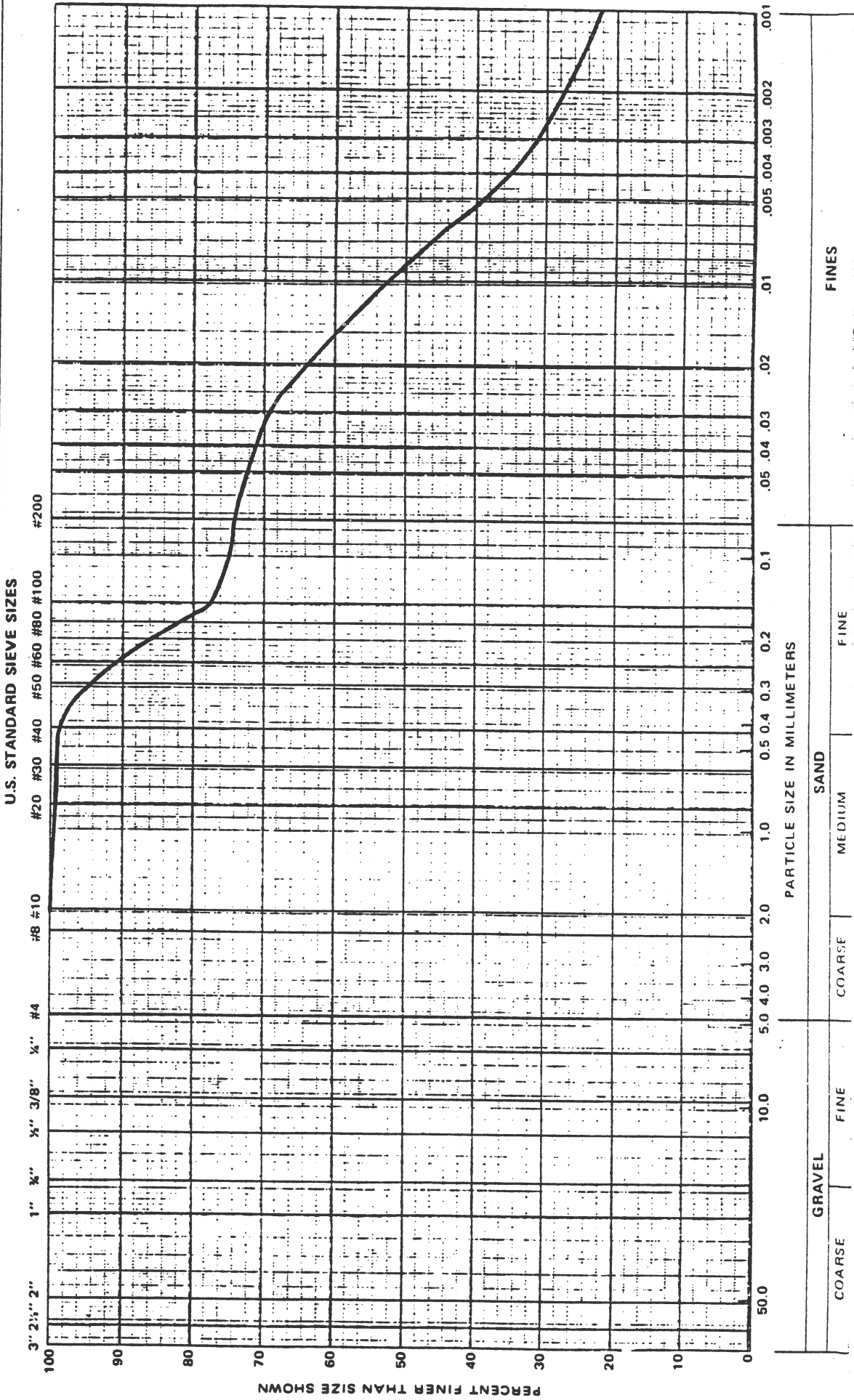
Description SHALE, (Textural Classification: Fat Clay)

Project: SOIL TESTING FOR MDU HESKETT

POWER PLANT - MANDAN, NORTH DAKOTA

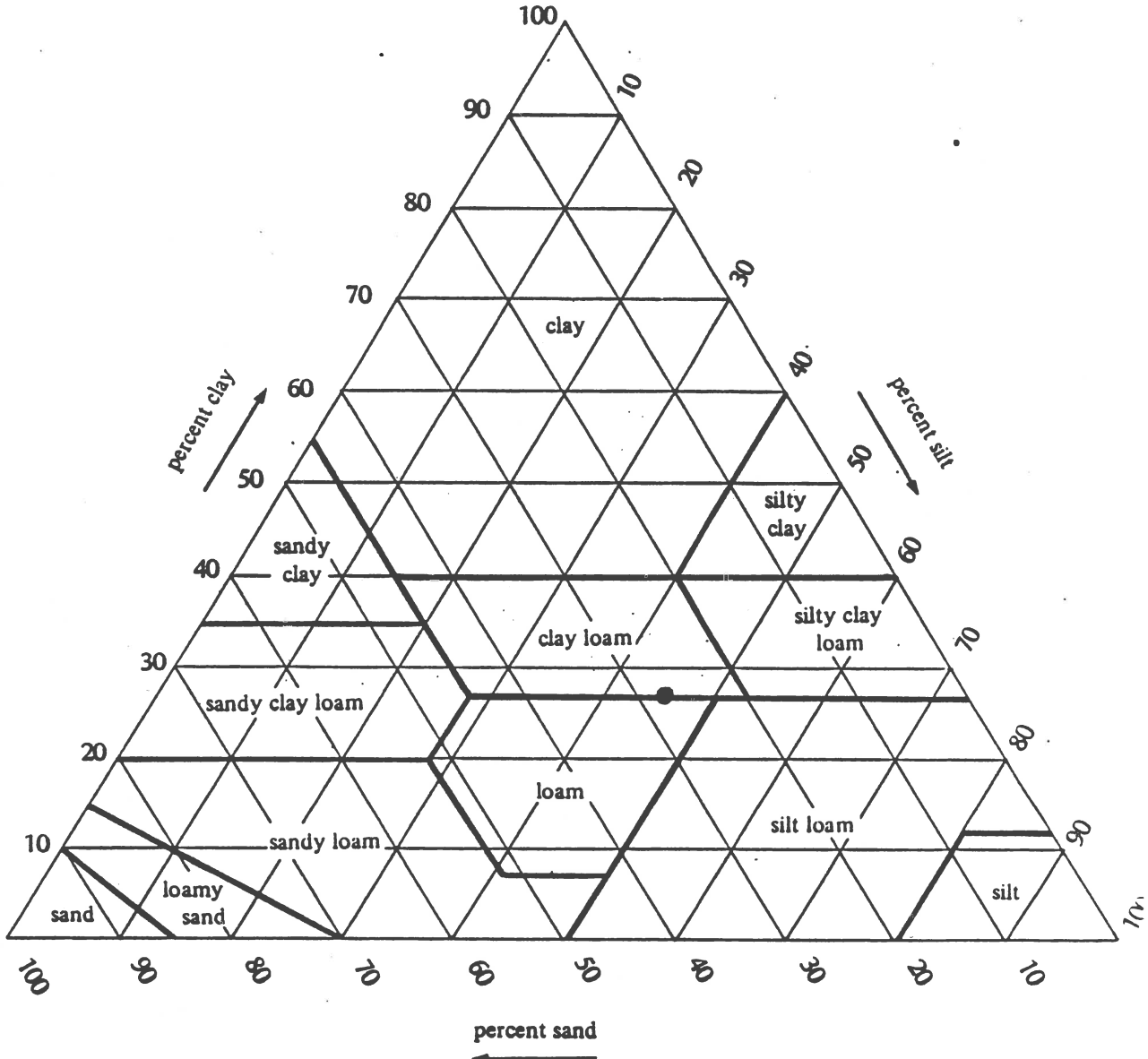
Reported To: Water Supply, Inc.

GRAIN SIZE DISTRIBUTION CURVE



USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #2, 29'-30'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

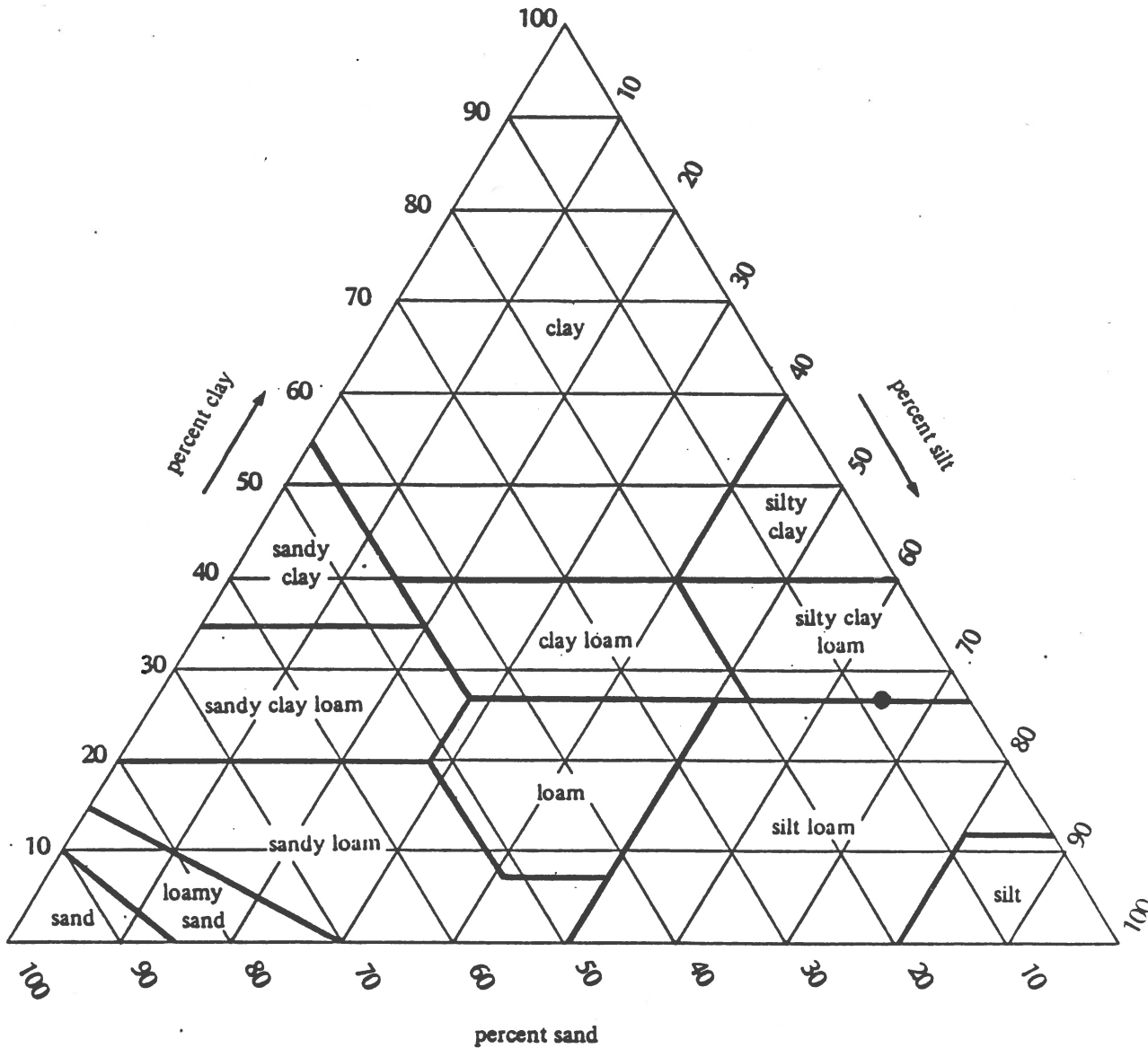
Size Range in Millimeters (Mean Diameter)											
75	2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008
GRAVEL	SAND					SILT			CLAY		
	Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine
	10	18	35	60	140	300					

U.S. Standard Sieve Numbers

TWIN CITY TESTING LAB

USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #2, 61'-62'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

Size Range in Millimeters (Mean Diameter)

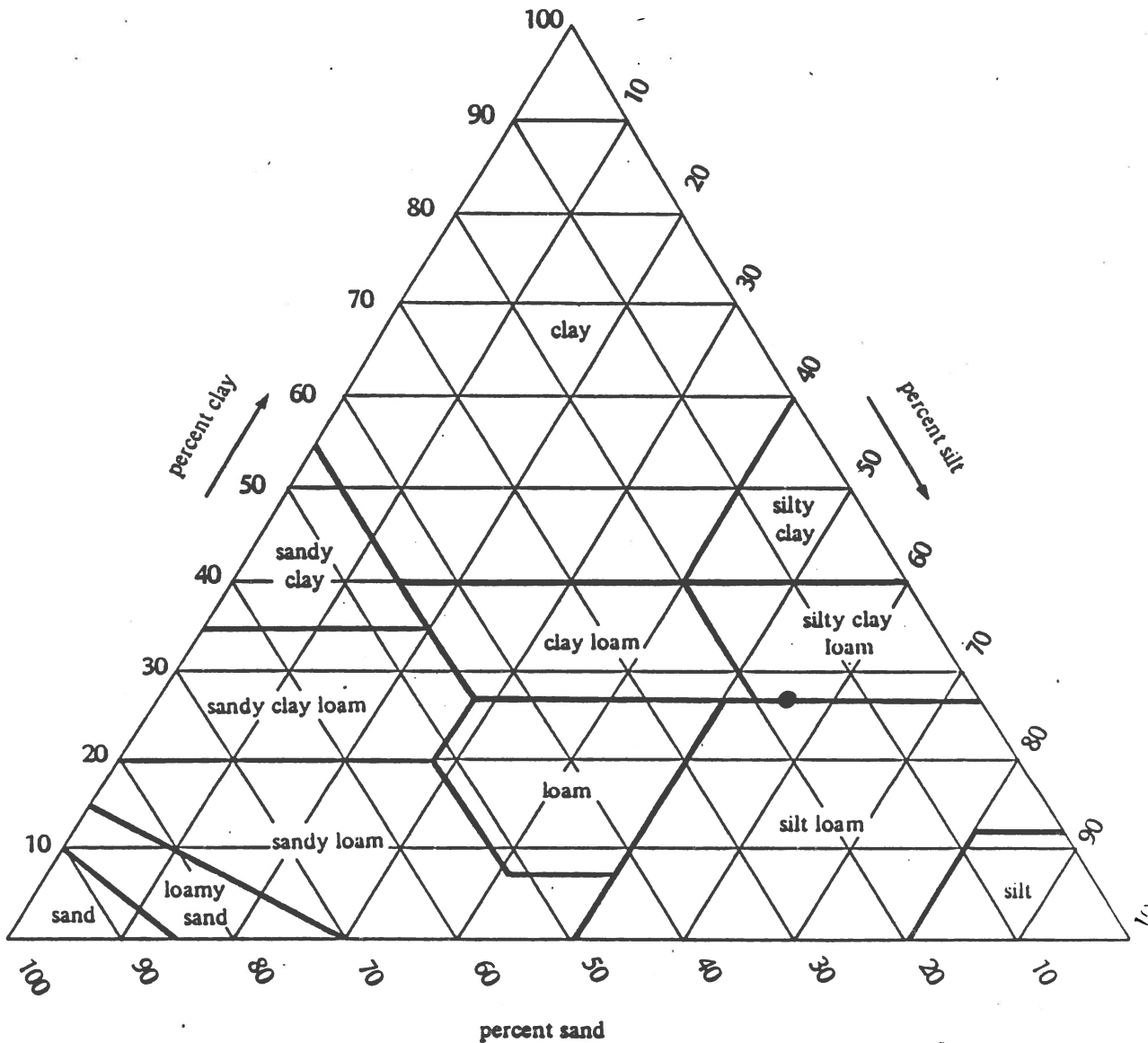
		2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008
GRAVEL	SAND					SILT				CLAY		
	Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine	
	10	18	35	60	140	300						

U.S. Standard Sieve Numbers

TWIN CITY TESTING LAB

USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #2, 73'-74'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

Size Range in Millimeters (Mean Diameter)

75	2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008
GRAVEL	SAND					SILT			CLAY		
	Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine
	10	18	35	60	140	300					

U.S. Standard Sieve Numbers

TWIN CITY TESTING LAB



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667 CROMWELL AVENUE
ST. PAUL, MN 55114
PHONE 612/645-3601

Job No. 52-0688

Sample No. MDU Heskett #3 Dept.: 15'-16'

Classification (ASTM: D2487) CL-ML

Description SILTY CLAY

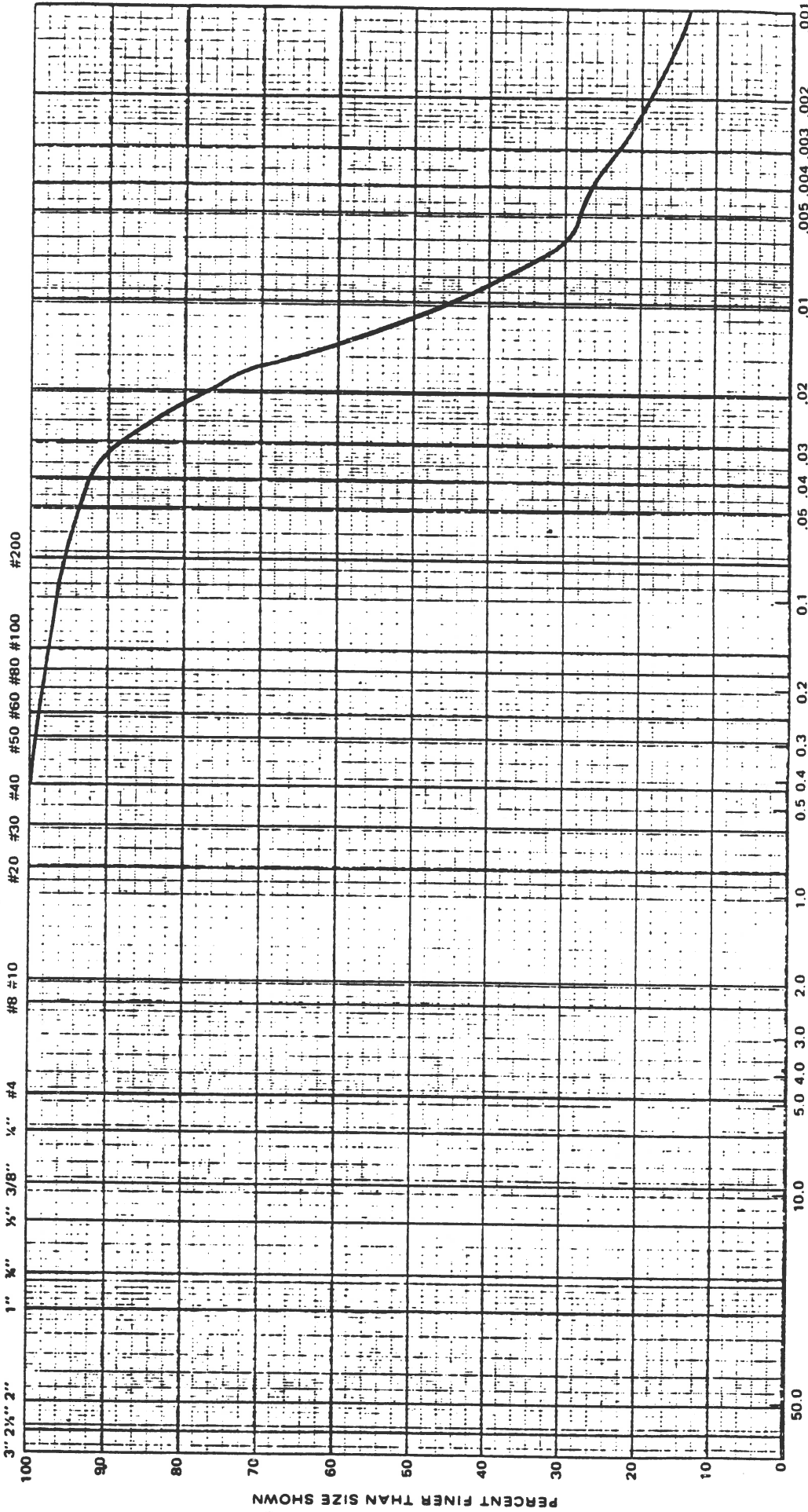
Project: SOIL TESTING FOR MDU HESKETT

POWER PLANT - MANDAN, NORTH DAKOTA

Reported To: Water Supply, Inc.

GRAIN SIZE DISTRIBUTION CURVE

U.S. STANDARD SIEVE SIZES



PARTICLE SIZE IN MILLIMETERS

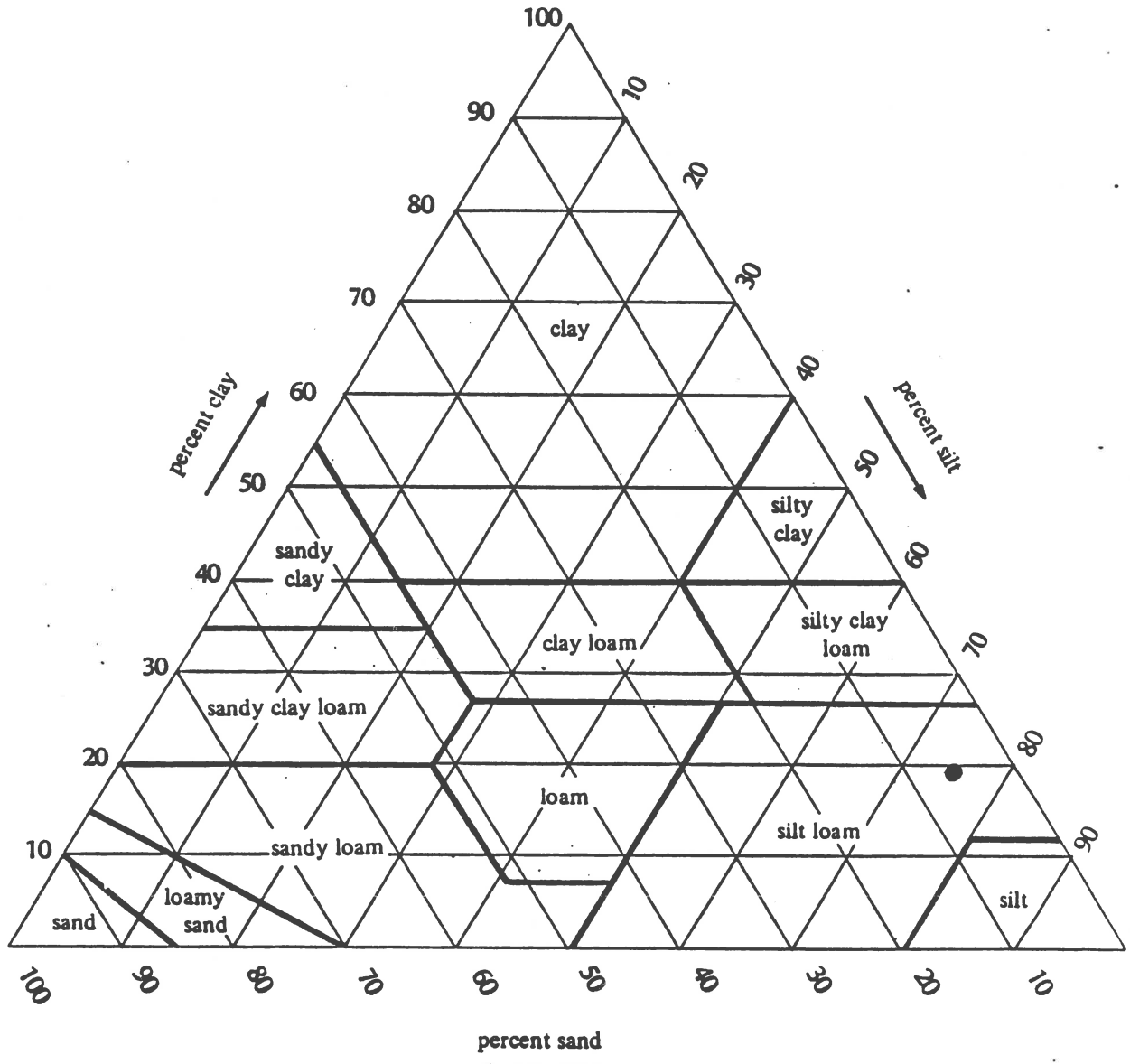
GRAVEL: COARSE, FINE

SAND: COARSE, MEDIUM, FINE

FINES: .001, .002, .003, .004, .005, .01, .02, .03, .04, .05, .1, .2, .3, .4, .5, .6, .75, 1.0, 1.18, 1.5, 2.0, 2.5, 3.0, 3.75, 4.75, 6.0, 7.5, 9.5, 12.5, 15, 19, 25, 30, 37.5, 47.5, 60, 75, 95, 125, 150, 190, 250, 300, 375, 475, 600, 750, 950, 1200, 1500, 1900, 2500, 3000, 3750, 4750, 6000, 7500, 9500, 12000, 15000, 19000, 25000, 30000, 37500, 47500, 60000, 75000, 95000, 120000, 150000, 190000, 250000, 300000, 375000, 475000, 600000, 750000, 950000, 1200000, 1500000, 1900000, 2500000, 3000000, 3750000, 4750000, 6000000, 7500000, 9500000, 12000000, 15000000, 19000000, 25000000, 30000000, 37500000, 47500000, 60000000, 75000000, 95000000, 120000000, 150000000, 190000000, 250000000, 300000000, 375000000, 475000000, 600000000, 750000000, 950000000, 1200000000, 1500000000, 1900000000, 2500000000, 3000000000, 3750000000, 4750000000, 6000000000, 7500000000, 9500000000, 12000000000, 15000000000, 19000000000, 25000000000, 30000000000, 37500000000, 47500000000, 60000000000, 75000000000, 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USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #3, 15'-16'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

Size Range in Millimeters (Mean Diameter)												
75	2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008	
GRAVEL	SAND					SILT			CLAY			
	Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine	
	10	18	35	60	140	300						
U.S. Standard Sieve Numbers												

TWIN CITY TESTING LAB



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662 CROMWELL AVENUE
ST. PAUL, MN 55114
PHONE 612/645-3601

Job No. 52-0688

Sample No. MDU Heskett #3 Dept.: 19'-20'

Classification (ASTM: D2487) CH & CL

Description FAT CLAY & SILTY CLAY (Note: Distribution curve based on
-10 material used for hydrometer test rather than total sample due
to small boulder in a small sample.)

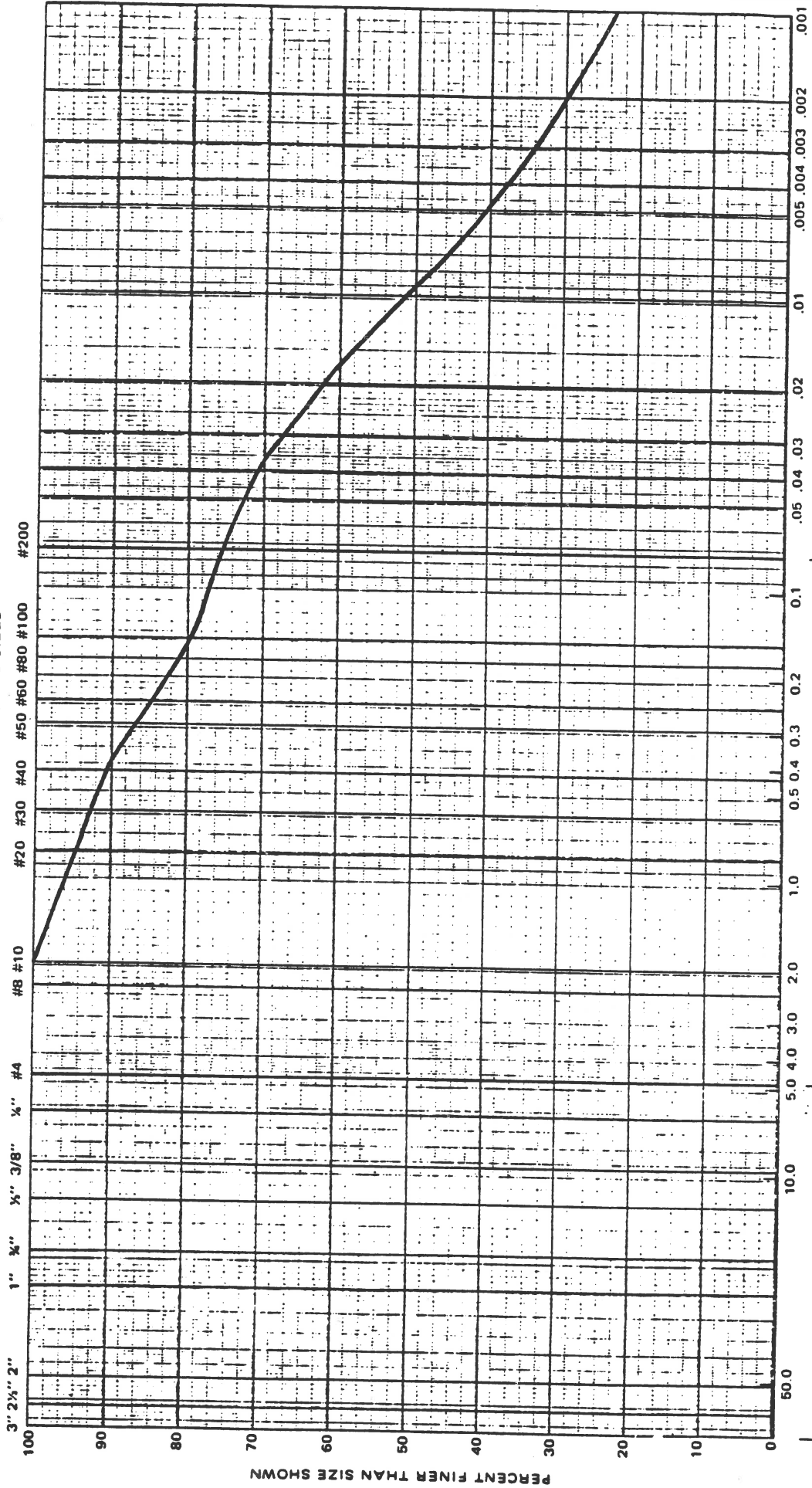
Project: SOIL TESTING FOR MDU HESKETT

POWER PLANT - MANDAN, NORTH DAKOTA

Reported To: Water Supply, Inc

GRAIN SIZE DISTRIBUTION CURVE

U.S. STANDARD SIEVE SIZES



PARTICLE SIZE IN MILLIMETERS

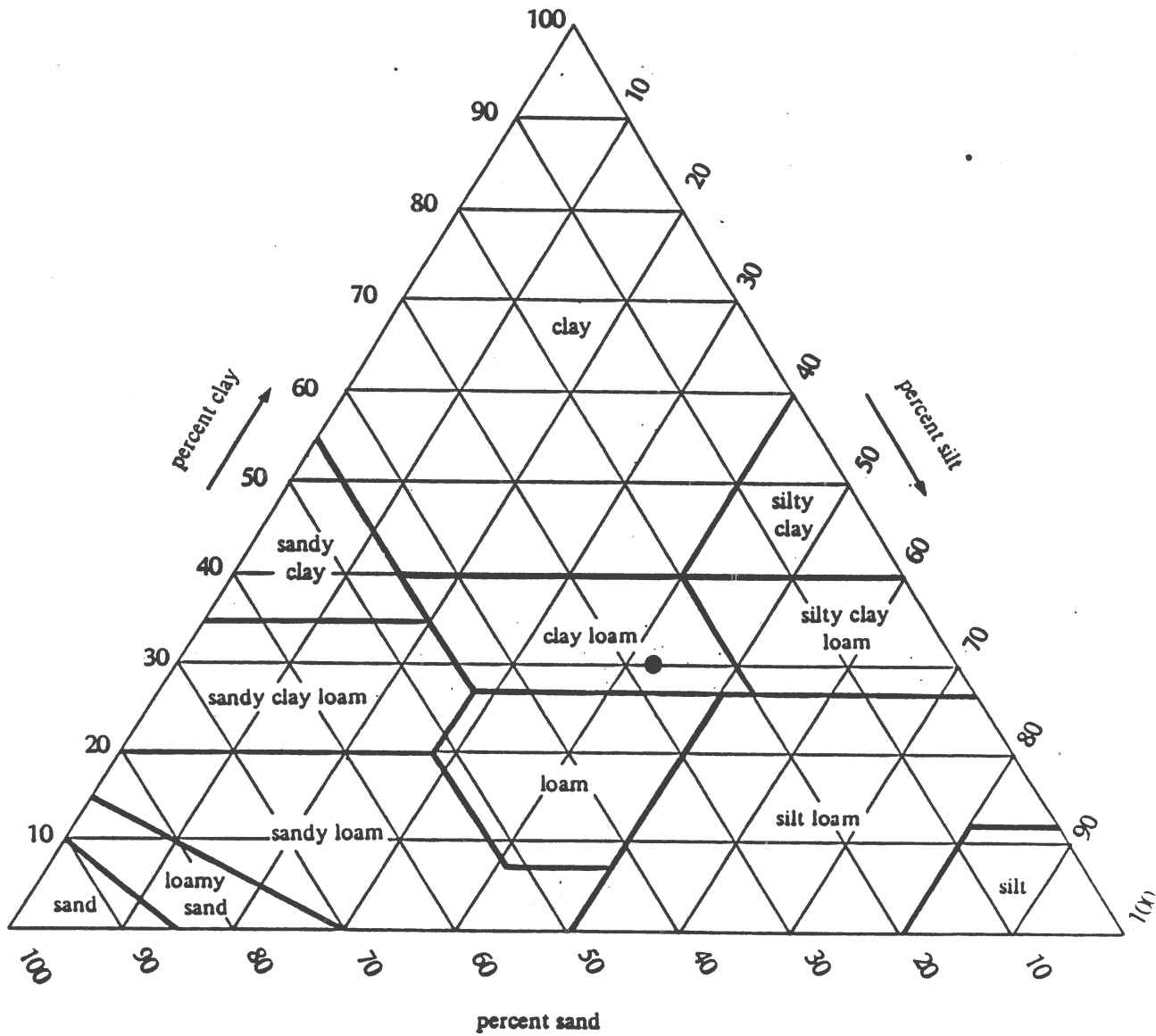
GRAVEL
COARSE FINE

SAND
MEDIUM FINE

FINES

USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #3, 19'-20'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

Size Range in Millimeters (Mean Diameter)												
75	2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008	
GRAVEL	SAND					SILT			CLAY			
	Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine	
	10	18	35	60	140	300						
U.S. Standard Sieve Numbers												

TWIN CITY TESTING LAB



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and engineering laboratory, inc.

662 CROMWELL AVENUE
ST PAUL, MN 55114
PHONE 612/645-3601

Job No. 52-0688

Sample No. MDU Heskett #3 Depth: 31' - 32'

Classification (ASTM:D2487) CL & CH

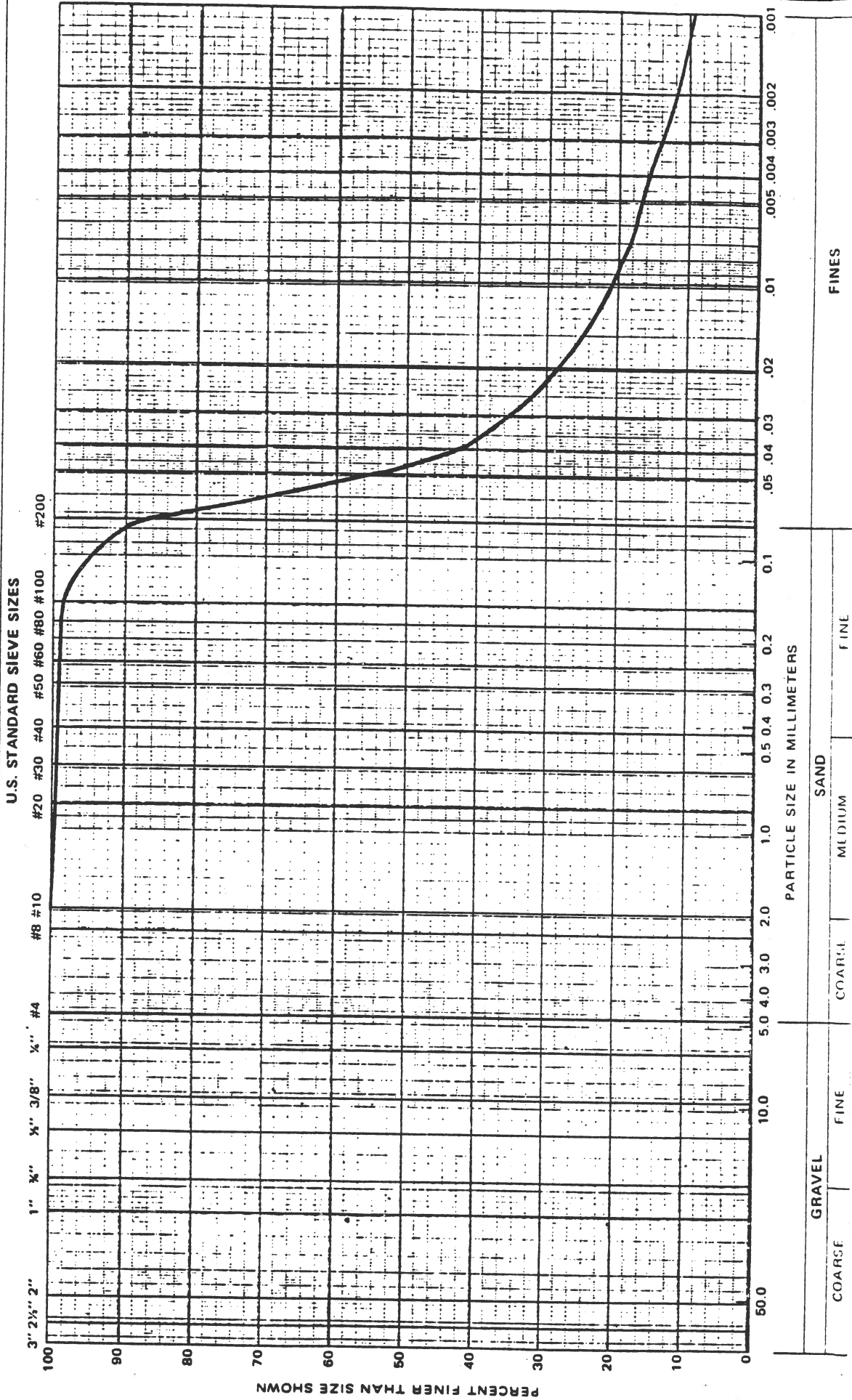
Description SILTY CLAY & FAT-CLAY

Project: SOIL TESTING FOR MDU HESKETT

POWER PLANT - MANDAN, NORTH DAKOTA

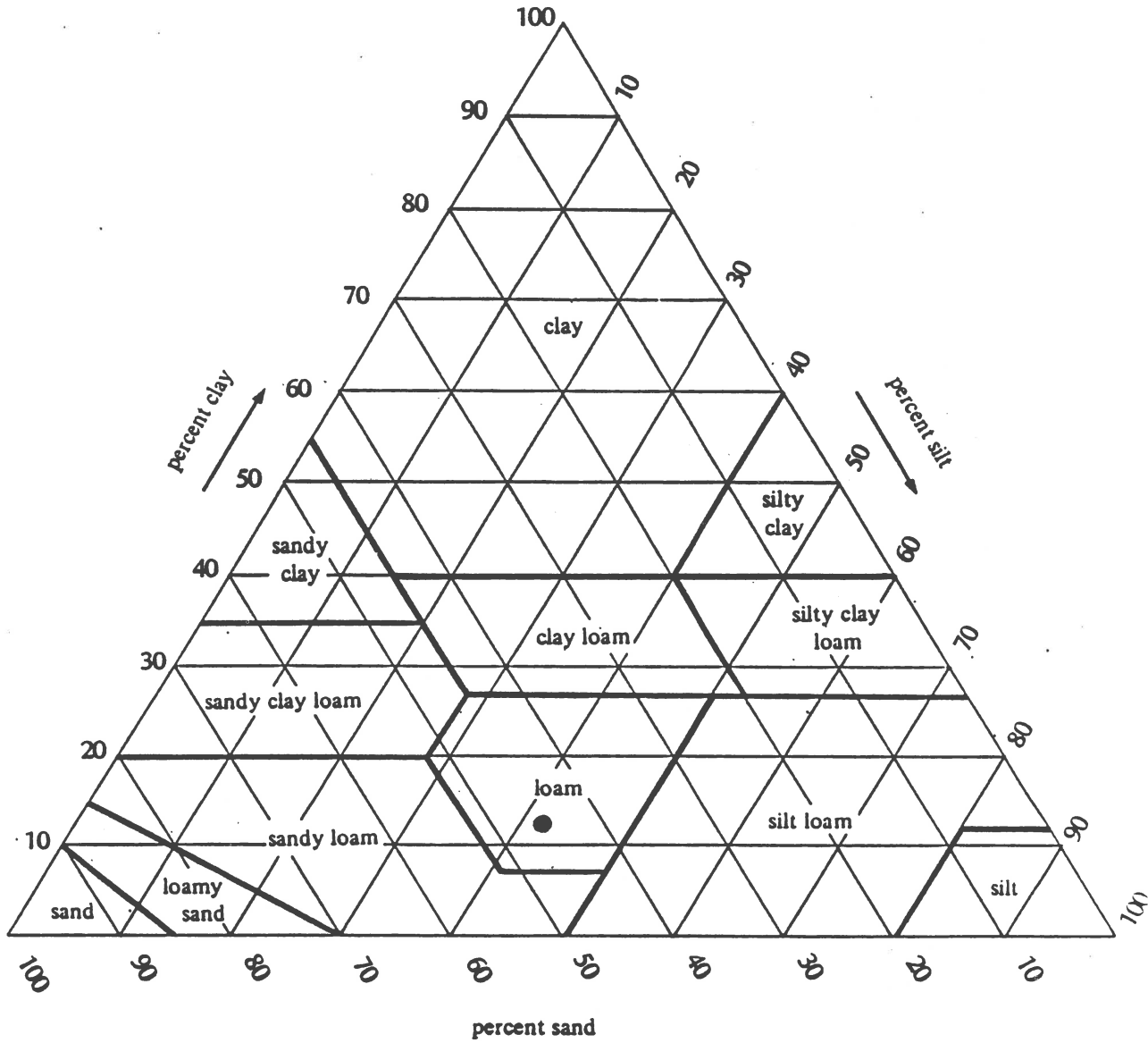
Reported To: Water Supply, Inc.

GRAIN SIZE DISTRIBUTION CURVE



USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #3, 31'-32'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

Size Range in Millimeters (Mean Diameter)											
75	2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008
GRAVEL	SAND					SILT			CLAY		
	Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine
	10	18	35	60	140	300					
U.S. Standard Sieve Numbers											

TWIN CITY TESTING LAB

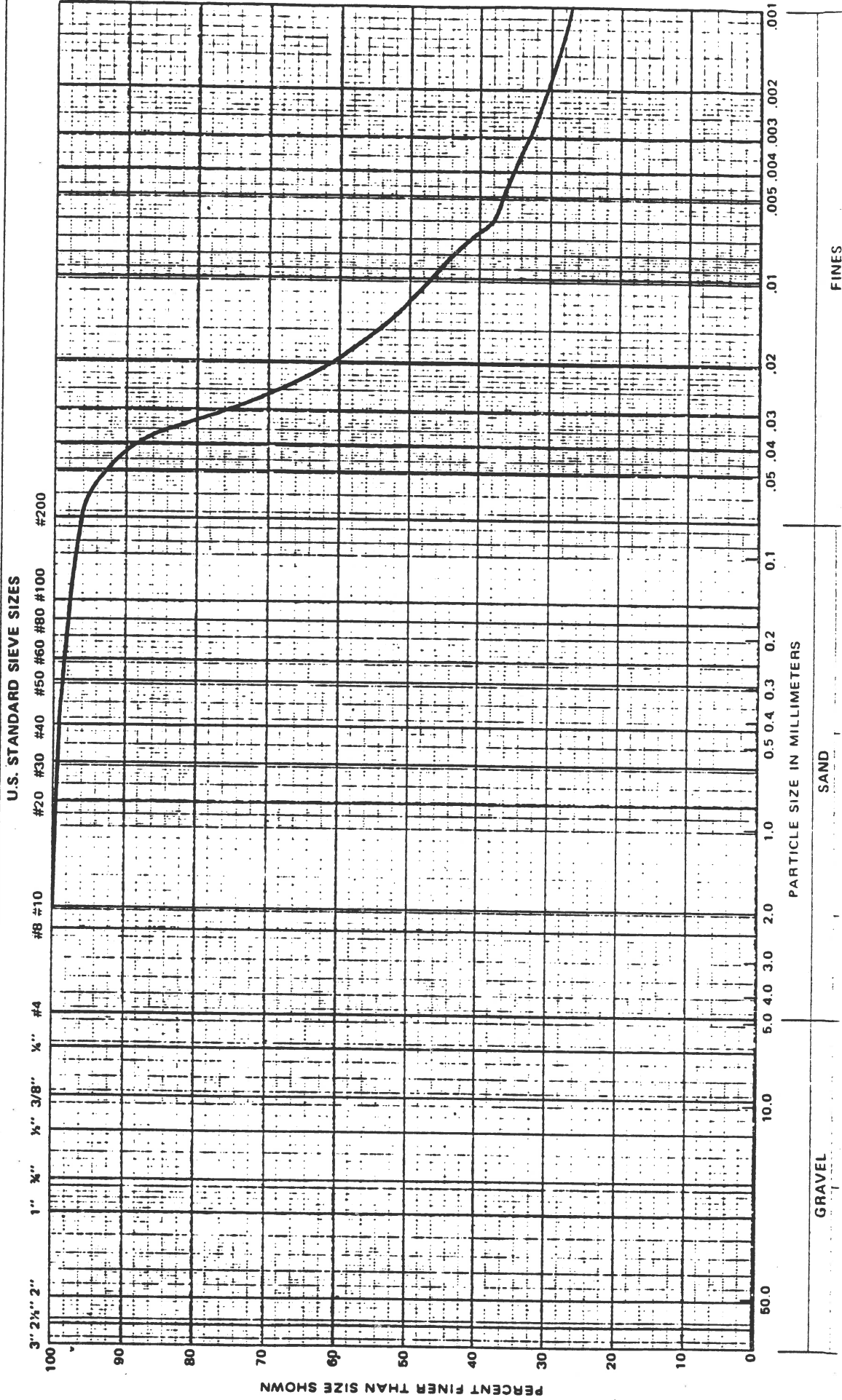


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ST. PAUL, MN 55114
PHONE 612/645-3601

Job No. 52-0688
SAMPLE NO. MDU Heskett #4 Dept.: 9' - 10'
Classification (ASTM: D2487) CH & CL
Description FAT CLAY & SILTY CLAY

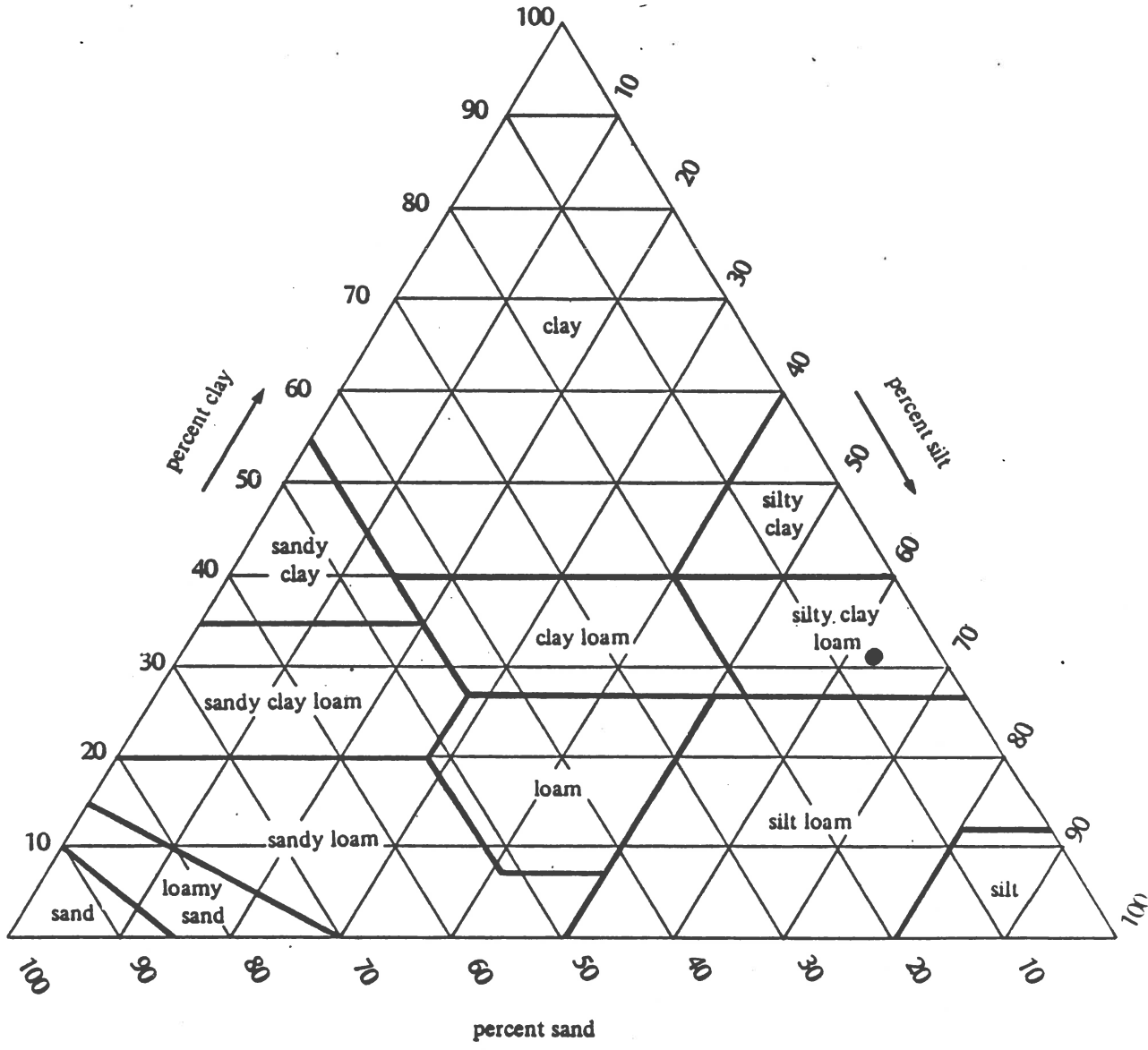
Project: SOIL TESTING FOR MDU HESKETT
POWER PLANT - MANDAN, NORTH DAKOTA
Reported To: Water Supply, Inc.

GRAIN SIZE DISTRIBUTION CURVE



USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #4, 9'-10'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

Size Range in Millimeters (Mean Diameter)												
75	2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008	
GRAVEL	SAND					SILT				CLAY		
	Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine	
	10	18	35	60	140	300						
U.S. Standard Sieve Numbers												

TWIN CITY TESTING LAB



Job No. 52-0688

Sample No. MDU Heskett #4 Depth: 15'-16'

Classification (ASTM:D2487) CL & CH

Description SILTY CLAY & FAT CLAY

twin city testing
and engineering laboratory, inc.

662 CROMWELL AVENUE
ST PAUL, MN 55114
PHONE 612/645-3601

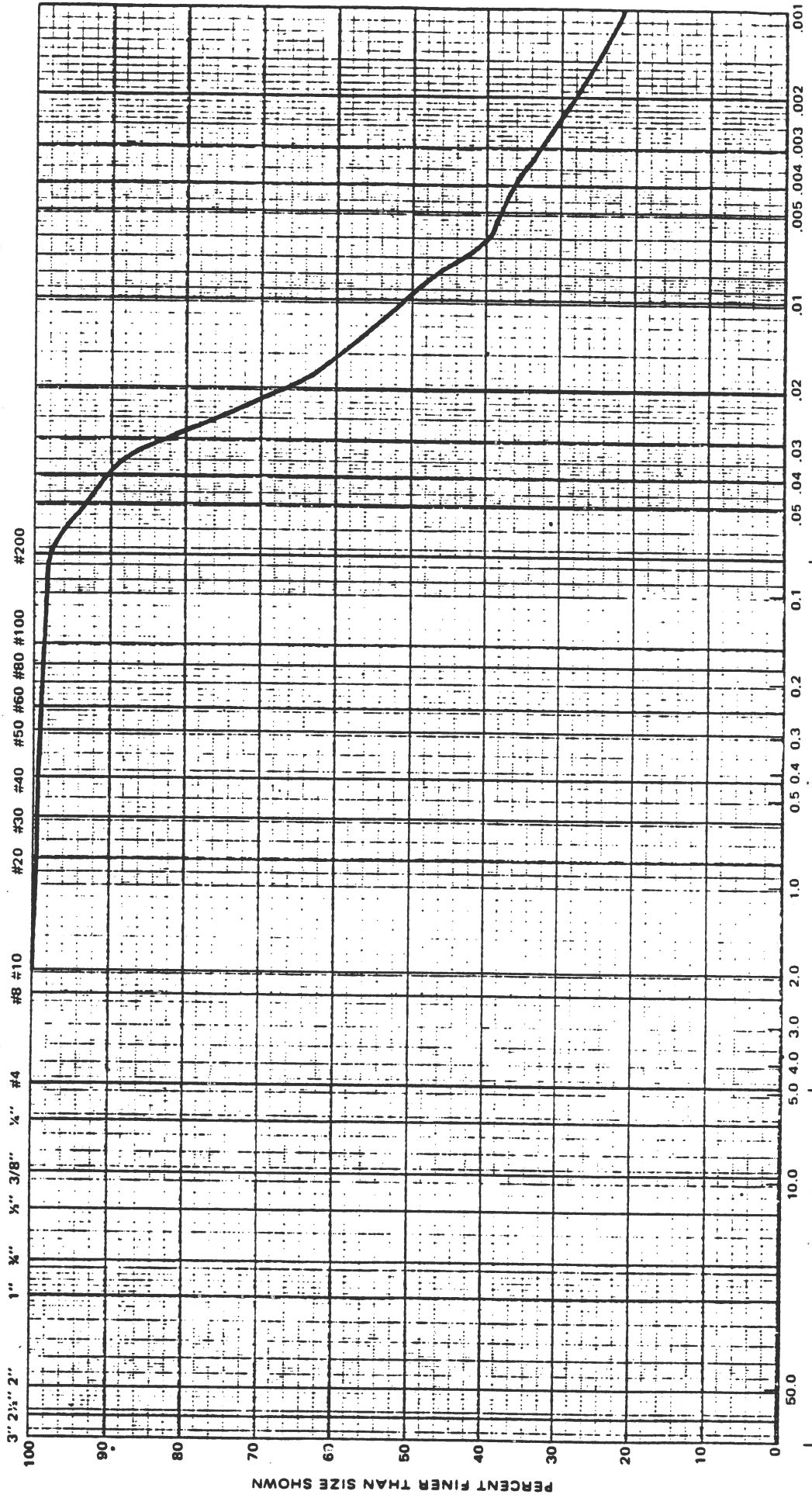
Project: SOIL TESTING FOR MDU HESKETT

POWER PLANT - MANDAN, NORTH DAKOTA

Reported To: Water Supply, Inc.

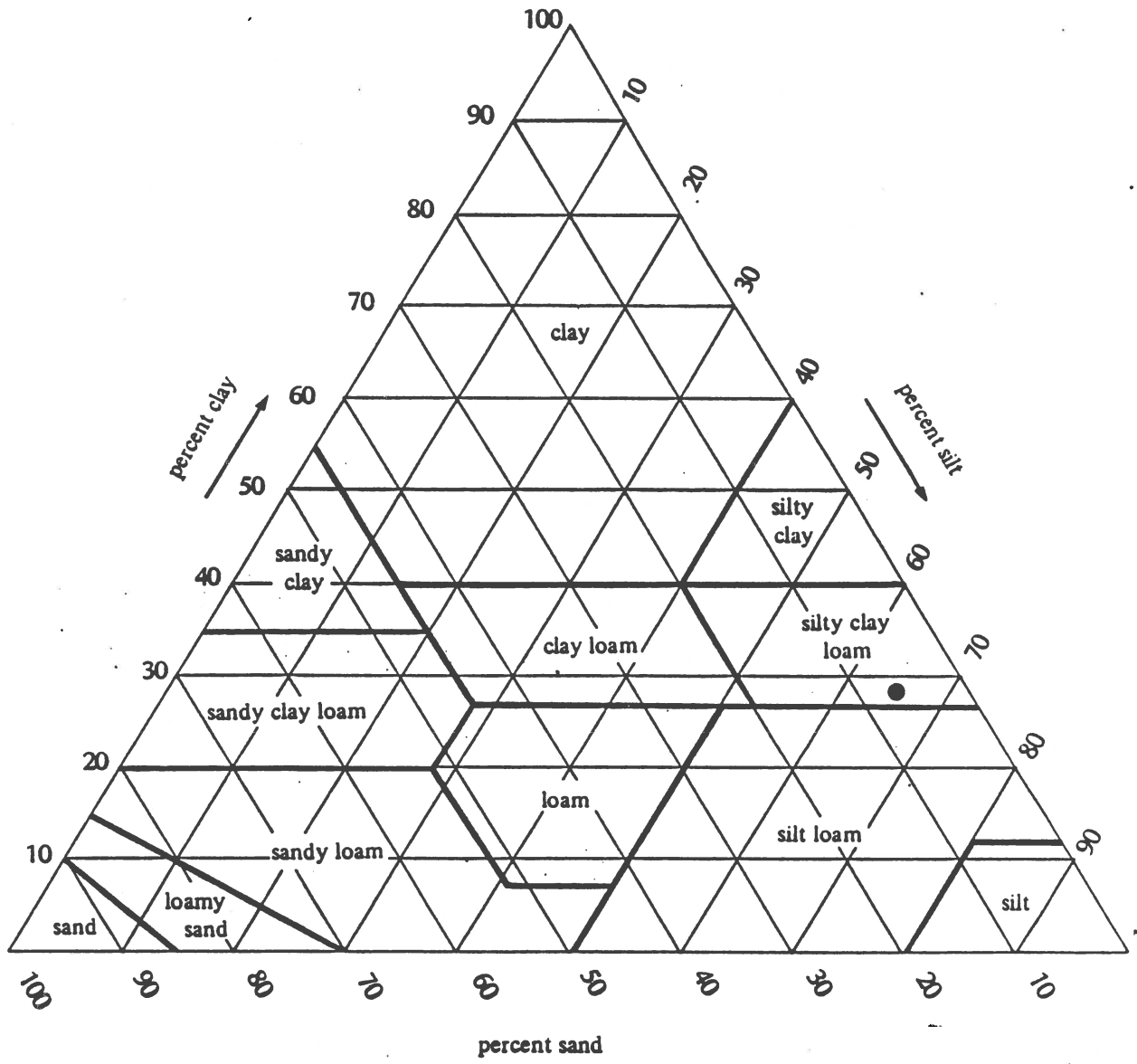
GRAIN SIZE DISTRIBUTION CURVE

U.S. STANDARD SIEVE SIZES



USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #4, 15'-16'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

Size Range in Millimeters (Mean Diameter)

	2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008
GRAVEL	SAND					SILT			CLAY		
	Very Coarse	Coarse	Me- dium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine
	10	18	35	60	140	300					
	U.S. Standard Sieve Numbers										

TWIN CITY TESTING LAB



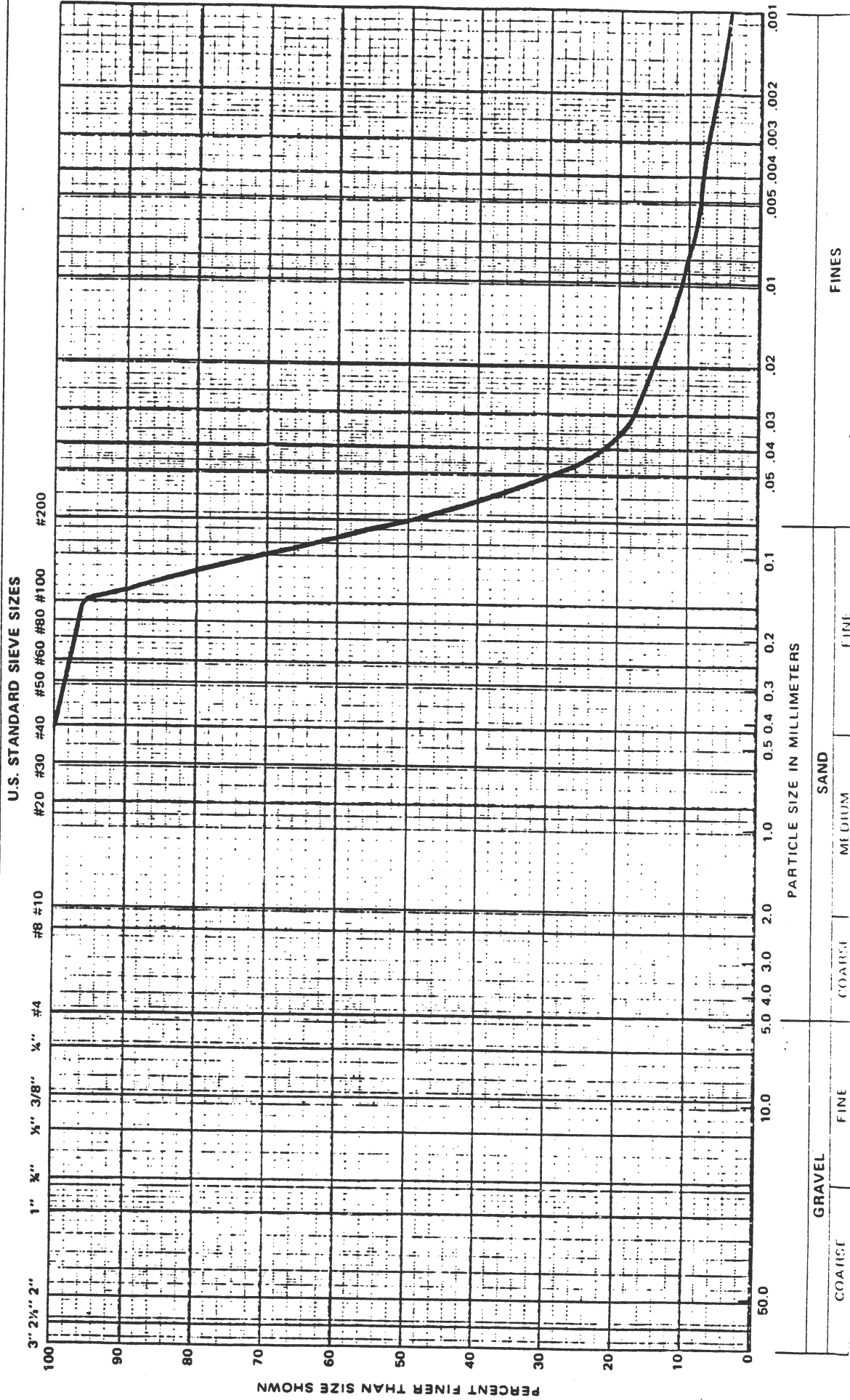
TWIN CITY TESTING
and engineering laboratory, inc.
662 CHOMWELL AVENUE
ST PAUL, MN 55114
PHONE 612/645-3601

Project: SOIL TESTING FOR MDU HESKETT
POWER PLANT - MANDAN, NORTH DAKOTA

Reported To: Water Supply, Inc.

Job No. 52-0688
Sample No. MDU Heskett #4 Depth: 31' -32'
Classification (ASTM: D2487) SM
Description SILTY SAND, fine grained

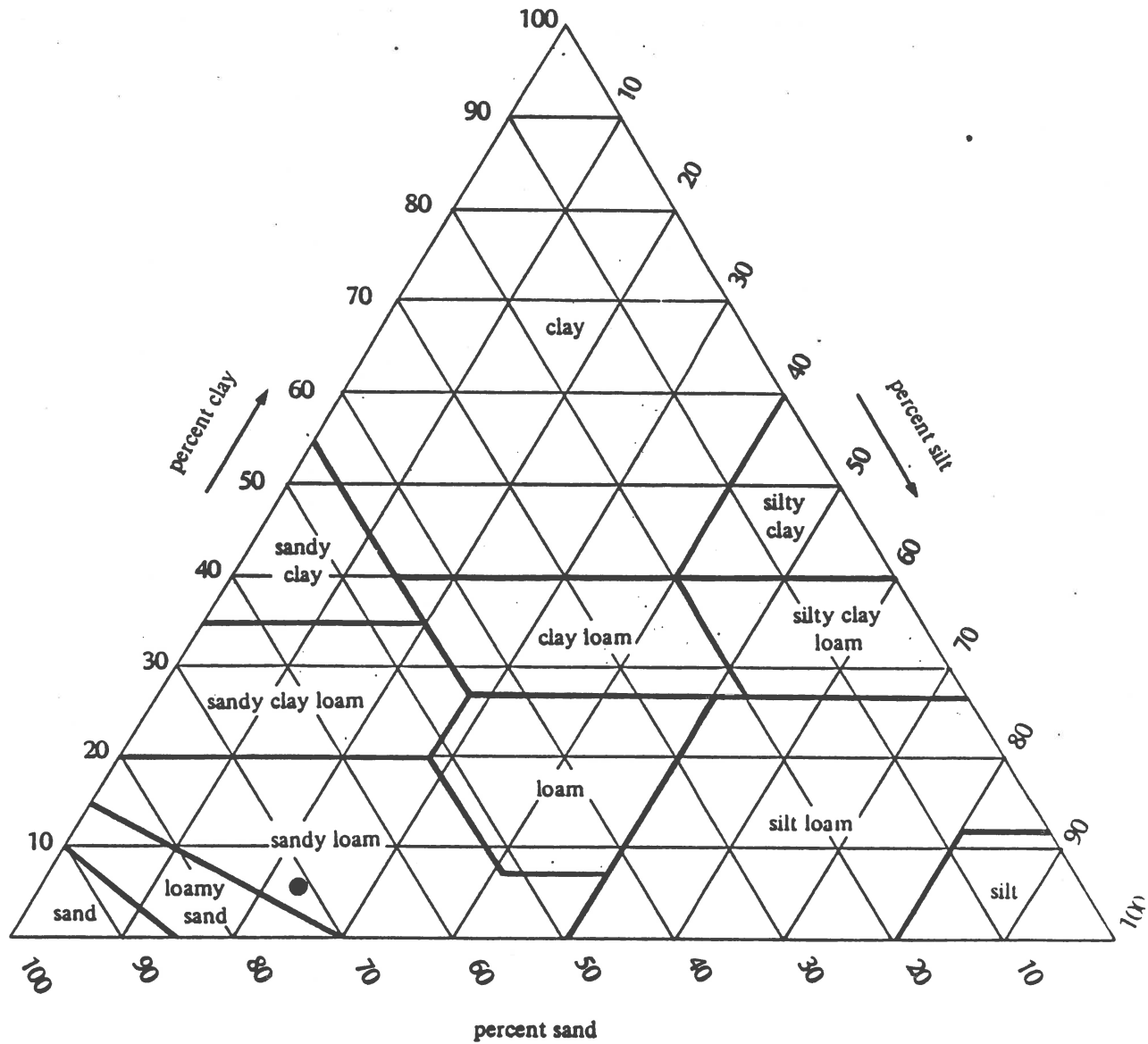
GRAIN SIZE DISTRIBUTION CURVE



PERCENT FINER THAN SIZE SHOWN

USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #4, 31'-32'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

Size Range in Millimeters (Mean Diameter)												
75	2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008	
GRAVEL	SAND					SILT			CLAY			
	Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine	
	10	18	38	60	140	300						
U.S. Standard Sieve Numbers												

TWIN CITY TESTING LAB



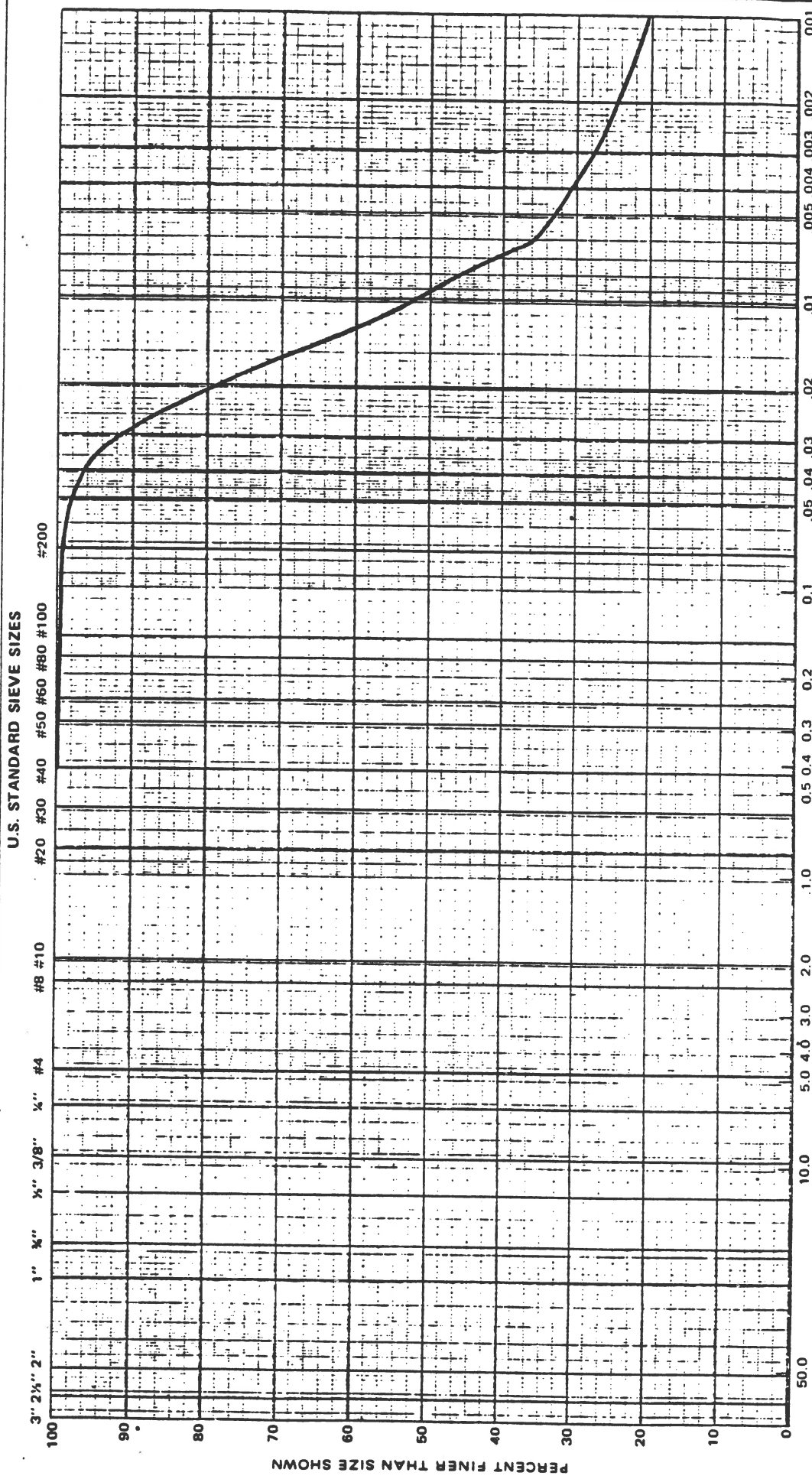
twin city testing
and engineering laboratory, inc.
662 CROMWELL AVENUE
ST PAUL, MN 55114
PHONE 612/645-3601

Project: SOIL TESTING FOR MDU HESKETT
POWER PLANT - MANDAN, NORTH DAKOTA

Reported To: Water Supply, Inc.

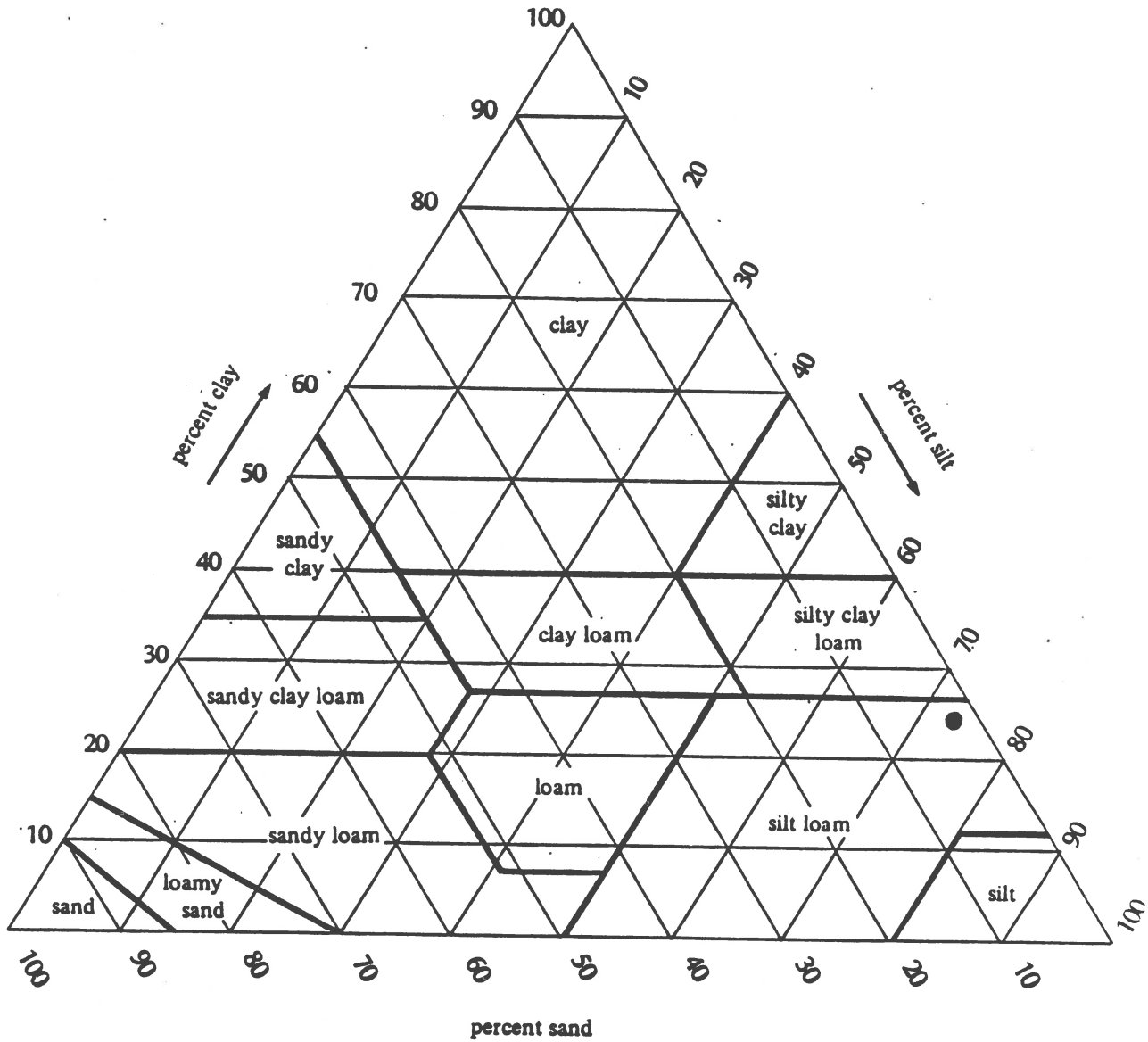
Job No. 52-0688
Sample No. MDU Heskett #4 Depth: 41'-42'
Classification (ASTM:D2487) CH-OH
Description SHALE, (Textural Classification -
tion: Organic Fat Clay)

GRAIN SIZE DISTRIBUTION CURVE



USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #4, 41-42'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

Size Range in Millimeters (Mean Diameter)											
75	2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008
GRAVEL	SAND					SILT			CLAY		
	Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine
	10	18	35	60	140	300					
U.S. Standard Sieve Numbers											

TWIN CITY TESTING LAB



twin city testing
and engineering laboratory, inc.

662 CROMWELL AVENUE
ST PAUL, MN 55114
PHONE 612-645-3501

Job No. 52-0688

Sample No. MDU Heskett #4 Dept. 51'-52'

Classification (ASTM: D2487) CL

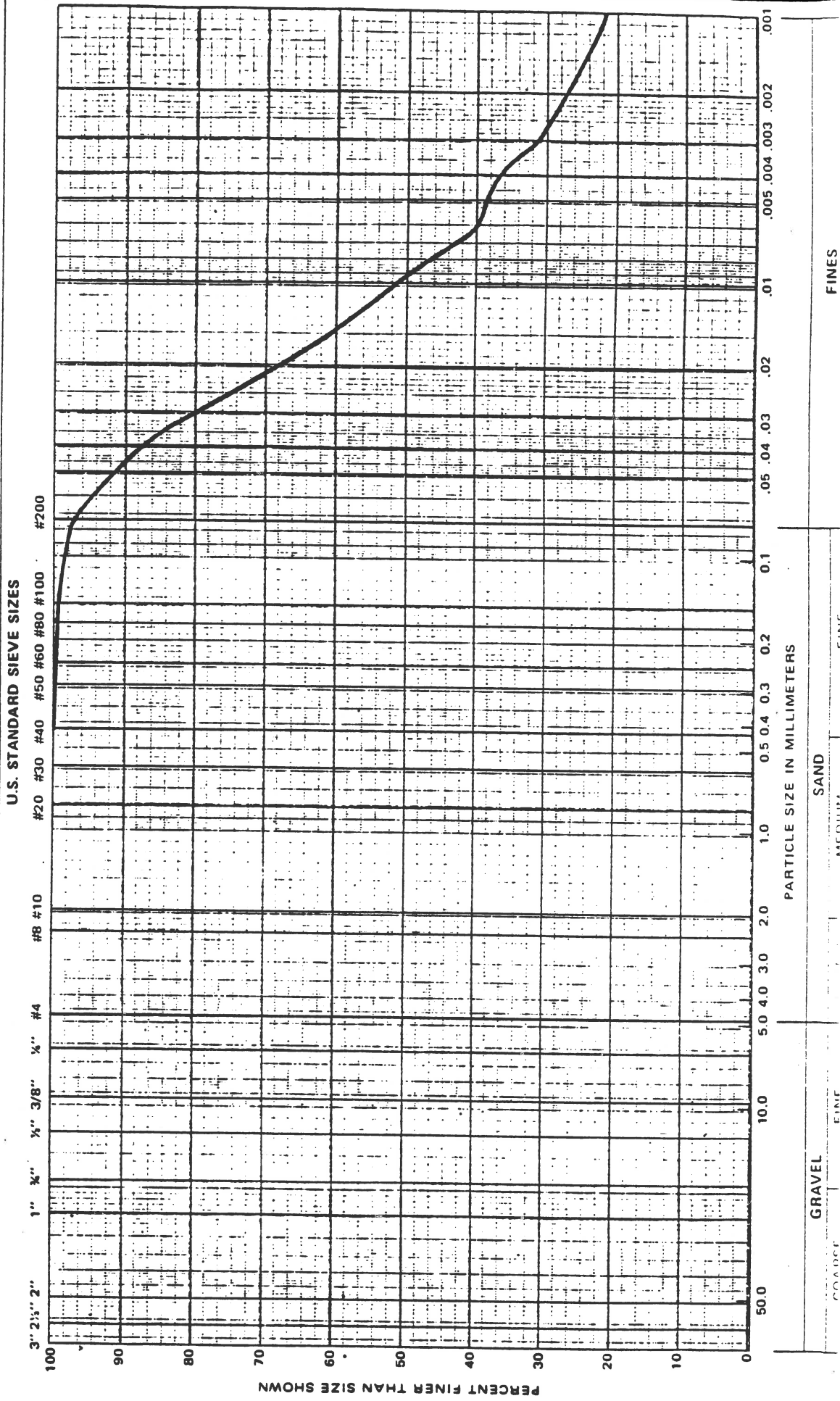
Description SHALE, (Textural Classification: Silty Clay)

Project: SOIL TESTING FOR MDU HESKETT

POWER PLANT - MANDAN, NORTH DAKOTA

Reported To: Water Supply, Inc.

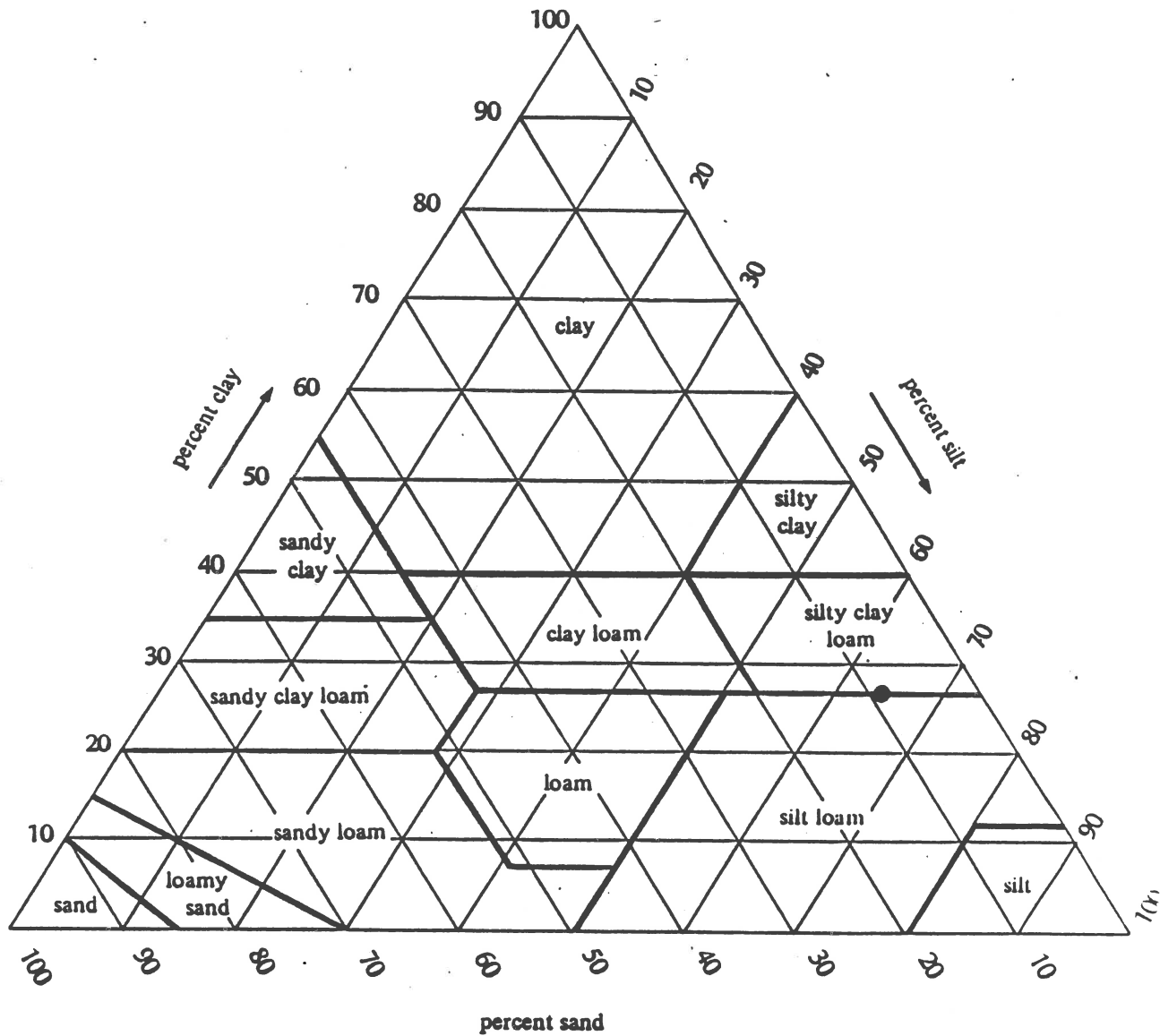
GRAIN SIZE DISTRIBUTION CURVE



PERCENT FINER THAN SIZE SHOWN

USDA SOIL TEXTURAL CLASSIFICATION

MDU HESKETT #4, 51'-52'



COMPARISON OF PARTICLE SIZES IN USDA SYSTEM

		Size Range in Millimeters (Mean Diameter)										
		2	1	0.5	0.25	0.1	0.05	0.02	0.005	0.002	0.0002	0.00008
GRAVEL		SAND					SILT			CLAY		
		Very Coarse	Coarse	Medium	Fine	Very Fine	Coarse	Medium	Fine	Coarse	Medium	Fine
		10	18	35	60	140	300					
		U.S. Standard Sieve Numbers										

TWIN CITY TESTING LAB

6.0 FACILITY CONSTRUCTION, OPERATION AND CLOSURE

6.1 Site Preparation and Construction

6.1.1 Access and Preconstruction

Exhibit 5-F presents soil information on the Heskett site currently available through the Morton County Agricultural Stabilization and Conservation Service office. Because this data was gathered from fieldwork conducted several decades ago and provides little site-specific soil depth information, a new soil survey will be commissioned. The survey will be conducted prior to the onset of construction and cover the entire permit area. Soil profiles will be developed identifying soil types and topsoil (A horizon) and subsoil (B horizon) depths. This information will be used to establish plant growth material (SPGM) salvage and replacement depths during future construction and reclamation activities.

Surface water drainage of adjoining land east of the site will be improved by the permanent installation of a grass-lined ditch (Exhibit 6-B). This drainageway will be located along the base of an existing draw and enhance movement of surface runoff waters and permitted discharges from impoundments located to the south on Amoco Refinery property. The drainageway will be about 8 feet deep, 8 feet wide at the base, and provide a slope of 1% to a discharge at Rock Haven Creek. Existing surface water drainage patterns should not be significantly altered by this installation.

Primary access to the site will be along a dedicated haul road extending eastward to Heskett Station (Exhibit 6-B). Roadbed construction will require 34,500 cy of excess earthen material removed during the excavation of the initial disposal slot. The road surface will be covered with

gravel to allow all weather access to the site. All haulage road construction activities will be performed on Montana-Dakota property and will not interfere with traffic on surrounding public roads.

Other points of access to the site will be restricted by the installation of a lockable personnel fence around the perimeter of the facility. Public access to the site will not be allowed.

6.1.2 Facility Construction

The first phase of the facility described in Exhibit 6-B will be constructed and made operational during the 1989 earthwork construction season. Waste placement will begin upon the completion of the initial waste disposal slot. To minimize impacts to the landscape and reduce potential fugitive dust and leachate generation, new disposal trenches of similar design will be excavated approximately every other year. Filled trenches will be closed and reclaimed concurrently with new trench construction

The 47 acre disposal facility will be developed in two phases. Phase I, comprising the disposal area on the north side of the haul road, will provide about 13 years (approximately 700,000 cy) of disposal capacity. The initial disposal slot will be constructed along the western edge of the Phase I area. Subsequent excavations will proceed eastward until the Phase I area is filled. Phase II of the disposal site lies south of the haul road and will provide disposal capacity for about 15 years (approximately 600,000 cy). Phase II development (Exhibit 6-C) will begin parallel to the southern edge of the haul road and proceed southward. The final trench excavation at the site will lie parallel to the southern edge of the site. It is not currently expected that ash will be placed directly beneath the on-site portion of the

haul road. However, ash emplacement beneath the road may be considered as a contingency if needed.

Exhibit 6-D provides information regarding earth quantity movements for each disposal trench. These estimates (and the subsequent size of the trenches) may be adjusted somewhat if ash waste generation rates markedly differ from projections. The initial slot of Phase I will be constructed to contain slightly over one year of waste (60,000 cy). Subsequent trenches will be constructed to contain all ash generated during the ensuing one to two years.

All construction activities will be performed during the normal earthwork construction season. Equipment such as bulldozers, scrapers, graders, and compactors will remove, modify, and/or replace earthen materials. Most material excavation and relocation operations will rely upon scrapers.

Each trench will have a compacted in-situ clay liner along its base to restrict downward migration of in-pit liquids. Available information (see Exhibits 5-E and 5-K) indicates an abundance of naturally occurring clay and silt which will be uncovered in conjunction with trench excavations. These materials will be scarified to a depth of 18 inches and recompact to a permeability of not more than 1×10^{-7} cm sec⁻¹. Occurrences of sand or gravel will be removed and replaced with clay-rich spoil. In-situ materials providing marginally acceptable rates of permeability will be replaced, treated with a soil liner admixture such as bentonite, or thickened to provide the equivalent permeability of 18 inches of 1×10^{-7} cm sec⁻¹ material. The in-situ liner will cover the entire floor of the trench, the liquids collection sump, and be extended to include the lower five feet of the trench sidewall. Liner installations associated with new trench construction will be keyed into the previous trench liners, thereby providing contiguous liquids

6.1.3 Excavated Materials

The removal and stockpiling of suitable plant growth material (SPGM) will be completed prior to any operation which would interfere with the use and integrity of the top soil. Top soil thickness information provided by the soil survey (see Section 6.1.1) will be used to establish SPGM salvage depth. SPGM will be removed by scraper in two lifts; soil horizon A will be removed in the first lift, soil horizon B will comprise the second lift. Each lift will be separately stockpiled in an area described in the Site Plan of Exhibit 6-B. Because filled trenches will be closed in conjunction with new trench construction, removed SPGM shall be stockpiled only when it is not practical for direct placement in areas concurrently undergoing reclamation.

Exhibit 6-D projects the amount of earthen materials which will be excavated. The largest single Phase I excavation (59,000 cy) will be the initial trench construction. Resulting excess materials from drainage ditch and disposal slot excavation will be used in the construction of the access road, evaporation pond, and a permanent visual obstruction berm along the southern perimeter of the site. Excess spoil may be diverted to the closure of the adjacent Heskett ash pile if available. Because future excavations will generate volumes of materials which approximate requirements for closure (i.e., cap construction and overburden placement) relatively little material should require stockpiling along the western edge of the site. Stockpile Area No. 1 and 2 may be converted into an additional visual obstruction berm if excess spoils require permanent dislocation from the reclamation area.

All temporary SPGM and clay material stockpiles will be maintained in a manner which minimizes the effects of erosion yet maintains soil integrity. Protective measures will be applied and include the planting of cover crops, mulching, use of chemical binders, contour tillage, or other site specific

infiltration protection. Verification of construction quality and attainment of proper rates of permeability will be made by an independent registered professional engineer.

Each trench floor will be positioned to provide at least five feet of separation between the waste and the 1986 water table elevation. Additionally, the base of each slot will be contoured to provide a positive drainage slope of not less than 1% both laterally and lengthwise, thus promoting rapid movement of in-pit liquids away from the waste and into the collection sump.

Exhibit 6-C, Section X-X illustrates a typical cross-section of the leachate collection pipe which will be permanently installed with each new trench. A perforated pipe will gather liquids from the operational and closed portions of the facility and discharge them into the liquids collection sump in use at that time. Liquids will continue to be gathered by the collection line after the closure of Phase I and discharge directly into the evaporation pond. Waste leachates collected by the Phase II line will not discharge into the active sump but rather directly into the evaporation pond.

All liquids collected within the pit sump and leachate collection lines will be evaporated in a 53,000 square foot evaporation pond (Exhibit 6-B, Section D-D). This pond will be constructed to contain in-pit liquids resulting from normally-occurring rainfall plus a single 24 hour 2.5 inch precipitation event. The evaporation pond will have 5 foot side walls and be equipped with a three foot thick clay liner possessing a permeability of not more than 1×10^{-7} cm sec⁻¹. The evaporation pond will service the disposal facility throughout the operational life of the site.

treatments. Annual cover crops may be planted in areas of frequent stockpile disturbance if necessary to control wind and water erosion. Obstructional berms will be permanently reclaimed to native grasses as soon as possible after completion.

6.2 Operation and Management

6.2.1 Waste Placement

Coal combustion ash will be loaded onto trucks and slightly wetted for dust control before transportation to the disposal site via the ash haul road. Haulage will take place daily during daylight hours; only in emergencies will ash haulage occur after nightfall. Spilled waste material on the haul road and at the site will be immediately cleaned-up and placed in the disposal trench. Ash waste will not be temporarily stored at the site prior to disposal.

Haul trucks will enter the trench by way of ramps located at the end of the trench with the highest elevation (Exhibit 6-B, Operational Schematic). Waste will be initially placed in each trench near the ramp and expanded to provide a surface for unloading activities. Vehicular traffic upon the disposal slot floor will be held to a minimum to reduce inadvertent liner damage. Dumped waste will be leveled with a front end loader and spread across the trench floor in lifts 5 to 8 feet thick. The active sump area will not be filled with waste. Ash will not be dumped from the pit highwall into the trench.

Because initial disposal activity will be conducted at an elevation below ground surface the waste will receive only moderate exposure to surface winds. Consequently, little fugitive dust is expected to be generated. As

the waste elevation increases, however, strong surface winds might produce increasing amounts of airborne nuisance particulates. Dust suppression measures will be implemented as required to control fugitive dust. These measures will include the selective placement of AFBC bottom ash (a relatively low dust emitting material) over other ash wastes or the thin spreading of earthen or other dust control material. A 2,500 gallon water spray truck is available for dust control applications over the ash haul road. Water spray will not be used for dust control over the disposed of waste.

Montana-Dakota personnel will perform all daily operational monitoring and disposal activities at the site. Facility points-of-contact are:

Station Superintendent - Duane Steen

Fuel and Grounds Supervisor - Darhl Bowers

Facility Telephone - (701) 663-9576

The Fuel and Grounds Supervisor (or his designee) at Heskett Station will have general supervision of the site and verify that procedures specified in this permit application are adhered to. The site will be monitored daily in conjunction with normal ash haulage activities. Weekly log entries will be made concerning the amount of ash hauled, waste-contaminated water transferences, and unusual operational occurrences such as waste spillages or failures in site reclamation. Corrective actions will also be noted.

6.2.2 Surface Water Management

Ground surface runoff waters will be prevented from entering the pit by either a positive slope away from the edge of the pit or the construction of diversionary trenches or berms. Uncontaminated ground surface runoff waters

will not be controlled at the site except in instances where erosion and/or sedimentation is occurring. Waste spillages at the site and on the haul road will be immediately cleaned-up after each incident; consequently no contaminated waters should be generated in these areas. The ash haul road will be graded to promote surface water run off away from the active disposal area (see Exhibit 6-B, Section b-b and Exhibit 6-C, Section b-b) and into the drainage ditch.

The in-pit sump will hold all meteoric-source precipitation falling within the trench (both waste contacting and non-contacting liquids) and infiltrated water gathered by the leachate collection line (Phase I only). Each collection sump will be sized to provide 100% retention of normal rainfall plus one 2.5 inch precipitation event occurring in a 24-hour period. The sumps will be equipped with an 18 inch compacted clay liner similar in design to the rest of the pit floor. When accumulated liquids approach 3 feet in depth (see Exhibit 6-B, Section X-X), the liquids will be transferred to the evaporation pond. It should be noted that restraints regarding weather, accessibility, equipment or personnel availability may occasionally change the 3 foot liquids volume transfer standard.

Liquid transfer to the evaporation pond will be performed through the use of a portable pump and an overland pipe constructed of PVC or similar material. Pumping activities will normally be conducted during periods of ash haulage and will be continually monitored for leakage during operation. Pumping will not be performed at night or during freezing conditions which could damage the pipe.

Minimal care should be required around the evaporation pond. Surface discharges will not be made from the pond. Growth of vegetation in the impoundment will be controlled through additions of herbicide or mechanical

cutting whenever damage to the clay liner is considered likely. The pond will be monitored monthly for evidence of deterioration and leakage. The groundwater monitoring plan provides for the installation of a water table elevation and quality monitoring well immediately downgradient of the impoundment. Samples of impounded liquids will be taken (if available) semi-annually in conjunction with the groundwater sampling program and analyzed for the same chemical parameters. Surface impoundment analytical data will be combined with the groundwater quality information and submitted to the NDS DH according to the schedule specified in Section 7.3

6.2.3 Contingencies and Potential Impacts

The proposed waste facility was sited and designed to reasonably ensure that groundwater will not intrude upon the waste. Two consecutive years of potentiometric monitoring has shown a relatively stable water table elevation with little apparent seasonal fluctuation. This general stability, even during the severe drought of 1988, might be partially attributable to constant upgradient recharge provided by surface impoundments on Amoco Refinery property to the south. Discussions with Amoco personnel has indicated there are no proposals to expand or otherwise modify this impoundment system.

The facility will be located over a marginal groundwater resource. Groundwater chemical characterizations (Exhibit 5-J) indicate it to be of comparable quality with the waste leachate (Exhibit 2-A). Furthermore, recent studies (referenced in Section 5.2.4) have shown that heavy metals which exist in the leachate (such as arsenic, cadmium, and lead) are effectively attenuated by clay and silt materials which naturally occur in abundance throughout the Heskett Site. The Cannonball Formation water at the Heskett Site is unsuitable for most domestic or agricultural purposes without prior

purification. Area residences rely upon other underlying aquifers such as the Ludlow for their domestic water supplies. Consequently, the proposed facility will not pose a threat to a desirable groundwater resource. Indeed, even major releases of Heskett ash leachate to the underlying groundwater might be expected to result in only minor deviations from normal background chemical makeup.

A number of simple remedial measures are available at the site should groundwater elevations rise to intrude upon the waste, thereby endangering an area resource. Because Rock Haven Creek on the west and north of the site, along with the small draw located to east, already provides natural points of surface discharge to a rising groundwater table, modification to these topographic depressions or the installation of a shallow subsurface drainage system in their vicinity would serve to allow groundwater discharge at a lower elevation. This would serve to permanently lessen the potentiometric level of the water table. Increasing the depth of the drainageway might be particularly appropriate due to its close proximity to the lowest point of waste placement (i.e. the eastern edges of Phases I and II). Another option includes the permanent installation of a subsurface drainage pipe or french drain five to eight feet below the southern edge of the last Phase II trench. Such a system would intercept the groundwater below and upgradient of the waste and divert flow laterally to a discharge point on the drainageway. This would hydraulically isolate the waste.

An in-pit leachate collection system will be constructed to detect and gather in-waste liquids that would occur during the operational life of the site. Significant leachate collections may extend the life of the gathering pipes (and evaporation pond) beyond the site closure date until the problem is remedied. The in-pit sump and evaporation pond will have compacted clay

liners to assure minimal rates of subsurface leachate migration. The evaporation pond will be monitored monthly to determine liquids volume and detect evidence of deterioration, erosion, seepage, or overtopping. The in-pit collection sump will be similarly inspected weekly and after precipitation events. Should a sudden drop occur in the liquids level of the impoundment or groundwater quality monitoring indicate significant leakage is occurring, repair or replacement of the liner with a soil-based or admixed liner will be performed. Similarly, the size of in-pit collection sumps will be expanded in subsequent trench excavations should it become apparent that more retention volume is needed.

Provisions have been made which allow for visual and acoustical obstructions (earthen berms and tree shelter belts) between facility operations and residences to the south. Additional tree plants and berm construction (depending upon materials availability) may be emplaced around the facility perimeter at a future date. Shelter belts or berms will not be placed over waste disposal areas. Decisions regarding these features will be made after the facility becomes operational and their need at a specific location becomes apparent. Dust control measures (as described in Section 6.2.1) will be implemented until these features become permanently established.

6.3 Closure and Reclamation

6.3.1 Closure Methods

As each trench is brought to its final waste elevation, a 1 to 3 inch layer of earthen material will be applied to the waste if fugitive waste dust requires suppression. New trenches will be first constructed adjacent to the

disposal area intended for closure. Excavated materials from the new trench will be used to close the waste filled trench. Excess excavated material may be temporarily stockpiled in the area described in Exhibit 6-B or used in permanent berm construction. Similarly, new trenches providing inadequate volumes of earth for closure work will require withdrawal from stockpiled inventories.

A two-foot thick compacted clay cap will be constructed over the waste (Exhibit 6-C, Sections A-A and B-B). The cap will be developed from clay-rich spoil materials such as those documented in Exhibit 5-K. Earth moving equipment such as bulldozers, scrapers, graders, and compactors will emplace materials so that compaction of approximately 95% of maximum dry density and a permeability of 1×10^{-7} cm sec⁻¹ or less is attained. If available materials cannot provide for a two-foot thickness of 1×10^{-7} cm sec⁻¹ permeability, cap thickness will be increase commensurably and/or treated with an admixture to a point which affords equivalent moisture infiltration protection. Verification of adequate construction quality and permeability will be made by an independent registered professional engineer.

Uncompacted spoil will be immediately spread over the completed clay cap and shaped to prevent surface water ponding. Surface slopes will range from 4% to 10%. Spread depth will be adequate to create a total earthen material profile above the waste (i.e., clay cap, uncompacted spoil, and SPGM) of not less than eight feet.

SPGM will be spread over the spoil material at a uniform depth determined by material availability. The respread will be done in accordance with currently accepted practices and procedures which assure proper interlift adhesion. Compaction of materials will be held to a minimum.

The final Phase II trench closure (thus leading to final site closure) will include the removal of the waste haulage road surface and the evaporation pond. All waste-contaminated material will be placed with the waste in the final disposal trench. Disturbed areas will be shaped to the topography illustrated in the site plan of Exhibit 6-D and reclaimed. The leachate collection lines will be abandoned in-place and will not be monitored or maintained. Points of access to the leachate collection line will be sealed during final closure for purposes of safety. The drainageway will not be modified or restored to original contours during or after final closure of the site unless deemed necessary at the time.

6.3.2 Reclamation

SPGM will be sampled and tested to determine soil nutrient status. Fertilizer application recommendations will be solicited from a soil testing laboratory and utilized in consideration of existing soil properties, topography, seed mix components, and practical experience.

The seedbed will be prepared in a fashion which would promote a stable, self-supporting prairie grassland. Rates for seed mixture will approximate:

<u>Species</u>	<u>Rate (lb/acre)</u>
Western Wheatgrass	6.0
Pubescent Wheatgrass	4.0
Smooth Brome	2.0

Seed implantation will be performed with a seed drill during the first favorable planting period; typically from April 15 through June 7, August 10 through September 15, or after October 20. A straw mulch or cover crop will be applied immediately after seeding to provide temporary erosion control. Reseeding or interseeding will be performed if grass fails to establish over

large areas. Bale dikes, excelsior mats, or other appropriate measures will be utilized for control of significant erosion features.

6.3.3 Post-Closure Surface Care

The Heskett Site will be incrementally reclaimed as individual disposal trenches are filled and closed. Post-closure surface care will continue until five years after final closure of the facility. Reclamation failures at the site would extend the surface care requirement period until such time as the deficiency is permanently corrected.

The post-closure maintenance will begin from the date of vegetation seeding. During the first year, each reclaimed area will be examined monthly and after storm events to:

1. Verify that final contours and drainages are maintained,
2. Ensure that healthy vegetative cover is established, and
3. Maintain proper erosion control measures which may be in-place at the site.

Post-closure inspections will be performed quarterly for the remaining four years of the surface care period. Inspection results and corrective actions will be logged. These records will be summarized into an annual facility status report and forwarded to the NDS DH.

The reclaimed area will resemble a gently sloping hill supporting a typical grassland prairie. The growth of woody species (whose root system might penetrate the underlying clay cap) will be suppressed through cutting or chemical treatment. Montana-Dakota may eventually sell hayland or pasture rights if the integrity and plant growth productivity of the site can be maintained with minimal care. No haying or grazing activities will be allowed

for at least three years following initial vegetation establishment of each reclaimed increment.

Montana-Dakota intends to continue ownership of the site for the foreseeable future. No plans to allow surface disturbance or agricultural utilization (except hayland or pasture usage) of the reclaimed area exist. The current industrial land use zoning classification will be retained.

EXHIBIT 6-A

EXISTING CONDITIONS AND AREA MAPS

EXHIBIT 6-B

PHASE I DEVELOPMENT

EXHIBIT 6-C

PHASE I CLOSURE - PHASE II DEVELOPMENT

EXHIBIT 6-D

FINAL CLOSURE

7.0 GROUNDWATER MONITORING

7.1 Operational Monitoring

Analysis of disposal site groundwater quality and potentiometric surfaces will focus upon the uppermost 15 feet of the Cannonball Formation saturated zone. Because facility expansion will eventually destroy most of the existing site instrumentation positioned for possible water quality monitoring purposes, a new series of monitoring wells will be installed prior to waste placement. Four new wells (3 downgradient, 1 upgradient) will be placed in the approximate areas described in Exhibit 6-B. These wells will be constructed similarly to existing site wells and fitted with a 20 foot screen, the lower 15 feet of which will be positioned below the existing water table. Each well will be lithologically logged during installation.

With the possible exception of infrequent potentiometric level determinations, all other wells existing at the site will not be relied upon for any monitoring functions. These deactivated wells will remain undisturbed until such time as their permanent closure is warranted by facility expansion.

Permanently closed wells will be sealed their entire length with grout or other appropriate material in order to assure that groundwater communication between subsurface strata does not occur along the well casing.

Wells which monitor facility operations will be sampled quarterly for the first year to establish background chemical data. The first quarterly sample will be acquired before waste is placed in the facility. The sampling frequency will thereafter be reduced to a semi-annual basis throughout the remaining operational life of the facility.

Water quality samples will be collected and analyzed by personnel experienced in groundwater characterization protocols. Static water table

elevation measurements will be made in advance of any well disturbances. Wells will be purged by pumping three to five well volumes (or until dry) immediately prior to well sampling. Delays in sampling greater than 24 hours will require re-purging.

All first-year background groundwater samples will be analyzed for water quality parameters specified in Table 7-1. This list of parameters will be reduced to a semi-annual groundwater quality characterization of Table 7-2 constituents subsequent to the completion of the first year collection of background data gathering.

7.2 Post-Closure Monitoring

Annual post-closure groundwater monitoring will continue for 30 years after final closure of the entire facility. Sampling for the first five years of the closure period will be performed on the same wells for the same chemical parameters as is in effect for operational monitoring program at the time of closure (i.e., Table 7-2 constituents).

If, after review of all accumulated operational and five years of post-closure data, no leachate contamination is statistically evident in the groundwater when compared to background levels, the suite of annually-monitored parameters will be reduced to:

pH	Static Water Level
Specific Conductance	Arsenic
Total Dissolved Solids	Boron
Carbonate	Selenium
Bicarbonate	Calcium
Sodium	Lead
Sulfate	Temperature

TABLE 7-1

Background Groundwater Quality Analysis Parameters

Alkalinity, total (as CaCO ₃)	Magnesium (Mg)
Arsenic (As)*	Manganese (Mn)*
Barium (Ba)*	Mercury (Hg)*
Bicarbonate (HCO ₃)	Molybdenum (Mo)*
Boron (B)*	Nitrate (NO ₃)
Cadmium (Cd)*	pH**
Calcium (Ca)	Potassium (K)*
Carbonate (CO ₃)	Selenium (Se)*
Chloride (Cl)	Silver (Ag)*
Chromium, total (Cr)*	Sodium (Na)
Fluorine (F)	Specific Conductance**
Hardness (as CaCO ₃)	Sulfate (SO ₄)
Iron (Fe)*	Temperature**
Lead (Pb)*	Total Dissolved Solids (TDS)

*Analyses only for dissolved metal concentration

**Field determinations

Static water levels will be measured from top-of-pipe.

TABLE 7-2

Operational Groundwater Quality Analysis Parameters

Alkalinity, total (as CaCO ₃)	Molybdenum (Mo)*
Arsenic (As)*	pH**
Bicarbonate (HCO ₃)	Potassium (K)*
Boron (B)*	Selenium (Se)*
Cadmium (Cd)*	Sodium (Na)
Calcium (Ca)	Specific Conductance**
Carbonate (CO ₃)	Sulfate (SO ₄)
Hardness (as CaCO ₃)	Temperature**
Lead (Pb)*	Total Dissolved Solids (TDS)
Magnesium (Mg)	

*Analyses only for dissolved metal concentration

**Field determinations

Static water levels will be measured from top-of-pipe.

Characterization of these groundwater quality indicator parameters will continue for the remaining 25 year post-closure groundwater monitoring period.

7.3 Quality Assurance and Data Management

Montana-Dakota currently relies upon experienced independent contractors to acquire analytical and potentiometric groundwater information. This practice is expected to continue for the foreseeable future. Minimum levels of performance for such contractors will include:

- Use of non-contaminating, non-aerating equipment for all monitoring activities. Equipment other than bailers or submersible diaphragm pumps for purging and sampling must be specifically approved by Montana-Dakota before use. Air-lift pumps may not be used in any circumstance.
- All samples must be conditioned, preserved, and analyzed according to methods and limitations prescribed in Methods for Chemical Analysis of Water and Wastes, EPA-600/4-79-020 (revised March 1983).
- Description of field sampling methods and analytical quality controls will be required of each contractor. Evidence of appropriate laboratory certification and participation in interlaboratory comparison will be requested. Brief resumes of involved personnel must also be provided.
- Cation/anion balances and replicate values for each set of data must be identified on the analysis report.

Montana-Dakota shall annually evaluate accumulated water table elevation and groundwater quality information gathered from site instrumentation by the contractor. Post-closure groundwater data obtained from wells surrounding

the adjacent Heskett ash waste pile (WS-series wells) will also be examined to determine their possible contribution to Heskett Site contamination monitoring. Data evaluation techniques will include chemical constituent comparisons between upgradient and downgradient wells at the same point in time and comparisons of individual wells to their historic background concentrations. A variety of statistical tools will be examined for application against the data base. Goodness-of-fit testing will confirm or deny the existence of normally distributed data. Specific test procedures might include hypothesis testing (t-test), parametric analysis of variance (ANOVA), ANOVA's based upon ranks, and perhaps tolerance intervals. Significance will be established at the 0.05 confidence level.

Operational groundwater monitoring will typically be performed in the second and fourth calendar quarters. Annual post-closure groundwater monitoring will be performed during the second or third quarter. All groundwater sample analysis results, water table surface elevations, and other associated information will be forwarded to the North Dakota State Department of Health within 30 days of its receipt from the independent groundwater sampling contractor. Cumulative statistical data summaries (including descriptions of the statistical methods employed) will be forwarded to the Department annually as they are completed.

8.0 PERMITTING

Upon approval by the North Dakota State Department of Health of the proposed solid waste disposal facility but before the onset of actual disposal activities, a notarized affidavit shall be recorded in the tract system of the Morton County Registrar of Deeds. This affidavit shall specify that the SW1/4 of Section 10, Range 81 West, Township 139 North, has been permitted to receive solid waste for disposal. Another affidavit shall be similarly filed upon final closure of the site which provides information concerning waste types, location, construction, and management. Copies of both instruments shall be forwarded to the North Dakota State Department of Health within 30 days of recording.

Other requirements, as specified by the North Dakota State Department of Health and other regulatory authorities, will be complied with as they become evident.

Upon the beginning of normal operations of the proposed disposal facility all waste placement at the current disposal facility (i.e. the Heskett Ash Pile) will cease. The ash pile will then be closed according to the specifications described in the relevant Special Use Disposal Site permit application (submitted to the North Dakota State Department of Health on March 10, 1986: Solid Waste Permit issuance still pending).



APPLICATION FOR PERMIT TO CONSTRUCT/OPERATE A
SPECIAL USE DISPOSAL SITE
NORTH DAKOTA STATE DEPARTMENT OF HEALTH
SFN 8376 (01/86)

NOTE: Please read the instructions for details on information and documents required to support your application.

PERSON TO BE RESPONSIBLE FOR OPERATION (APPLICANT) Station Manager, Heskett Station				APPLICATION DATE March 1, 1989
ADDRESS OF APPLICANT 400 North Fourth Street, Bismarck, ND 58501				TELEPHONE NUMBER (701) 222-7900
NAME OF SITE Heskett Ash Site	ADDRESS OF SITE Heskett Station, 2 Miles North of Mandan, ND			TELEPHONE NUMBER (701) 663-9576
PROPERTY OWNER Montana-Dakota Utilities	ADDRESS OF PROPERTY OWNER 400 North Fourth St., Bismarck, ND 58501			TELEPHONE NUMBER (701) 222-7900
LEGAL DESCRIPTION OF SITE A Portion of the SW $\frac{1}{4}$	SECTION 10	TOWNSHIP 139N	RANGE 81W	COUNTY Morton
PRESENT ZONING CLASSIFICATION OF SITE Industrial	DOES PRESENT ZONING ALLOW THIS PROPOSED USE? <input checked="" type="checkbox"/> YES <input type="checkbox"/> NO			EXPECTED LIFETIME OF SITE <u>28</u> YEARS

I hereby affirm all information in this application is true and accurate to the best of my knowledge and belief.

Bruce Finsdall

SIGNATURE OF APPLICANT

SEND COMPLETED APPLICATION TO:

NORTH DAKOTA STATE DEPARTMENT OF HEALTH
DIVISION OF HAZARDOUS WASTE MANAGEMENT AND SPECIAL STUDIES
1200 MISSOURI AVENUE, ROOM 302
BOX 5520
BISMARCK, ND 58502-5520

**INSTRUCTIONS FOR COMPLETING AN APPLICATION FOR A
PERMIT TO CONSTRUCT AND/OR OPERATE A SPECIAL USE DISPOSAL SITE**

**APPLICATION AND ALL ACCOMPANYING DOCUMENTS MUST
BE SUBMITTED IN QUADRUPPLICATE**

These instructions are considered to be general guidelines only. More or less data may be required by the Department depending on the waste and on conditions at the specific disposal sites. The information required for a specific site will be determined by a preliminary site evaluation by the Department. This may eliminate the expense of investigations at some sites which are obviously unacceptable. After the required site investigation has been completed by the applicant, further work may be required as deemed necessary by the results of the initial investigation.

Permit applications must be prepared and compiled as one cohesive document that logically presents all information necessary to review a permit. Any modifications or information submitted to the Department subsequent to the initial permit application should be in a format that can be physically incorporated into the formal permit application. The Department reserves the right to reject or return a permit application if it is not complete, or if the information is not presented in an orderly and logical format.

The instructions below address the following required information:

- I. Waste Information
 - II. Location Information
 - III. General Geographic Setting
 - IV. Site Specific Characteristics (Geology and Hydrology)
 - V. Construction Plans and Specifications
 - VI. Groundwater Monitoring
 - VII. Operation and Management Methods
 - VIII. Record Solid Waste Activity with County Registrar of Deeds
 - IX. Closure
-
- I. **WASTE INFORMATION:** For each type of solid waste to be managed, specify (a) amount in tons per day or cubic yards per day, or gallons per day; (b) physical description; and (c) qualitative and quantitative chemical analyses.
 - II. **LOCATION INFORMATION:** Show the facility location on a USGS 7 1/2 minute quadrangle map (scale not less than 1:24,000). Also include a current map or aerial photograph of the area showing existing land use. Aerial

photographs are often available from the Agricultural Stabilization and Conservation Service (ASCS). The map or aerial photograph shall be of sufficient scale to show those man-made and natural features of the area, such as water courses, flood plains, dry runs, wells, roads, and other appropriate details and the general topography of the area.

This section should also address the zoning within a quarter mile of the proposed location and any proposed changes in zoning required for waste disposal activities. The Department may request additional information from the applicant and/or the local zoning authorities regarding the zoning requirements for the site.

III. GENERAL GEOGRAPHIC SETTING: This narrative should be a general description of the site. It should include a general treatment of the geography, climate, soils, vegetation, geology, and groundwater to give an adequate background and foundation for effective presentation of the hydrogeology of the site and adjacent areas. The description should not be more elaborate than is necessary to accomplish this purpose.

IV. SITE SPECIFIC CHARACTERISTICS: (Geology and Hydrology) - This information shall be a detailed, integrated evaluation of the hydrogeologic conditions beneath and adjacent to the proposed site pertinent to the production and migration of refuse leachate, and to the capability for leachate containment and attenuation to acceptable quality before reaching a present or potential water source.

A qualitative and quantitative analysis of the effects of the emplacement of the refuse on the existing hydrologic regime must be addressed. Hydrogeologic data must be based on a systematic investigation utilizing data from borings, piezometers, water wells and other nearby water sources, the chemical characteristics of subsurface waters, and other available information.

After all pertinent information has been obtained, site investigation borings must be properly sealed or grouted in a manner that will prevent cross-contamination or interconnection of formations of strata.

A. TYPE AND EXTENT OF SUBSURFACE MATERIALS: A minimum of one boring is required for each ten (10) acres at the site. Regardless of minimum requirements, the degree of subsurface information obtained must be sufficiently comprehensive to allow the design hydrologist/geologist or engineer to make a detailed evaluation of the hydrologic and geologic properties of the subsurface materials, both at the site and laterally extrapolated, such that a reasonable estimate of the effects of these materials on the containment, migration, and attenuation of the leachate can be made. The site specific details must be incorporated into at least two or three cross-sections showing details on the site's geology, hydrology, and elevation. Any clay-rich soil to be used for compacted clay liners or cap must be accurately identified, located, and analyzed.

Borings used for the cross-sections must extend to a minimum depth of fifty (50) feet below the proposed elevation of the buried refuse, or if pertinent, a sufficient depth into bedrock to

determine its character and hydraulic characteristics. In-situ permeability tests may be necessary to determine the permeability of the formations surrounding and underlying the proposed facility. A lithologic and geophysical log may be required for each boring. The geophysical log may include a gamma-gamma and a gamma-density log.

The placement, construction and design of borings piezometer(s) and/or monitoring well(s) should be coordinated with an appropriate representative of the Department. The complete logs of each boring must be provided as well as the following information.

1. Date of boring
 2. Location of boring
 3. Method of drilling including the circulation technique (air, air-mist, water, mud)
 4. Method of sampling
 5. Diameter of borehole
 6. Elevation at surface of boring, referenced to mean sea level to the nearest 0.1 foot
 7. For monitoring wells, the elevations of the screened interval
 8. Depth and elevation of the water level in the borehole or piezometer
 9. Method of piezometer and/or monitor well completion or method used to seal and abandon borehole, whichever is applicable
- B. MATERIAL CLASSIFICATION AND ANALYSIS: Material samples should be taken by split spoon or shelly tube at depths in the boring operation where the type of material encountered differs from that immediately overlying, or in homogeneous materials, at regular intervals. These samples and any samples of clay-rich soil to be used for clay liners must be classified, tested, and analyzed in a materials testing laboratory and the following data reported:
1. Textural classification (USDA System or Unified System) plotted on the appropriate textural classification.
 2. Particle size distribution curves of representative samples.
 3. Coefficient of permeability - based on field (preferred) and/or laboratory tests.
 4. Ion-exchange capacity of samples and ability to adsorb and "fix" heavy metals. Results should be reported in millequivalents per 100 grams of sample. Most fine textured materials will favor ion-exchange because of their mineralogy,

low permeability and large surface area. Sands and gravels are less effective and hence will permit less attenuation of leachate per unit of flow path, and will allow more rapid rates of travel.

- C. **HYDROLOGY:** The hydrology of the site will dictate its ultimate suitability and the final design of the facility.

The design and operation, if soundly based on hydrogeologic principles, will incorporate one or more of the following: elevating the base of the disposal facility above any existing or potential zones of saturation; utilization of existing natural environment to contain and "treat" the leachate; modification of the natural environment to provide the desired hydrogeologic characteristics to either contain the leachate within the refuse, or to provide attenuation in the resulting hydrologic flow system and; isolate the refuse from the surrounding flow system by the use of a natural or artificially-installed liner, and thence collecting and treating the leachate by an engineered system.

Placement of refuse above the zone of saturation does not preclude all leachate production and resultant groundwater pollution, since precipitation during site operation as well as after site closure may generate leachate.

The hydrogeological factors which must be sufficiently considered include:

1. The permeability of the subsurface materials beneath and surrounding the area to be filled with waste;
2. The rate(s) and direction(s) of groundwater movement;
3. The spatial distribution of the potentiometric surface(s) at the time instrumentation is completed, as well as after the facility is constructed, including the water table and the potentiometric surfaces for aquifers in the vicinity of the site;
4. Any structural features which may affect the flow path for groundwater and/or leachate migration. Facilities proposed for areas underlain by significant lignite seams or for areas where lignite has been mined should include a structural contour map of the base of the lignite seam;
5. The effects of facility construction and the emplacement of the refuse on the existing hydrologic regimen, including consideration of flow-system changes as a result of site disruption, construction, or pumpage from present or potential water sources; and
6. The thickness, composition, and configuration of the final cover of the filled area, as well as the post-reclamation vegetation and its effect on surface water infiltration.

V. **CONSTRUCTION PLANS AND SPECIFICATIONS:** Submit a detailed narrative report with the following:

- A. A detailed topographic map of the existing site, (scale 1" = 200' or larger) using a contour interval of five (5) feet where the relief exceeds twenty (20) feet, and two (2) foot contour intervals where the relief is less than twenty (20) feet. The map should show all buildings, ponds, streams, ditches, utilities, roads, fences, location(s) of boreholes, and any other items of significance.
- B. A second topographic map, matched to the scale of the above map, prepared to completely describe the final construction of the proposed site. This should include the construction of disposal areas of trenches; the development of control features for surface water run-off, run-on, and drainage; any installation for the collection and treatment of leachate; access roads; buildings; utilities; fencing; monitoring wells; topsoil and subsoil stockpiles; cover material stockpiles; liner and clay cap material stockpiles; and all other features of the developed facility.
- C. A soil survey report with appropriate maps and a narrative. This section should describe the types of soils at the site and describe the thickness of the topsoil ("A" horizons) and the subsoil ("B" horizons). A description of how these horizons will be removed, handled, and stockpiled for later respreading during site reclamation must be included in detail. This stockpiled soil material (Suitable Plant Growth Material or SPGM) must be handled, stockpiled, and the piles revegetated in a manner that minimizes erosion and/or contamination of the material. The maps included in the construction plans should identify locations of SPGM stockpiles.
- D. Submit a series of cross-sections or profiles (scale 1" = 200' or larger) of the developed site. These sections should number no less than three (3), but in any case must be adequate to define the three dimensional distribution of materials to a depth of fifty (50) feet below the proposed elevation of refuse.

These profiles should clearly indicate the constructed pits, the geologic strata or lithology surrounding and underlying the disposal facility, the placement of any required side and/or bottom liners, the placement of any surface water sumps, the placement and screened interval of appropriate monitoring wells, the levels of the water table, groundwater flow directions, the proposed sequence of placement and total compacted thickness of each lift of waste, thickness of cover material for each lift, and the slope of the completed landfill with final cover in place. These cross-sections should be in a format that allows permit reviewers to obtain a quick and concise view of the proposed facility.

- E. The construction plans should address the Quality Control and Assurance Procedures to be used during site construction, liner

installation, groundwater monitoring, site operation, and site closure. The Department may require a routine report from the facility on the status of the operation and its construction (especially the liners) and its operation (especially surface water control and dust control). The description of the Quality Control Procedures for liner construction or any other appropriate construction (clay cap, etc.) should be signed by an independent registered engineer. A routine status report could be included with the quarterly groundwater monitoring report.

VI. GROUNDWATER MONITORING: The design of a groundwater monitoring system and the parameters for water analysis should be based on an assessment of the waste analysis, the site's geology and hydrology, the plans for construction, and the facility's method of operation. Items that should be discussed include:

- A. The water level in the boreholes immediately after boring completion and sufficient periodic measurements of the depth to water until stabilization has been attained.
- B. The vertical and horizontal components of the hydraulic gradients; a contour map for each potentiometric surface (data for which may be based on local domestic and industrial wells, and on-site piezometers and boreholes).
- C. The location of one or more up-gradient groundwater quality monitoring well nests and a minimum of two down-gradient groundwater quality monitoring piezometer nests to be located in the expected path(s) of the leachate migration. The location and construction of the piezometers should be in accordance with the hydrogeology of the site as determined by the exploratory program, subject to final approval by the Department.
- D. All monitoring wells must be cased and must be installed in compliance with Chapter 43-35 of the North Dakota Century Code and in compliance with Chapter 33-18-01 of the North Dakota Administrative Code governing water well construction. Monitoring wells must be completed in a manner that maintains the integrity of the borehole and precludes cross-contamination or interconnection of aquifers or geologic strata. The casing must be screened with an appropriately sized factory slotted pipe and packed with clean sand or gravel to allow collection of groundwater samples. The annular space between the well casing and borehole must be properly sealed to prevent contamination of samples and the groundwater.

At the surface, all wells must have a proper apron to prevent surface water infiltration and a protective outer casing to prevent physical damage to the well. The outer casing should include a cap and lock.

The monitoring piezometer should be constructed of non-metallic material, with a two (2) inch or greater inside diameter. Such piezometers will aid in evaluation of the effectiveness of the proposed facility design, and provide an early warning of design malfunction so that timely remedial measures can be initiated.

- E. Background analysis for the following chemical characteristics shall be mandatory for at least one groundwater sample taken from a piezometer installed in the expected flow path(s) of the leachate.

EPA standard procedure shall be used for obtaining, transporting, and analyzing samples. The results of the analysis shall be submitted to the Department before an operating permit can be issued.

CHEMICAL PARAMETERS FOR GROUNDWATER ANALYSIS

1. Total Alkalinity (CaCO_3)
2. Arsenic (AS*)
3. Bicarbonate (HCO_3)
4. Cadmium (Cd)*
5. Calcium (Ca)*
6. Carbonate (CO_3)
7. Chloride (Cl)
8. Total Chromium *
9. Fluoride (F-)
10. Hardness (as calcium carbonate)
11. Iron (Fe)*
12. Lead (pb)*
13. Magnesium (Mg)*
14. Manganese (Mn)*
15. Mercury (Hg)*
16. Nitrate (NO_3)
17. pH
18. Potassium (K)*
19. Sodium (Na)*
20. Specific Conductance**
21. Sulfate (SO_4)
22. Total Dissolved Solids
23. Selenium (Se)*
24. Barium (Ba)*
25. Silver (Ag)*
26. Molybdenum *

* Analyzed for "dissolved" metals. (i.e. samples filtered through an 0.45u membrane filter.

** Reported in micromhos at 25 degrees C.

Additional parameters may be assigned by the Department. These parameters will be determined by the detailed chemical analysis of the waste.

All constituents reported in milligrams per liter (mg/l).

Periodic groundwater samples shall be collected and analyzed by the applicant, or his designated representative, to monitor for alterations in groundwater quality. The frequency of samples and parameters required for analysis will be specified by the Department.

VII. OPERATION AND MANAGEMENT METHODS: The permit application must contain details on the facility's operation and maintenance. This should include in detail:

- A - Personnel
- B - Contingency and emergency plans
- C - Control of access to the site (fence, gates, signs, etc.)
- D - Roads (including maintenance)
- E - Confining disposal to as small an area as possible
- F - Dust control
- G - Spill prevention and cleanup
- H - Storage (if any)
- I - Source and thickness of cover
- J - Frequency of covering
- K - Methods of waste handling and haulage
- L - Leachate (including pit water) and surface water run-on/run-off control, handling, and disposal
- M - Recordkeeping
- N - Development Plans
- O - Quality Assurance and Quality Control

VIII. RECORD OF SOLID WASTE DISPOSAL ACTIVITY WITH THE COUNTY REGISTER OF DEEDS: Prior to onset of disposal activities, the permittee shall record a notarized affidavit with the County Register of Deeds to place a notation in the County's tract system specifying that this solid waste management site, as specified in the legal description, is permitted to accept solid wastes for disposal.

This affidavit shall specify that another affidavit must be recorded upon the facility's final closure.

Upon closure, an additional affidavit shall be recorded, as above, specifying any final details regarding the types of wastes disposed at the site, as well as any final details regarding the site's location, construction, management, etc.

The Department must be provided with a copy of both affidavits certified by the County Register of Deeds in the county in which the disposal site is located, within thirty (30) days of their recorded dates.

IX. CLOSURE: A closure plan must be included which describes in detail the procedures to be followed and the materials and manpower to be used in accomplishing final closure of the disposal facility. Generally, closed sites should have an adequate slope to promote surface water run-off without causing active erosion of the final cover.

The plan should include whatever maps, cross-sections, diagrams, and narrative is necessary to detail such things as:

- A. Schedule or timetable of closure.
- B. Final elevation of disposed wastes.

- C. Equipment necessary to accomplish closure.
- D. Type, volume, and source of cover material.
- E. Construction and placement of clay and/or synthetic cap and any drainage layers.
- F. Final grading/contouring of the facility.
- G. Topsoil replacement.
- H. Seed, fertilizer, and irrigation necessary to establish cover.
- I. Surface water run-off.
- J. Schedule for post-closure groundwater monitoring.
- K. Maintenance of leachate control or collection system.
- L. A short description of the utilization and maintenance of the disposal area after closure. The closed site should be managed in a careful manner that will prevent deterioration of the desired plant community and the low permeability final cover. The closure plan should provide for routine inspection and maintenance of the closed site, including the replanting of vegetation and the replacement of any eroded final cover.

9.0 SUMMARY

A permanent coal combustion ash disposal facility will be constructed north of Mandan, ND adjacent to the R. M. Heskett power station. The disposal site will be incrementally developed to minimize impact upon the landscape and reduce potential for fugitive dust emissions and waste leachate generation. Disposal trenches will be bi-annually constructed and equipped with an in situ clay liner sloping towards an in-pit leachate collection system. Collected leachate will be evaporatively treated in a clay-lined surface impoundment.

Earthen berms and tree plantings will provide visual and acoustical obstructions between facility operations and adjacent dwellings to the south. Additional landscaping may be performed as needed. Filled trenches will be covered with a compacted clay cap along with uncompacted overburden and plant growth materials to a total depth of eight feet. Reclamation will be performed with each disposal trench closure and produce a gently sloping grassland.

The groundwater immediately beneath the site is of poor quality and marginally useful as a domestic or agricultural resource. All waste will be emplaced above the historic water table. Facility operations should not effect local groundwater flow. A monitoring program will be established to characterize deviations in groundwater hydrology and chemistry. Contingencies have been identified in the event of site characterization errors, incompatible facility design, or operational difficulties as outlined in this permit application.

10.0 REFERENCES

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Appendix E 2014-2016 Boring Logs

Project: Heskett Station
 Project No.: 34301012
 Location: Mandan, ND
 Coordinates: Lat: 46.86620° Long: -100.89313°
 Datum:

Surface Elevation:
 Drilling Method: HSA
 Sampling Method: Split Spoon
 Completion Depth: 46.0 ft

Unique Well No.: MW-44 R

Depth, feet	Sample Type & Recovery	Sample No.	Blows/6in.	SOUC	Graphic Log	LITHOLOGIC DESCRIPTION	WELL OR PIEZOMETER CONSTRUCTION DETAIL	Elevation, feet
0						0-1': TOPSOIL (OL/OH): Very Dark Brown (2.5/2 7.5YR); low to medium plasticity; roots, fine to medium grained sand.		
1		1	3-3-5-8.	OL/OH		1-46': SANDY CLAY (CL): Brown (5/4 7.5YR) to Dark Gray (4/1 7.5YR); medium to high plasticity; massive; fine to medium grained sand. Moist: 20% gravel, 30% sand, 50% fines. At 1-5': Gravel sized inclusions. Moist: 10% gravel, 20% sand, 70% fines.	PRO. CASING Diameter: 4" by 4" Type: Steel Interval: 3' up & 3' down RISER CASING Diameter: 2" Type: Schd 40 PVC Interval: Stick up to screen (23') GROUT Type: Cement Interval: 0-0.5' BGS SEAL Type: Bentonite Interval: Chips 0.5-21' BGS SANDPACK Type: Granusil Interval: 21-46' BGS SCREEN Diameter: 2" Type: No. 10 Slot Interval: 23-43' BGS	
2		2	9-9-7-7.			Moist: 0% gravel, 30% sand, 70% fines.		
3		3	7-5-5-7.			Moist: 0% gravel, 20% sand, 80% fines.		
4		4	7-9-11-13.			At 8': Oxidized staining.		
5		5	7-9-12-13.					
6		6	6-7-11-13.					
7		7	7-10-12-14.	CL				
8		8	6-10-14-14.					
9		9	10-10-13-16.			At 20': Interbedded layer of sand.		
10		10	10-10-12-16.	CL		(CL): At 24': Color change to dark brown (3/3 7.5YR). Moist: 0% gravel, 20% sand, 80% fines. At 25': Sand lens.		

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Date Boring Started: 10/20/14
 Date Boring Completed: 10/20/14
 Logged By: JEG3
 Drilling Contractor: Midwest Testing (Terracon)
 Drill Rig:

Remarks: Water encountered at 28.7' BGS in MW-44R while drilling on 10/2014

Additional data may have been collected in the field which is not included on this log.
 Weather:

Project: Heskett Station
 Project No.: 34301012
 Location: Mandan, ND
 Coordinates: Lat: 46.86620° Long: -100.89313°
 Datum: Surface Elevation: Drilling Method: HSA Unique Well No.: MW-44 R
Completion Depth: 46.0 ft Sampling Method: Split Spoon

Depth, feet	Sample Type & Recovery	Sample No.	Blows/6in.	soos	Graphic Log	LITHOLOGIC DESCRIPTION	WELL OR PIEZOMETER CONSTRUCTION DETAIL	Elevation, feet	
30		11	8-12-14-18.	CL		(CL): At 24': Color change to dark brown (3/3 7.5YR). (continued) Wet; 0% gravel, 20% sand, 80% fines. At 30.5': Sand lens. (CL): At 32': Color change to dark gray (4/1 7.5YR).	 PRO. CASING Diameter: 4" by 4" Type: Steel Interval: 3' up & 3' down RISER CASING Diameter: 2" Type: Schd 40 PVC Interval: Stick up to screen (23') GROUT Type: Cement Interval: 0-0.5' BGS SEAL Type: Bentonite Interval: Chips 0.5-21' BGS SANDPACK Type: Granusil Interval: 21-46' BGS SCREEN Diameter: 2" Type: No. 10 Slot Interval: 23-43' BGS		
35		12	8-13-16-27.	CL					
40		13	11-19-25-27.	CL					
45		14	14-18-27-34.	SC		(SC): At 45.8': Clayey Sand (SC), fine to medium grained, low to medium plasticity, dark greenish gray (4/10G Gley 2).			
50									
55									

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Date Boring Started: 10/20/14
 Date Boring Completed: 10/20/14
 Logged By: JEG3
 Drilling Contractor: Midwest Testing (Terracon)
 Drill Rig:

Remarks: Water encountered at 28.7' BGS in MW-44R while drilling on 10/20/14

 Additional data may have been collected in the field which is not included on this log.
 Weather:



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 234 West Century Avenue
 Bismarck, ND 58503
 Telephone: 701-255-5460

LOG OF BORING MW-80 R

SHEET 1 OF 1

Project: Heskett Station
 Project No.: 34301012
 Location: Mandan, ND
 Coordinates: Lat: 46.86789° Long: -100.89320°
 Datum:

Surface Elevation:
 Drilling Method: HSA
 Sampling Method: Split Spoon
 Completion Depth: 27.0 ft

Unique Well No.: MW-80 R

Depth, feet	Sample Type & Recovery	Sample No.	Blows/ft.	so to c	Graphic Log	LITHOLOGIC DESCRIPTION	WELL OR PIEZOMETER CONSTRUCTION DETAIL	Elevation, feet	
0						0-0.5': TOPSOIL (OL/OH): Black; organic roots.			
		1	4-4-4-5.			0.5-27': SANDY CLAY (CL): Brown (4/4 7.5 YR) to Black (2.5/1 7.5YR); medium to high plasticity; fine to medium grained sand. Moist; 0% gravel, 30% sand, 70% fines. At 2': Gravel inclusions.	<p>PRO. CASING Diameter: 4" by 4" Type: Steel Interval: 3' up & 3' down</p> <p>RISER CASING Diameter: 2" Type: Schd 40 PVC Interval: Stick up to screen (7')</p> <p>GROUT Type: Cement Interval: 0-0.5' BGS</p> <p>SEAL Type: Bentonite Interval: Chips 0.5-5' BGS</p> <p>SANDPACK Type: Granusil Interval: 5-27' BGS</p> <p>SCREEN Diameter: 2" Type: No 10 Slot Interval: 7-27' BGS</p>		
		2	4-5-7-9.			Moist; 10% gravel, 30% sand, 60% fines.			
5		3	4-4-5-8.	CL		Moist; 0% gravel, 20% sand, 80% fines.			
		4	4-4-6-6.			(CL): At 8': Color change to 2.5/1 7.5YR black, no odor.			
		5	3-4-5-6.	CL		(CL): At 9': Color change to 2.5/2 7.5YR very dark brown. Moist; 0% gravel, 20% sand, 80% fines.			
10		6	1-3-3-4.	CL		(CL): At 11': Color change to 3/3 7.5YR dark brown. Moist; 0% gravel, 20% sand, 80% fines.			
		7	1-1-2-1.			(CL): At 13': Color change to 4/4 7.5YR brown. Wet; 0% gravel, 20% sand, 80% fines.			
15		8	1-2-2-1.						
20		9	7-11-12-17.	CL		At 21': Thin sand lens less than 0.1" thick. Wet; 0% gravel, 20% sand, 80% fines. At 21.5': Thin sand lens less than 0.1" thick.			
25		10	7-11-17-17.			Wet; 0% gravel, 20% sand, 80% fines. At 26.5': Thin sand lens less than 0.1" thick.			

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Date Boring Started: 10/20/14
 Date Boring Completed: 10/20/14
 Logged By: JEG3
 Drilling Contractor: Midwest Testing (Terracon)
 Drill Rig:

Remarks: Water encountered at 11.8' BGS in MW-80R while drilling on 10/20/14

Additional data may have been collected in the field which is not included on this log.
 Weather:



Barr Engineering Company
 4300 MarketPointe Drive Suite 200
 Minneapolis, MN 55435
 Telephone: 952-832-2600

LOG OF BORING MW-101 DRAFT

SHEET 1 OF 3

Project: R.M. Haskett Station CCR Monitoring Network
 Project No.: 34300014.12
 Location: Mandan, ND
 Coordinates: Lat: 438844.919° Long: 1868647.777°
 Datum: NAD 83

Surface Elevation: 1716.6 ft
 Drilling Method: HSA
 Sampling Method: SPT
 Completion Depth: 58.0 ft

Unique Well No.:

Depth, feet	Sample Type & Recovery	Sample No.	Blows/6in.	S C S C	Graphic Log	LITHOLOGIC DESCRIPTION	WELL OR PIEZOMETER CONSTRUCTION DETAIL	Elevation, feet
0						TOPSOIL: Brown (5/4 7.5YR).		
1		1	4-4-4-6.			SANDY LEAN CLAY WITH GRAVEL (CL): fine to medium grained; Brown (5/3 7.5YR); moist; thinly laminated; some mottling; low plasticity; [Cannonball Formation]. At 2': Start to see gravel inclusions.	PRO. CASING Diameter: 4" Type: Steel pipe Interval: 3.5' ags - 1.5' bgs	1715
2		2	4-6-6-7.			At 4': Oxidized staining.	RISER CASING Diameter: 2" Type: PVC SCH 80 Interval: 2.98' ags - 34' bgs	1710
3		3	7-9-14-16.			At 5': Oxidized staining.		
4		4	8-9-12-15.			At 7': Oxidized staining and white staining.	GROUT Type: Neat cement Interval: 0 - 29' bgs	
5		5	10-15-21-26.				SEAL Type: Bentonite chips Interval: 29 - 32' bgs	
6		6	7-18-24-27.	CL		At 11': Oxidized staining.	SANDPACK Type: Silica 40-70 Interval: 32 - 56' bgs	1705
7		7	8-12-19-23.				SCREEN Diameter: 2"; No.6 slot Type: PVC SCH 80 Interval: 34 - 54' bgs	1700
8		8	8-14-18-23.			At 15': Gypsum. 16-20': No recovery.		
9		9	7-10-13-15.			At 20.5': Gypsum.		
10		10	7-9-13-15.	CL		LEAN CLAY (CL): Dark Brown (3/2 7.5YR); oxidized staining, some mottling; medium to high plasticity; [Cannonball Formation]. At 22': Color change to Brown (4/2 7.5YR).		1695
11						At 24': Interbedded sand, fine grained.		

25
 Date Boring Started: 8/18/15
 Date Boring Completed: 8/19/15
 Logged By: JEG3
 Drilling Contractor: Terracon
 Drill Rig: Rig mounted HSA

Remarks: Hole caved in from 56 - 58' bgs.
 DTW = 36.66' TOR on 9/23/2015 (elev. 1682.87)

Additional data may have been collected in the field which is not included on this log.
 Weather:

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 Minneapolis, MN 55435
 Telephone: 952-832-2600

LOG OF BORING MW-101 DRAFT

SHEET 2 OF 3

Project: R.M. Haskett Station CCR Monitoring Network
 Project No.: 34300014.12
 Location: Mandan, ND
 Coordinates: Lat: 438844.919° Long: 1868647.777°
 Datum: NAD 83

Surface Elevation: 1716.6 ft
 Drilling Method: HSA
 Sampling Method: SPT
 Completion Depth: 58.0 ft

Unique Well No.:

Depth, feet	Sample Type & Recovery	Sample No.	Blows/6in.	S C S C	Graphic Log	LITHOLOGIC DESCRIPTION	WELL OR PIEZOMETER CONSTRUCTION DETAIL	Elevation, feet
25		11	7-11-13-15.			LEAN CLAY (CL): Dark Brown (3/2 7.5YR); oxidized staining, some mottling; medium to high plasticity; [Cannonball Formation]. (continued) At 25' and 25.5': Gypsum.	PRO. CASING Diameter: 4" Type: Steel pipe Interval: 3.5' ags - 1.5' bgs	1690
		12	8-11-15-19.			At 26.5': Gypsum.		RISER CASING Diameter: 2" Type: PVC SCH 80 Interval: 2.98' ags - 34' bgs
		13	8-11-13-15.			At 29.5': Gypsum.	GROUT Type: Neat cement Interval: 0 - 29' bgs	
		14	6-11-14-17.	CL				SEAL Type: Bentonite chips Interval: 29 - 32' bgs
		15	8-13-17-22.			At 33': Gypsum.	SANDPACK Type: Silica 40-70 Interval: 32 - 56' bgs	
		16	8-14-19-21.			At 34.5': Gypsum.		SCREEN Diameter: 2"; No.6 slot Type: PVC SCH 80 Interval: 34 - 54' bgs
		17	11-16-20-27.			At 35.5-36': Color change to Black (2.5/1 7.5YR), turns back to brown.		
		18	9-13-20-25.			FAT CLAY (CH): Black (2.5/1 7.5YR); very stiff; high plasticity; wet at 43'; [Cannonball Formation].		
		19	7-14-23-26.			At 38': Oxidized staining.		
		20	9-16-23-26.	CH		At 41': Oxidized staining.		

Date Boring Started: 8/18/15
 Date Boring Completed: 8/19/15
 Logged By: JEG3
 Drilling Contractor: Terracon
 Drill Rig: Rig mounted HSA

Remarks: Hole caved in from 56 - 58' bgs.
 DTW = 36.66' TOR on 9/23/2015 (elev. 1682.87)

Additional data may have been collected in the field which is not included on this log.
 Weather:

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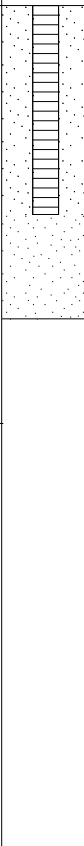
LOG OF BORING MW-101
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SHEET 3 OF 3

Project: R.M. Haskett Station CCR Monitoring Network
 Project No.: 34300014.12
 Location: Mandan, ND
 Coordinates: Lat: 438844.919° Long: 1868647.777°
 Datum: NAD 83

Surface Elevation: 1716.6 ft
 Drilling Method: HSA
 Sampling Method: SPT
 Completion Depth: 58.0 ft

Unique Well No.:

Depth, feet	Sample Type & Recovery	Sample No.	Blows/6in.	S C S C	Graphic Log	LITHOLOGIC DESCRIPTION	WELL OR PIEZOMETER CONSTRUCTION DETAIL	Elevation, feet
50						FAT CLAY (CH): Black (2.5/1 7.5YR); very stiff; high plasticity; wet at 43'; [Cannonball Formation]. (continued)	 <p>PRO. CASING Diameter: 4" Type: Steel pipe Interval: 3.5' ags - 1.5' bgs</p> <p>RISER CASING Diameter: 2" Type: PVC SCH 80 Interval: 2.98' ags - 34' bgs</p> <p>GROUT Type: Neat cement Interval: 0 - 29' bgs</p> <p>SEAL Type: Bentonite chips Interval: 29 - 32' bgs</p> <p>SANDPACK Type: Silica 40-70 Interval: 32 - 56' bgs</p> <p>SCREEN Diameter: 2"; No.6 slot Type: PVC SCH 80 Interval: 34 - 54' bgs</p>	1665
55								1660
60						End of boring 58.0 feet		
65								
70								
75								

Date Boring Started: 8/18/15
 Date Boring Completed: 8/19/15
 Logged By: JEG3
 Drilling Contractor: Terracon
 Drill Rig: Rig mounted HSA

Remarks: Hole caved in from 56 - 58' bgs.
 DTW = 36.66' TOR on 9/23/2015 (elev. 1682.87)

Additional data may have been collected in the field which is not included on this log.
 Weather:

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LOG OF BORING MW-102 DRAFT

SHEET 1 OF 2

Project: R.M. Haskett Station CCR Monitoring Network
 Project No.: 34300014.12
 Location: Mandan, ND
 Coordinates: Lat: 438161.145° Long: 1868782.871°
 Datum: NAD 83

Surface Elevation: 1703.8 ft
 Drilling Method: HSA
 Sampling Method: SPT
 Completion Depth: 46.0 ft

Unique Well No.:

Depth, feet	Sample Type & Recovery	Sample No.	Blows/6in.	SCUC	Graphic Log	LITHOLOGIC DESCRIPTION	WELL OR PIEZOMETER CONSTRUCTION DETAIL	Elevation, feet
0						TOPSOIL: Brown (5/4 7.5YR).		
1		1	3-3-3-2.			LEAN CLAY (CL): medium grained; Brown (4/3 7.5YR); moist; low to medium plasticity; with gravel to 4"; [Cannonball Formation].	PRO. CASING Diameter: 4" Type: Steel pipe Interval: 3.5' ags - 1.5' bgs RISER CASING Diameter: 2" Type: PVC SCH 80 Interval: 2.85' ags - 10' bgs GROUT Type: None Interval: None	1700
2		2	3-2-2-3.					
3		3	3-3-4-5.	CL				
4		4	3-4-5-7.					
5		5	4-8-7-4.	ML		SANDY SILT WITH GRAVEL (ML): Strong Brown (5/6 7.5YR); fine to coarse sand, fine to medium gravel, unconsolidated; [Cannonball Formation].		1695
6		6	4-3-5-9.	CL		LEAN CLAY WITH GRAVEL (CL): fine to medium grained; Brown (5/3 7.5YR); some mottling; medium plasticity; [Cannonball Formation].	SEAL Type: Bentonite chips Interval: 0 - 8' bgs	
7		7	3-5-7-9.			LEAN CLAY (CL): Dark Brown (3/2 7.5YR); medium to high plasticity; [Cannonball Formation].	SANDPACK Type: Silica 40-70 Interval: 8 - 31' bgs	1690
8		8	6-8-12-14.				SCREEN Diameter: 2"; No.6 slot Type: PVC SCH 80 Interval: 20 - 30' bgs	1685
9		9	6-10-12-16.					
10		10	5-9-14-16.	CL				
11		11	5-12-15-18.					
12		12	9-15-18-22.			At 21': Color changes to Black (2.5/1).		1680

Date Boring Started: 8/18/15
 Date Boring Completed: 8/18/15
 Logged By: JEG3
 Drilling Contractor: Terracon
 Drill Rig: Rig mounted HSA

Remarks: Lithological descriptions for a hole that was abandoned. Monitoring well blind drilled and installed next to abandoned hole.
 DTW = 17.09' TOR on 8/21/2015 (elev. 1689.51)

Additional data may have been collected in the field which is not included on this log.
 Weather:

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 Telephone: 952-832-2600

LOG OF BORING MW-102
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SHEET 2 OF 2

Project: R.M. Haskett Station CCR Monitoring Network
 Project No.: 34300014.12
 Location: Mandan, ND
 Coordinates: Lat: 438161.145° Long: 1868782.871°
 Datum: NAD 83

Surface Elevation: 1703.8 ft
 Drilling Method: HSA
 Sampling Method: SPT
 Completion Depth: 46.0 ft

Unique Well No.:

Depth, feet	Sample Type & Recovery	Sample No.	Blows/6in.	SPT	Graphic Log	LITHOLOGIC DESCRIPTION	WELL OR PIEZOMETER CONSTRUCTION DETAIL	Elevation, feet
25		13	9-14-19-22.			LEAN CLAY (CL): Dark Brown (3/2 7.5YR); medium to high plasticity; [Cannonball Formation]. (continued)	 PRO. CASING Diameter: 4" Type: Steel pipe Interval: 3.5' ags - 1.5' bgs RISER CASING Diameter: 2" Type: PVC SCH 80 Interval: 2.85' ags - 10' bgs GROUT Type: None Interval: None SEAL Type: Bentonite chips Interval: 0 - 8' bgs SANDPACK Type: Silica 40-70 Interval: 8 - 31' bgs SCREEN Diameter: 2"; No.6 slot Type: PVC SCH 80 Interval: 20 - 30' bgs	1675
		14	10-17-18-24.			At 29': Gypsum.		
		15	6-15-18-26.			At 33.5' and 34': Gypsum.		
30		16	7-14-18-22.					
		17	11-16-20-27.					
		18	10-14-15-24.					
35		19	13-19-25-35.					
		20	8-17-26-31.					
		21	10-20-27-38.					
		22	13-20-27-37.					
45		23	15-27-27-32.			SILTY SAND (SM): fine to medium grained; Dark Gray (4/1 7.5YR); wet; [Cannonball Formation].	1660	
						End of boring 46.0 feet		

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Date Boring Started: 8/18/15
 Date Boring Completed: 8/18/15
 Logged By: JEG3
 Drilling Contractor: Terracon
 Drill Rig: Rig mounted HSA

Remarks: Lithological descriptions for a hole that was abandoned. Monitoring well blind drilled and installed next to abandoned hole.
 DTW = 17.09' TOR on 8/21/2015 (elev. 1689.51)

Additional data may have been collected in the field which is not included on this log.
 Weather:



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 Minneapolis, MN 55435
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LOG OF BORING MW-103 DRAFT

SHEET 1 OF 2

Project: R.M. Haskett Station CCR Monitoring Network
 Project No.: 34300014.12
 Location: Mandan, ND
 Coordinates: Lat: 437578.205° Long: 1869355.992°
 Datum: NAD 83

Surface Elevation: 1714.7 ft
 Drilling Method: HSA
 Sampling Method: SPT
 Completion Depth: 44.0 ft

Unique Well No.:

Depth, feet	Sample Type & Recovery	Sample No.	Blows/6in.	S C S U	Graphic Log	LITHOLOGIC DESCRIPTION	WELL OR PIEZOMETER CONSTRUCTION DETAIL	Elevation, feet
0						TOPSOIL (OL/OH): Brown (5/4 7.5YR).		
1		1	3-4-5-5.		OL/OH	LEAN CLAY (CL): Very Dark Gray (3/1 7.5YR); moist; stiff; medium to high plasticity; [Cannonball Formation].	PRO. CASING Diameter: 4" Type: Steel pipe Interval: 3.5' ags - 1.5' bgs	1710
2		2	5-5-8-8.		CL			
3		3	5-8-10-11.		CL	POORLY GRADED SAND WITH GRAVEL (SP): fine to coarse grained; Brown (5/4 7.5YR); some oxidized staining, some mottling; [Cannonball Formation].	RISER CASING Diameter: 2" Type: PVC SCH 80 Interval: 2.79' ags - 24' bgs	1705
4		4	6-9-15-15.		SP			
5		5	5-6-5-4.		SP	POORLY GRADED SAND WITH SILT (SP-SM): fine to medium grained; Brown (5/4 7.5YR); [Cannonball Formation].	GROUT Type: Neat cement Interval: 0 - 19' bgs	1700
6		6	4-5-5-7.		SP-SM			
7		7	2-2-2-3.		SP-SM	NO RECOVERY (16 - 20').	SEAL Type: Bentonite chips Interval: 19 - 22' bgs	1695
8		8	3-3-3-3.		SP-SM			
9		9	3-3-5-5.		CL	SANDY LEAN CLAY (CL): fine to medium grained; Light Brown (6/4 7.5YR); wet; some mottling and oxidized staining, cohesive; low to medium plasticity; [Cannonball Formation].	SANDPACK Type: Silica 40-70 Interval: 22 - 44' bgs	1690
10								
15								
20								
25								

Date Boring Started: 8/19/15
 Date Boring Completed: 8/20/15
 Logged By: JEG3
 Drilling Contractor: Terracon
 Drill Rig: Rig mounted HSA

Remarks: DTW = 33.24' TOR on 8/20/2015 (elev. 1684.29)
 Additional data may have been collected in the field which is not included on this log.
 Weather:

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LOG OF BORING MW-103 DRAFT

SHEET 2 OF 2

Project: R.M. Haskett Station CCR Monitoring Network
 Project No.: 34300014.12
 Location: Mandan, ND
 Coordinates: Lat: 437578.205° Long: 1869355.992°
 Datum: NAD 83

Surface Elevation: 1714.7 ft
 Drilling Method: HSA
 Sampling Method: SPT
 Completion Depth: 44.0 ft

Unique Well No.:

Depth, feet	Sample Type & Recovery	Sample No.	Blows/6in.	S C S C	Graphic Log	LITHOLOGIC DESCRIPTION	WELL OR PIEZOMETER CONSTRUCTION DETAIL	Elevation, feet
25		10	2-2-4-4.	CL		SANDY LEAN CLAY (CL): fine to medium grained; Light Brown (6/4 7.5YR); wet; some mottling and oxidized staining, cohesive; low to medium plasticity; [Cannonball Formation]. <i>(continued)</i>	PRO. CASING Diameter: 4" Type: Steel pipe Interval: 3.5' ags - 1.5' bgs RISER CASING Diameter: 2" Type: PVC SCH 80 Interval: 2.79' ags - 24' bgs GROUT Type: Neat cement Interval: 0 - 19' bgs SEAL Type: Bentonite chips Interval: 19 - 22' bgs SANDPACK Type: Silica 40-70 Interval: 22 - 44' bgs SCREEN Diameter: 2"; No.6 slot Type: PVC SCH 80 Interval: 24 - 44' bgs	1685
30		11	10-10-7-9.	SM		SILTY SAND WITH GRAVEL (SM): wet; [Cannonball Formation].		
		12	8-15-17-22.			LEAN CLAY (CL): Brown (4/4 7.5YR); moist; oxidized staining; medium to high plasticity; [Cannonball Formation]. At 32.5': Sand lens, color changes to Black (2.5/1 7.5YR). At 33.5': Sand lens. At 34': Interbedded sand with oxidized staining.		
35		13	7-19-15-25.					1680
		14	11-16-21-50 for 5".	CL		At 36.5': Sand lens. At 37': Sand lens. At 37.5': Color change to Gray (5/1 7.5YR). At 38-38.5': 6" thick layer of hard material.		
40		15	50 for 2"-.					
		16	12-17-22-30.					
		17	9-18-24-50.			At 42-42.5': Silt layer.		
						At 43.5-44': Silt layer.		
45						End of boring 44.0 feet		

Date Boring Started: 8/19/15
 Date Boring Completed: 8/20/15
 Logged By: JEG3
 Drilling Contractor: Terracon
 Drill Rig: Rig mounted HSA

Remarks: DTW = 33.24' TOR on 8/20/2015 (elev. 1684.29)

Additional data may have been collected in the field which is not included on this log.
 Weather:

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 Minneapolis, MN 55435
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LOG OF BORING MW-104 DRAFT

SHEET 1 OF 2

Project: R.M. Haskett Station CCR Monitoring Network
 Project No.: 34300014.12
 Location: Mandan, ND
 Coordinates: Lat: 438853.542° Long: 1869832.72°
 Datum: NAD 83

Surface Elevation: 1681.5 ft
 Drilling Method: HSA
 Sampling Method: SPT
 Completion Depth: 32.0 ft

Unique Well No.:

Depth, feet	Sample Type & Recovery	Sample No.	Blows/6in.	S C S C	Graphic Log	LITHOLOGIC DESCRIPTION	WELL OR PIEZOMETER CONSTRUCTION DETAIL	Elevation, feet
0						TOPSOIL: Brown (5/4 7.5YR).		
1		1	4-5-5-5.			LEAN CLAY WITH SAND (CL): fine to medium grained; Brown (5/4 7.5YR); moist; gravel; medium plasticity; [Cannonball Formation].	PRO. CASING Diameter: 4" Type: Steel pipe Interval: 3.5' ags - 1.5' bgs	1680
2		2	3-5-6-8.	CL				
3		3	3-7-9-10.			LEAN CLAY (CL): Brown (4/4 7.5YR); oxidized staining and mottling; medium to high plasticity; with gypsum throughout; [Cannonball Formation].	RISER CASING Diameter: 2" Type: PVC SCH 80 Interval: 3.06' ags - 9' bgs	1675
4		4	5-7-9-10.					
5		5	5-9-9-10.					
6		6	5-7-9-10.	CL			GROUT Type: None Interval: None	
7		7	5-8-8-12.			At 12': Heavily oxidized.		
8		8	5-9-11-15.			At 15': Start seeing black staining.	SEAL Type: Bentonite chips Interval: 0 - 7' bgs	1670
9		9	6-9-11-13.			At 17': Heavily oxidized.		
10		10	4-7-16-19.			SILTY SAND (SM): Strong Brown (5/6 7.5YR); wet; [Cannonball Formation].	SANDPACK Type: Silica 40-70 Interval: 7 - 32' bgs	
11		11	5-16-22-26.	SM		At 19.5': Color change to Brown (5/4 7.5YR). At 21': Oxidized layer.		
12		12	7-11-14-16.			FAT CLAY (CH): Dark Gray (4/1 7.5YR); moist; stiff; high plasticity; with interbedded sand layers below 27'; [Cannonball Formation].		
13							SCREEN Diameter: 2"; No. 6 slot Type: PVC SCH 80 Interval: 9 - 29' bgs	1665
14								
15								1660
16								
17								
18								
19								
20								
21								
22								
23								
24								
25								

Date Boring Started: 8/20/15
 Date Boring Completed: 8/20/15
 Logged By: JEG3
 Drilling Contractor: Terracon
 Drill Rig: Rig mounted HSA

Remarks: DTW = 13.25' TOR on 8/21/2015 (elev. 1671.26)

Additional data may have been collected in the field which is not included on this log.
 Weather:

M:\GINT\PROJECTS\34300014.GPJ_BARR\LIBRARY.GLB_ENVIRO LOG_BARR TEMPLATE.GDT



Barr Engineering Company
 4300 MarketPointe Drive Suite 200
 Minneapolis, MN 55435
 Telephone: 952-832-2600

LOG OF BORING MW-104
DRAFT

SHEET 2 OF 2

Project: R.M. Haskett Station CCR Monitoring Network
 Project No.: 34300014.12
 Location: Mandan, ND
 Coordinates: Lat: 438853.542° Long: 1869832.72°
 Datum: NAD 83

Surface Elevation: 1681.5 ft
 Drilling Method: HSA
 Sampling Method: SPT
 Completion Depth: 32.0 ft

Unique Well No.:

Depth, feet	Sample Type & Recovery	Sample No.	Blows/6in.	S C S C	Graphic Log	LITHOLOGIC DESCRIPTION	WELL OR PIEZOMETER CONSTRUCTION DETAIL	Elevation, feet	
25		13	6-12-16-17.			FAT CLAY (CH): Dark Gray (4/1 7.5YR); moist; stiff; high plasticity; with interbedded sand layers below 27'; [Cannonball Formation]. (continued)	 PRO. CASING Diameter: 4" Type: Steel pipe Interval: 3.5' ags - 1.5' bgs RISER CASING Diameter: 2" Type: PVC SCH 80 Interval: 3.06' ags - 9' bgs GROUT Type: None Interval: None SEAL Type: Bentonite chips Interval: 0 - 7' bgs SANDPACK Type: Silica 40-70 Interval: 7 - 32' bgs SCREEN Diameter: 2"; No.6 slot Type: PVC SCH 80 Interval: 9 - 29' bgs	1655	
		14	8-12-16-21.	CH					
		15	8-12-16-20.						
30		16				Driller notes: sluff.		1650	
						End of boring 32.0 feet			

Date Boring Started: 8/20/15
 Date Boring Completed: 8/20/15
 Logged By: JEG3
 Drilling Contractor: Terracon
 Drill Rig: Rig mounted HSA

Remarks: DTW = 13.25' TOR on 8/21/2015 (elev. 1671.26)

 Additional data may have been collected in the field which is not included on this log.
 Weather:

M:\GINT\PROJECTS\34300014.GPJ_BARR\LIBRARY.GLB_ENVIRO LOG_BARR TEMPLATE.GDT



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 Minneapolis, MN 55435
 Telephone: 952-832-2600

LOG OF BORING MW-105 DRAFT

SHEET 1 OF 2

Project: R.M. Haskett Station CCR Monitoring Network
 Project No.: 34300014.12
 Location: Mandan, ND
 Coordinates: Lat: 438042.079° Long: 1870325.657°
 Datum: NAD 83

Surface Elevation: 1686.0 ft
 Drilling Method: HSA
 Sampling Method: SPT
 Completion Depth: 30.0 ft

Unique Well No.:

Depth, feet	Sample Type & Recovery	Sample No.	Blows/6in.	SCSU	Graphic Log	LITHOLOGIC DESCRIPTION	WELL OR PIEZOMETER CONSTRUCTION DETAIL	Elevation, feet
0						TOPSOIL: Brown (5/4 7.5YR).		
1		1	6-7-6-5.			SANDY LEAN CLAY (CL): fine to medium grained; Brown (4/2 7.5YR); moist; gravel; medium plasticity; [Cannonball Formation].	PRO. CASING Diameter: 4" Type: Steel pipe Interval: 3.5' ags - 1.5' bgs RISER CASING Diameter: 2" Type: PVC SCH 80 Interval: 3.16' ags - 10' bgs	1685
2		2	5-5-5-6.					
3		3	3-2-4-5.	CL				
4		4	2-2-2-3.					
5						LEAN CLAY (CL): Brown (4/2 7.5YR); soft; high plasticity; wet at 16"; [Cannonball Formation].	GROUT Type: None Interval: None SEAL Type: Bentonite chips Interval: 0 - 7' bgs	1680
6		5	2-1-2-2.					
7		6	2-1-2-1.		At 10.5': Color change to Reddish-Yellow (6/6 7.5YR).			
8		7	2-1-1-3.			At 14.5-15.5': Gravel inclusions. At 15.5': Color change to Brown (4/3 7.5YR).	SANDPACK Type: Silica 40-70 Interval: 7 - 30' bgs	1675
9		8	4-3-5-5.	CL				
10						At 18': Color change to Brown (5/3 7.5YR).	SCREEN Diameter: 2"; No.6 slot Type: PVC SCH 80 Interval: 10 - 30' bgs	1670
11		9	7-9-11-13.					
12		10	7-9-11-13.					
13						POORLY GRADED SAND WITH SILT (SP-SM): medium to coarse grained; Brown (5/4 7.5YR); [Cannonball Formation].		1665
14		11	7-9-13-15.					
15		12	19-26-28-30.	SP-SM				

25
 Date Boring Started: 8/17/15
 Date Boring Completed: 8/17/15
 Logged By: JEG3
 Drilling Contractor: Terracon
 Drill Rig: Rig mounted HSA

Remarks: DTW = 13.22' TOR on 8/21/2015 (elev. 1675.92)

Additional data may have been collected in the field which is not included on this log.
 Weather:

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 4300 MarketPointe Drive Suite 200
 Minneapolis, MN 55435
 Telephone: 952-832-2600

LOG OF BORING MW-105
DRAFT

SHEET 2 OF 2

Project: R.M. Haskett Station CCR Monitoring Network
 Project No.: 34300014.12
 Location: Mandan, ND
 Coordinates: Lat: 438042.079° Long: 1870325.657°
 Datum: NAD 83

Surface Elevation: 1686.0 ft
 Drilling Method: HSA
 Sampling Method: SPT
 Completion Depth: 30.0 ft

Unique Well No.:

Depth, feet	Sample Type & Recovery	Sample No.	Blows/6in.	S C S C	Graphic Log	LITHOLOGIC DESCRIPTION	WELL OR PIEZOMETER CONSTRUCTION DETAIL	Elevation, feet
25		13	15-25-31-40.			FAT CLAY (CL): Dark Brown (3/4 7.5YR); high plasticity; sand lens at 26.5'; [Cannonball Formation]. At 26': Color change to Gray (5/1 7.5YR).		1660
		14	10-15-18-30.	CL				
		15	11-16-22-32.					
30						End of boring 30.0 feet	<p>RISER CASING Diameter: 2" Type: PVC SCH 80 Interval: 3.16' ags - 10' bgs</p> <p>GROUT Type: None Interval: None</p> <p>SEAL Type: Bentonite chips Interval: 0 - 7' bgs</p> <p>SANDPACK Type: Silica 40-70 Interval: 7 - 30' bgs</p> <p>SCREEN Diameter: 2"; No.6 slot Type: PVC SCH 80 Interval: 10 - 30' bgs</p>	

Date Boring Started: 8/17/15
 Date Boring Completed: 8/17/15
 Logged By: JEG3
 Drilling Contractor: Terracon
 Drill Rig: Rig mounted HSA

Remarks: DTW = 13.22' TOR on 8/21/2015 (elev. 1675.92)

Additional data may have been collected in the field which is not included on this log.
 Weather:

M:\GINT\PROJECTS\34300014.GPJ_BARR\LIBRARY.GLB_ENVIRO LOG_BARR TEMPLATE.GDT

**Alternative Source Demonstration:
April 2018 Event**

R.M. Heskett Station

Prepared for
Montana-Dakota Utilities Co.

December 2018



Alternative Source Demonstration: April 2018 Event

R.M. Heskett Station

Prepared for
Montana-Dakota Utilities Co.

December 2018

Alternative Source Demonstration
April 2018 Event

December 2018

Contents

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- Figure 2 Piper Plot

List of Attachments

- Attachment 1 2011 Ash SPLP Laboratory Report

Certifications

I hereby certify that I, or my agent, have examined this written demonstration and attest that this Coal Combustion Residuals Facility Alternative Source Demonstration (ASD) is accurate and has been prepared in accordance with good engineering practice, including consideration of applicable industry standards and the requirements of 40 CFR §257.94. I further certify that this report was prepared by me or under my direct supervision and that I am a duly Licensed Professional Engineer under the laws of the state of North Dakota.

Revision	Date	Summary of Revisions
0	December 20, 2018	Initial Alternative Source Demonstration



Thomas J. Radue, P.E.
Barr Engineering Co.
ND Registration Number PE – 3632

1.0 Introduction

Montana-Dakota Utilities Co. (MDU) owns and operates R.M. Heskett Station (Site), a coal-fired generating station and a gas-fired turbine located in Mandan, North Dakota (Figure 1). One CCR (coal combustion residual) unit, as defined by 40 CFR 257.53, is located on the property. The CCR unit contains coal combustion by-products, asbestos wastes generated from construction activity associated with MDU-owned facilities, and ash derived from burning of tire-derived fuel (TDF) at the facility.

The CCR Rule (US EPA, 2015) §257.94(e)(2) allows for an alternative source demonstration (ASD) in the event of an identified statistically significant increase (SSI) in a downgradient monitoring well over background levels:

The owner or operator may demonstrate that a source other than the CCR unit caused the statistically significant increase over background levels for a constituent or that the statistically significant increase resulted from error in sampling, analysis, statistical evaluation, or natural variation in groundwater quality. The owner or operator must complete the written demonstration within 90 days of detecting a statistically significant increase over background levels to include obtaining a certification from a qualified professional engineer verifying the accuracy of the information in the report.

The purpose of this work is to evaluate the data collected as part of the April 2018 monitoring event, along with historical data, to demonstrate if the identified SSIs are the results of a source other than the CCR unit or due to natural variation in groundwater quality, an error in sampling, analysis, or statistical evaluation.

2.0 April 2018 SSIs

Sampling for the first detection monitoring event was conducted on April 2-5, 2018. Four potential SSIs over background were identified: chloride at MW-105, sulfate and total dissolved solids (TDS) at MW-104, and fluoride at MW2-90.

Two methods of evaluation were subsequently undertaken in an effort to review potential alternative sources for the SSIs. These include the following evaluations:

- Comparison with leaching tests of CCR materials;
- Comparison with regional (background) groundwater quality data.

A successful alternative source demonstration is discussed in Section 3.0.

3.0 Alternative Source Demonstration

Methods used to evaluate potential alternative sources for the SSIs (fluoride at MW2-90, chloride at MW-105; and sulfate and TDS at MW-104) over background from the April 2018 detection monitoring event are discussed below.

3.1 Fluoride at MW2-90

The fluoride concentration in the sample from MW2-90 was detected at 1.03 mg/L during the April 2018 sampling event. The interwell prediction limit derived from baseline sampling is 0.93 mg/L. Verification resampling was conducted on August 13, 2018 for fluoride at MW2-90 to verify the potential SSI. The fluoride concentration observed at the verification resampling event (1.03 mg/L) was equal to the April 2018 event (1.03 mg/L), which exceeds the prediction limit. Therefore, the fluoride SSI was verified.

Two hypotheses were tested to evaluate the potential source of the fluoride concentrations observed at MW2-90. The first hypothesis evaluated was the CCR Unit is the source of fluoride at MW2-90 due to a release of leachate. To accept this hypothesis, it would be assumed that groundwater chemistry at MW2-90 would appear to be geochemically similar to that of impacted water from the CCR unit. However, if the comparison of the two types of water samples indicate that they are geochemically dissimilar, this indicates that a source "other than the CCR unit" is responsible for the SSI. Therefore, major ion chemistry from the CCR monitoring locations (upgradient and downgradient) were compared to CCR ash Synthetic Precipitation Leaching Procedure (SPLP method; EPA Method 1312) data collected July 2011.

The second hypothesis evaluated was that fluoride concentrations observed at MW2-90 are consistent with regional (background) groundwater data. To test this hypothesis, results of verification sampling were compared to regional groundwater quality data from the Cannonball Formation and associated units to determine if natural variation is a potential alternative source for the fluoride concentrations observed at MW2-90.

3.1.1 Source Hypothesis #1: CCR Unit Release

In order to test this hypothesis, Piper diagrams were used to visually compare the CCR SPLP results and the measured groundwater quality at the Site (Figure 2). Piper diagrams are plots of major ion chemistry of water samples (calcium, magnesium, potassium, sodium, chloride, sulfate, and alkalinity) that are used to differentiate between water types and to identify potential mixing of water types. This method is a means to identify or "fingerprint" water samples by their common characteristics (major ions) to assess which types of water are similar or dissimilar to potential CCR sources or non-source water types (Hensel and Hirsch, 2002).

Downgradient water quality (and of particular interest, at MW2-90) is characterized as a Ca/Mg-SO₄ type water, whereas the ash SPLP results are Na-SO₄ type water. The major difference observed between the downgradient water quality (MW2-90) and the SPLP results is the dominant cation concentration (calcium and magnesium vs. sodium). Because water quality data from MW2-90 is clustered with the upgradient wells rather than near the SPLP results, it indicates that the water chemistry at MW2-90 is more similar to

upgradient groundwater than a potential release from the CCR unit. **Therefore, we reject the hypothesis that the CCR Unit is the source of the fluoride observed at MW2-90.**

3.1.2 Source Hypothesis #2: Natural Variation of Regional Groundwater Quality

This hypothesis was tested by comparing fluoride concentrations collected as part of several regional groundwater quality studies on the Cannonball Formation and associated units. A summary of the range of fluoride concentrations in the Cannonball Formation and associated units are included in the table below.

Reference	Fluoride Conc. Range	Formation/Units	Data Source Location
Ackerman, D.J., 1980. Ground-Water Resources of Morton County, North Dakota. North Dakota Geological Survey Bulletin 72, Part III. 51 p.	0.0 to 4.0 mg/L	Cannonball and Ludlow formations, undifferentiated	Morton County
Robinove, C.J., Langford, R.H., Brookhart, J.W., 1958. Saline-Water Resources of North Dakota. USGS Water-Supply Paper 1428, 72 p.	0.0 to 6.5 mg/L	Hell Creek formation, Cannonball member of Fort Union Formation, and upper part of Fort Union Formation	Throughout North Dakota
Crosby, O.A. and Klausung, R.L., 1984. Hydrology of Area 47, Northern Great Plains and Rocky Mountain Coal Provinces, North Dakota, South Dakota, and Montana. USGS Water-Resources Investigations Open-File Report 83-221, 93 p.	0.1 to 6.3 mg/L	Entire Fort Union Formation (includes Cannonball Formation)	Morton County

The Ackerman study provides summary statistics for the fluoride concentrations observed in Morton County. Forty-six samples were analyzed for fluoride; of those, 20 (or 43%) had concentrations greater than 1.3 mg/L (Ackerman, 1980). The fluoride concentrations observed at MW2-90 are within the range of values consistent with naturally-occurring concentrations of fluoride associated with the Cannonball Formation in Morton County. **Therefore, we accept the hypothesis that fluoride concentrations observed at MW2-90 are consistent with regional (background) groundwater data.**

3.2 Other ASDs

Similar ASDs were documented for chloride at MW-105 and sulfate and TDS at MW-104 as part of the October 2017 ASD (Barr, 2018). Concentrations for these parameter-well pairs observed in April 2018 are similar to those observed in October 2017. The results of the ASD conducted in October 2017 are therefore valid for the April 2018 results. The previous ASD documented that each of the SSIs for these parameters can be explained by natural variability based on concentrations that were present at the Site before the landfill was constructed.

4.0 Conclusions

Four SSIs were identified from the April 2018 detection monitoring event. This report demonstrates that a “source other than the CCR unit” caused the SSIs, that the SSIs resulted from analytical error, or natural variation in groundwater quality, as allowed by §257.94(e)(2). The results of this alternative source demonstration are summarized in the table below.

Summary of SSIs and Alternative Sources

Well	Parameter	Report Section	Evidence for Alternative Source
MW2-90	Fluoride	3.1	Natural variability (geologic background)
MW-105	Chloride	3.2	Source other than CCR unit (water quality not consistent with samples from CCR unit, spatial trend inconsistent with hydraulic gradient), natural variability (pre-landfill values higher than current groundwater concentrations)
MW-104	Sulfate	3.2	Natural variability (pre-landfill values and geologic background)
MW-104	Total Dissolved Solids	3.2	Natural variability (pre-landfill values and geologic background)

Based on the foregoing, the alternative source demonstration presented herein meets the requirements of CCR Rule §257.94(e)(2).

5.0 References

Ackerman, D.J., 1980. Ground-Water Resources of Morton County, North Dakota. North Dakota Geological Survey Bulletin 72, Part III. 51 p.

Barr Engineering Co., 2018. Alternative Source Demonstration: October 2017 Event. R.M. Heskett Station. Prepared for Montana-Dakota Utilities Co. April 2018.

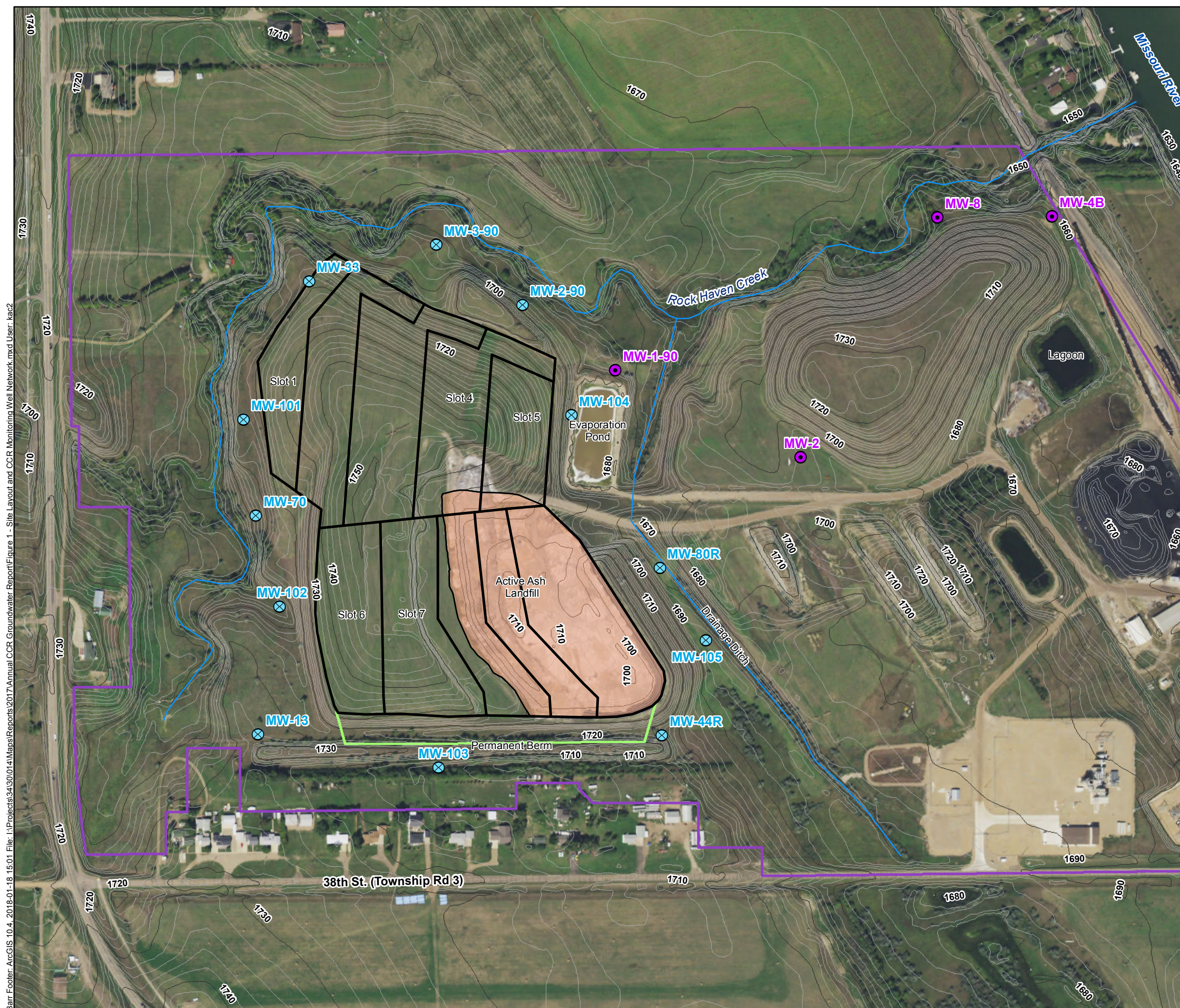
Crosby, O.A. and Klausning, R.L., 1984. Hydrology of Area 47, Northern Great Plains and Rocky Mountain Coal Provinces, North Dakota, South Dakota, and Montana. USGS Water-Resources Investigations Open-File Report 83-221, 93 p.

Hensel, D.R. and R. M. Hirsch, 2002. Statistical Methods in Water Resources Techniques of Water Resources Investigations, Book 4, chapter A3. U.S. Geological Survey. 522 pages.

Robinove, C.J., Langford, R.H., Brookhart, J.W., 1958. Saline-Water Resources of North Dakota. USGS Water-Supply Paper 1428, 72 p.

US EPA, 2015, Hazardous and Solid Waste Management Systems; Management of Coal Combustion Residuals From Electric Utility, CFR Parts 257 and 261 , Federal Register, Vol. 80, No. 74, April 17, 2015.

Figures



Barr Footer: ArcGIS 10.4, 2018-01-18 15:01 File: I:\Projects\3430\014\Maps\Reports\2017\Annual CCR Groundwater Report\Figure 1 - Site Layout and CCR Monitoring Well Network.mxd User: kac2



- Monitoring Well Location
- Monitoring Well Location - Water Level Only
- Existing Slot Boundaries
- Streams
- Property Line
- Future Landfill Boundary
- 10ft Contours
- 2ft Contours
- Active Portion of Landfill

Image Source: 2017 Statewide Imagery (ND GIS Hub)

CAD Data Source: Slot Linework.dwg

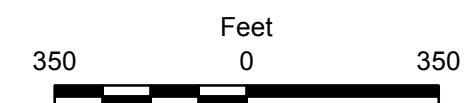
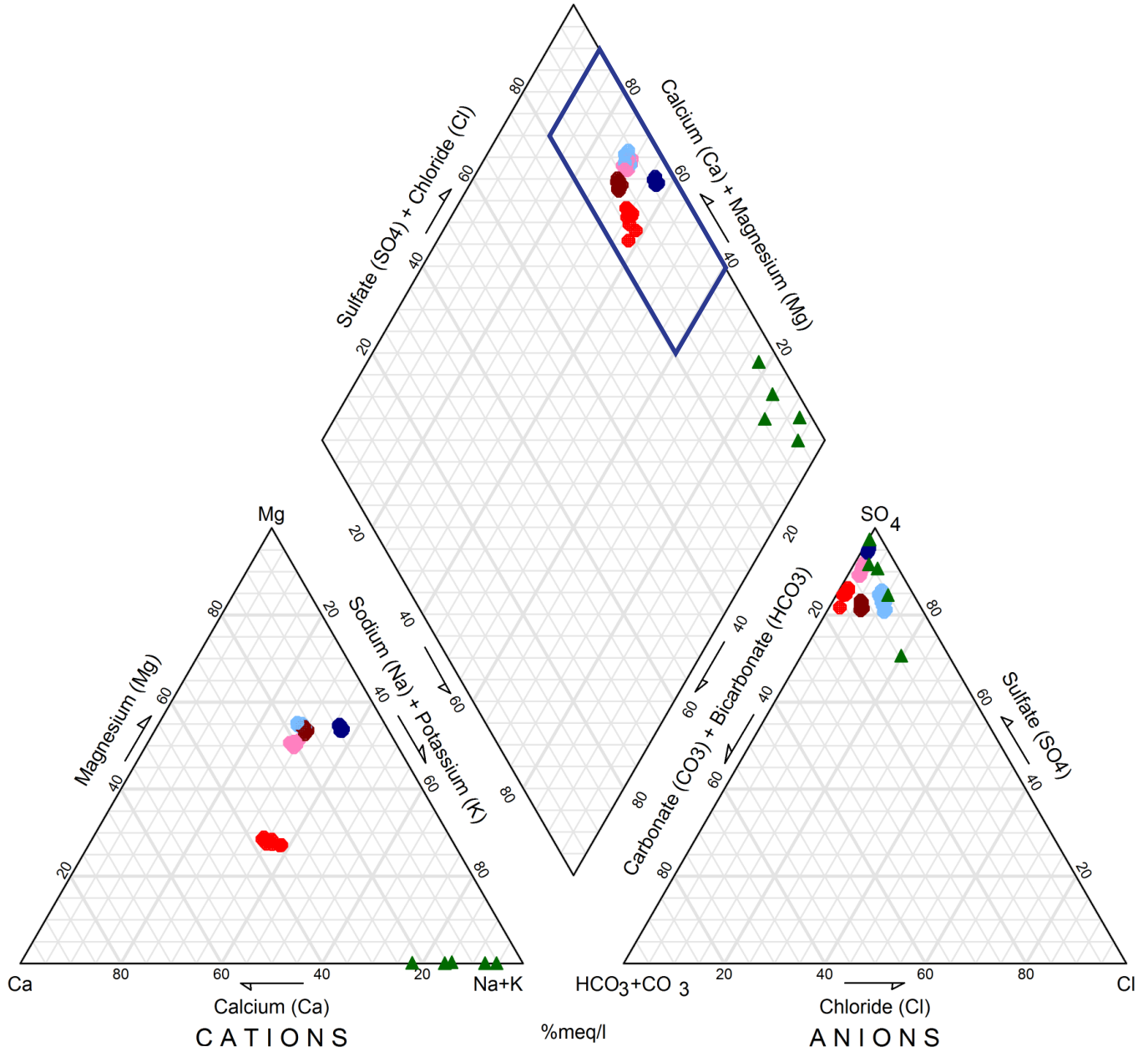


Figure 1

**SITE LAYOUT AND CCR
MONITORING WELL NETWORK
R. M. Heskett Station**

Montana Dakota Utilities
Mandan, North Dakota

Piper Diagram



- MW104
- MW105
- MW2-90
- MW3-90
- MW-80R
- Upgradient
- ▲ Ash SPLP

Figure 2
 PIPER PLOT
 R.M. Heskett Station
 Alternative Source Demonstration
 April 2017 Event
 Montana Dakota Utilities
 Mandan, North Dakota

Attachment 1

2011 Ash SPLP Laboratory Report



MINNESOTA VALLEY TESTING LABORATORIES, INC.

1126 North Front St. ~ New Ulm, MN 56073 ~ 800-782-3557 ~ Fax 507-359-2890
 2616 East Broadway Ave. ~ Bismarck, ND 58501 ~ 800-279-6885 ~ Fax 701-258-9724
 51 West Lincoln Way ~ Nevada, IA 50201 ~ 800-362-0855 ~ Fax 515-382-3885
 www.mvttl.com



Page: 1 of 2

Duane Leingang
 Montana Dakota Utilities
 PO Box 40
 Mandan ND 58554

Report Date: 8 Sep 11
 Lab Number: 11-M2450
 Work Order #: 81-818
 Account #: 013479
 Date Sampled:
 Date Received: 28 Jun 11 9:00
 PO #: 131460 OP

Sample Description: Unit I Bottom Ash
 Sample Site: MDU Heskett

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
SPLP Extraction				1312	22 Jul 11	SS
pH	12.2	units	N/A	SM4500 H+ B	22 Jul 11 17:00	Claudette
Specific Conductance	8778	umhos/cm	N/A	SM2510-B	22 Jul 11 17:00	Claudette
Total Suspended Solids	3	mg/l	1	SM2540-D	22 Jul 11 14:00	CLB
Total Alkalinity	1120	mg/l CaCO3	4	SM2320-B	22 Jul 11 17:00	Claudette
Phenolphthalein Alk	1090	mg/l CaCO3	4	SM2320-B	22 Jul 11 17:00	Claudette
Bicarbonate	< 4	mg/l CaCO3	4	SM2320-B	22 Jul 11 17:00	Claudette
Carbonate	60	mg/l CaCO3	4	SM2320-B	22 Jul 11 17:00	Claudette
Hydroxide	1060	mg/l CaCO3	0	SM2320-B	22 Jul 11 17:00	Claudette
Tot Dis Solids (Summation)	4860	mg/l	NA	SM1030-F	3 Aug 11 8:40	Calculated
Total Hardness as CaCO3	524	mg/l	NA	SM2340-B	3 Aug 11 8:40	Calculated
Hardness in grains/gallon	30.7	gr/gal	NA	SM2340-B	3 Aug 11 8:40	Calculated
Cation Summation	74.3	meq/L	NA	SM1030-F	3 Aug 11 8:40	Calculated
Anion Summation	74.6	meq/L	NA	SM1030-F	28 Jul 11 14:30	Calculated
Percent Error	-0.24	%	NA	SM1030-F	3 Aug 11 8:40	Calculated
Sodium Adsorption Ratio	27.1		NA	USDA 20b	3 Aug 11 8:40	Calculated
Gross Alpha Radiation	Attached	pCi/l			22 Aug 11 2:03	
Radon 222	Attached				28 Jul 11 4:37	
Radium 226	Attached	pCi/l			22 Aug 11 22:20	
Radium 228	Attached	pCi/l			16 Aug 11 16:50	
Total Organic Carbon	0.7	mg/l	0.5	SM5310-C	1 Aug 11 8:00	Eric
Fluoride	< 0.1	mg/l	0.10	SM4500-F-C	4 Aug 11 17:00	CLB
Sulfate	2440	mg/l	5.00	ASTM D516-02	27 Jul 11 9:00	KMP
Chloride	50.5	mg/l	1.0	SM4500-Cl-E	27 Jul 11 14:00	KMP
Nitrate-Nitrite as N	0.21	mg/l	0.10	EPA 353.2	28 Jul 11 14:30	KMP
Ammonia-Nitrogen as N	0.32	mg/l	0.10	EPA 350.1	28 Jul 11 10:45	KMP
Phosphorus as P - Total	< 0.1	mg/l	0.10	EPA 365.1	28 Jul 11 13:00	KMP
Mercury - Total	< 0.0002	mg/l	0.0002	EPA 245.1	28 Jul 11 8:00	Eric
Chemical Oxygen Demand	< 5	mg/l	5.0	HACH 8000	1 Aug 11 8:30	Wayne
Calcium - Total	210	mg/l	1.0	6010	3 Aug 11 8:40	Stacy
Magnesium - Total	< 2.5	mg/l	1.0	6010	3 Aug 11 8:40	Stacy
Sodium - Total	1440	mg/l	1.0	6010	3 Aug 11 8:40	Stacy
Potassium - Total	44.8	mg/l	1.0	6010	3 Aug 11 8:40	Stacy
Aluminum - Total	< 0.5	mg/l	0.10	6010	2 Aug 11 9:30	Stacy
Iron - Total	< 0.5	mg/l	0.10	6010	2 Aug 11 9:30	Stacy
Strontium - Total	28.2	mg/l	0.10	6010	2 Aug 11 9:30	Stacy
Titanium - Total	< 0.5	mg/l	0.10	6010	2 Aug 11 9:30	Stacy
Boron - Total	< 0.5	mg/l	0.10	6010	11 Aug 11 8:40	Stacy

RL = Method Reporting Limit

Elevated "Less Than Result" (<): @ = Due to sample matrix
 ! = Due to sample quantity

= Due to sample concentration
 + = Due to extract volume

CERTIFICATION: MN LAB # 038-999-267 ND # ND-00016



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1126 North Front St. ~ New Ulm, MN 56073 ~ 800-782-3557 ~ Fax 507-359-2890
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www.mvttl.com



Page: 2 of 2


Duane Leingang
Montana Dakota Utilities
PO Box 40
Mandan ND 58554

Report Date: 8 Sep 11
Lab Number: 11-M2450
Work Order #: 81-818
Account #: 013479
Date Sampled:
Date Received: 28 Jun 11 9:00
PO #: 131460 OP

Sample Description: Unit I Bottom Ash
Sample Site: MDU Heskett

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
Antimony - Total	< 0.002	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Arsenic - Total	0.0044	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Barium - Total	0.1135	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Beryllium - Total	< 0.001	mg/l	0.0010	6020	25 Jul 11 16:18	Claudette
Cadmium - Total	0.00164	mg/l	0.00100	6020	25 Jul 11 16:18	Claudette
Chromium - Total	0.0065	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Cobalt - Total	< 0.002	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Copper - Total	0.0213	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Lead - Total	< 0.002	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Manganese - Total	0.0027	mg/l	0.0010	6020	25 Jul 11 16:18	Claudette
Molybdenum - Total	0.6860	mg/l	0.0020	6020	26 Jul 11 12:46	Claudette
Nickel - Total	0.0074	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Selenium - Total	0.0133	mg/l	0.0020	6020	26 Jul 11 9:46	Claudette
Silver - Total	< 0.001	mg/l	0.0010	6020	25 Jul 11 16:18	Claudette
Thallium - Total	< 0.002	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Tin - Total	< 0.05	mg/l	0.0500	6020	25 Jul 11 16:18	Claudette
Vanadium - Total	0.0189	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Zinc - Total	0.0151	mg/l	0.0100	6020	25 Jul 11 16:18	Claudette
Uranium	< 0.002	mg/l	0.002	6020	25 Jul 11 16:18	Claudette

All analyses were performed on the extract from Method 1312 (SPLP) with a modified solution to solids ratio of 4:1.

Approved by: 

RL = Method Reporting Limit

Elevated "Less Than Result" (<): @ = Due to sample matrix
! = Due to sample quantity

= Due to sample concentration
+ = Due to extract volume

CERTIFICATION: MN LAB # 038-999-267 ND # ND-00016



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Page: 1 of 2

Duane Leingang
 Montana Dakota Utilities
 PO Box 40
 Mandan ND 58554

Report Date: 8 Sep 11
 Lab Number: 11-M2451
 Work Order #: 81-818
 Account #: 013479
 Date Sampled:
 Date Received: 28 Jun 11 9:00
 PO #: 131460 OP

Sample Description: Unit II Sand Ash
 Sample Site: MDU Heskett

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
SPLP Extraction				1312	22 Jul 11	SS
pH	11.1	units	N/A	SM4500 H+ B	22 Jul 11 17:00	Claudette
Specific Conductance	20110	umhos/cm	N/A	SM2510-B	22 Jul 11 17:00	Claudette
Total Suspended Solids	21	mg/l	1	SM2540-D	22 Jul 11 14:00	CLB
Total Alkalinity	203	mg/l CaCO3	4	SM2320-B	22 Jul 11 17:00	Claudette
Phenolphthalein Alk	171	mg/l CaCO3	4	SM2320-B	22 Jul 11 17:00	Claudette
Bicarbonate	< 4	mg/l CaCO3	4	SM2320-B	22 Jul 11 17:00	Claudette
Carbonate	64	mg/l CaCO3	4	SM2320-B	22 Jul 11 17:00	Claudette
Hydroxide	139	mg/l CaCO3	0	SM2320-B	22 Jul 11 17:00	Claudette
Tot Dis Solids(Summation)	22500	mg/l	NA	SM1030-F	3 Aug 11 8:40	Calculated
Total Hardness as CaCO3	1200	mg/l	NA	SM2340-B	3 Aug 11 8:40	Calculated
Hardness in grains/gallon	70.2	gr/gal	NA	SM2340-B	3 Aug 11 8:40	Calculated
Cation Summation	318	meq/L	NA	SM1030-F	3 Aug 11 8:40	Calculated
Anion Summation	314	meq/L	NA	SM1030-F	28 Jul 11 14:30	Calculated
Percent Error	0.65	%	NA	SM1030-F	3 Aug 11 8:40	Calculated
Sodium Adsorption Ratio	80.9		NA	USDA 20b	3 Aug 11 8:40	Calculated
Gross Alpha Radiation	Attached	pCi/l			22 Aug 11 2:03	
Radon 222	See Attached				28 Jul 11 4:37	
Radium 226	Attached	pCi/l			22 Aug 11 22:20	
Radium 228	Attached	pCi/l			16 Aug 11 16:50	
Total Organic Carbon	< 0.5	mg/l	0.5	SM5310-C	1 Aug 11 8:00	Eric
Fluoride	< 0.1	mg/l	0.10	SM4500-F-C	4 Aug 11 17:00	CLB
Sulfate	14900	mg/l	5.00	ASTM D516-02	27 Jul 11 9:00	KMP
Chloride	2.0	mg/l	1.0	SM4500-Cl-E	27 Jul 11 14:00	KMP
Nitrate-Nitrite as N	< 0.1	mg/l	0.10	EPA 353.2	28 Jul 11 14:30	KMP
Ammonia-Nitrogen as N	0.10	mg/l	0.10	EPA 350.1	28 Jul 11 10:45	KMP
Phosphorus as P - Total	< 0.1	mg/l	0.10	EPA 365.1	28 Jul 11 13:00	KMP
Mercury - Total	< 0.0002	mg/l	0.0002	EPA 245.1	28 Jul 11 8:00	Eric
Chemical Oxygen Demand	< 5	mg/l	5.0	HACH 8000	1 Aug 11 8:30	Wayne
Calcium - Total	481	mg/l	1.0	6010	3 Aug 11 8:40	Stacy
Magnesium - Total	< 5	mg/l	1.0	6010	3 Aug 11 8:40	Stacy
Sodium - Total	6500	mg/l	1.0	6010	3 Aug 11 8:40	Stacy
Potassium - Total	459	mg/l	1.0	6010	3 Aug 11 8:40	Stacy
Aluminum - Total	1.09	mg/l	0.10	6010	2 Aug 11 9:30	Stacy
Iron - Total	< 1	mg/l	0.10	6010	2 Aug 11 9:30	Stacy
Strontium - Total	66.0	mg/l	0.10	6010	2 Aug 11 9:30	Stacy
Titanium - Total	< 1	mg/l	0.10	6010	2 Aug 11 9:30	Stacy
Boron - Total	5.96	mg/l	0.10	6010	11 Aug 11 8:40	Stacy

RL = Method Reporting Limit

Elevated "Less Than Result" (<): @ = Due to sample matrix
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CERTIFICATION: MN LAB # 038-999-267 ND # ND-00016



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Duane Leingang
Montana Dakota Utilities
PO Box 40
Mandan ND 58554

Report Date: 8 Sep 11
Lab Number: 11-M2451
Work Order #: 81-818
Account #: 013479
Date Sampled:
Date Received: 28 Jun 11 9:00
PO #: 131460 OP

Sample Description: Unit II Sand Ash
Sample Site: MDU Heskett

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
Antimony - Total	< 0.002	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Arsenic - Total	0.0822	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Barium - Total	0.0930	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Beryllium - Total	< 0.001	mg/l	0.0010	6020	25 Jul 11 16:18	Claudette
Cadmium - Total	0.00182	mg/l	0.00100	6020	25 Jul 11 16:18	Claudette
Chromium - Total	0.0244	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Cobalt - Total	< 0.002	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Copper - Total	0.1108	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Lead - Total	< 0.002	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Manganese - Total	0.0052	mg/l	0.0010	6020	25 Jul 11 16:18	Claudette
Molybdenum - Total	0.1000	mg/l	0.0020	6020	26 Jul 11 12:46	Claudette
Nickel - Total	0.0136	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Selenium - Total	0.0937	mg/l	0.0020	6020	26 Jul 11 9:46	Claudette
Silver - Total	< 0.001	mg/l	0.0010	6020	25 Jul 11 16:18	Claudette
Thallium - Total	< 0.002	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Tin - Total	< 0.05	mg/l	0.0500	6020	25 Jul 11 16:18	Claudette
Vanadium - Total	0.3026	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Zinc - Total	0.0327	mg/l	0.0100	6020	25 Jul 11 16:18	Claudette
Uranium	< 0.002	mg/l	0.002	6020	25 Jul 11 16:18	Claudette

All analyses were performed on the extract from Method 1312 (SPLP) with a modified solution to solids ratio of 4:1.

Approved by:

RL = Method Reporting Limit

Elevated "Less Than Result" (<): @ = Due to sample matrix
! = Due to sample quantity

= Due to sample concentration
+ = Due to extract volume

CERTIFICATION: MN LAB # 038-999-267 ND # ND-00016



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Page: 1 of 2

Duane Leingang
 Montana Dakota Utilities
 PO Box 40
 Mandan ND 58554

Report Date: 8 Sep 11
 Lab Number: 11-M2452
 Work Order #: 81-818
 Account #: 013479
 Date Sampled:
 Date Received: 28 Jun 11 9:00
 PO #: 131460 OP

Sample Description: Unit I Fly Ash
 Sample Site: MDU Heskett

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
SPLP Extraction				1312	22 Jul 11	SS
pH	12.9	units	N/A	SM4500 H+ B	22 Jul 11 17:00	Claudette
Specific Conductance	50660	umhos/cm	N/A	SM2510-B	22 Jul 11 17:00	Claudette
Total Suspended Solids	30	mg/l	1	SM2540-D	22 Jul 11 14:00	CLB
Total Alkalinity	7020	mg/l CaCO3	4	SM2320-B	25 Jul 11 17:00	Claudette
Phenolphthalein Alk	6900	mg/l CaCO3	4	SM2320-B	25 Jul 11 17:00	Claudette
Bicarbonate	< 4	mg/l CaCO3	4	SM2320-B	25 Jul 11 17:00	Claudette
Carbonate	240	mg/l CaCO3	4	SM2320-B	25 Jul 11 17:00	Claudette
Hydroxide	6780	mg/l CaCO3	0	SM2320-B	25 Jul 11 17:00	Claudette
Tot Dis Solids (Summation)	42200	mg/l	NA	SM1030-F	3 Aug 11 8:40	Calculated
Total Hardness as CaCO3	1750	mg/l	NA	SM2340-B	3 Aug 11 8:40	Calculated
Hardness in grains/gallon	102	gr/gal	NA	SM2340-B	3 Aug 11 8:40	Calculated
Cation Summation	663	meq/L	NA	SM1030-F	3 Aug 11 8:40	Calculated
Anion Summation	613	meq/L	NA	SM1030-F	28 Jul 11 14:30	Calculated
Percent Error	3.99	%	NA	SM1030-F	3 Aug 11 8:40	Calculated
Sodium Adsorption Ratio	143		NA	USDA 20b	3 Aug 11 8:40	Calculated
Gross Alpha Radiation	Attached	pCi/l			22 Aug 11 2:03	
Radon 222	Attached				28 Jul 11 4:37	
Radium 226	Attached	pCi/l			22 Aug 11 22:20	
Radium 228	Attached	pCi/l			16 Aug 11 16:50	
Total Organic Carbon	1.5	mg/l	0.5	SM5310-C	1 Aug 11 8:00	Eric
Fluoride	5.60	mg/l	0.10	SM4500-F-C	10 Aug 11 17:00	CLB
Sulfate	22600	mg/l	5.00	ASTM D516-02	27 Jul 11 9:00	KMP
Chloride	53.8	mg/l	1.0	SM4500-Cl-E	27 Jul 11 14:00	KMP
Nitrate-Nitrite as N	0.68	mg/l	0.10	EPA 353.2	28 Jul 11 14:30	KMP
Ammonia-Nitrogen as N	7.22	mg/l	0.10	EPA 350.1	28 Jul 11 10:45	KMP
Phosphorus as P - Total	< 0.1	mg/l	0.10	EPA 365.1	28 Jul 11 13:00	KMP
Mercury - Total	< 0.0002	mg/l	0.0002	EPA 245.1	28 Jul 11 8:00	Eric
Chemical Oxygen Demand	22.4	mg/l	5.0	HACH 8000	1 Aug 11 8:30	Wayne
Calcium - Total	700	mg/l	1.0	6010	3 Aug 11 8:40	Stacy
Magnesium - Total	< 25	mg/l	1.0	6010	3 Aug 11 8:40	Stacy
Sodium - Total	14100	mg/l	1.0	6010	3 Aug 11 8:40	Stacy
Potassium - Total	580	mg/l	1.0	6010	3 Aug 11 8:40	Stacy
Aluminum - Total	< 5	mg/l	0.10	6010	2 Aug 11 9:30	Stacy
Iron - Total	< 5	mg/l	0.10	6010	2 Aug 11 9:30	Stacy
Strontium - Total	59.5	mg/l	0.10	6010	2 Aug 11 9:30	Stacy
Titanium - Total	< 5	mg/l	0.10	6010	2 Aug 11 9:30	Stacy
Boron - Total	1.89	mg/l	0.10	6010	11 Aug 11 8:40	Stacy

RL = Method Reporting Limit

Elevated "Less Than Result" (<): @ = Due to sample matrix
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= Due to sample concentration
 + = Due to extract volume

CERTIFICATION: MN LAB # 038-999-267

ND # ND-00016



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Page: 2 of 2

Duane Leingang
Montana Dakota Utilities
PO Box 40
Mandan ND 58554

Report Date: 8 Sep 11
Lab Number: 11-M2452
Work Order #: 81-818
Account #: 013479
Date Sampled:
Date Received: 28 Jun 11 9:00
PO #: 131460 OP

Sample Description: Unit I Fly Ash
Sample Site: MDU Heskett

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
Antimony - Total	< 0.002	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Arsenic - Total	0.1128	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Barium - Total	0.0906	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Beryllium - Total	< 0.001	mg/l	0.0010	6020	25 Jul 11 16:18	Claudette
Cadmium - Total	0.00244	mg/l	0.00100	6020	25 Jul 11 16:18	Claudette
Chromium - Total	0.0270	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Cobalt - Total	< 0.002	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Copper - Total	0.2934	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Lead - Total	0.0161	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Manganese - Total	0.0102	mg/l	0.0010	6020	25 Jul 11 16:18	Claudette
Molybdenum - Total	0.9246	mg/l	0.0020	6020	26 Jul 11 12:46	Claudette
Nickel - Total	0.0175	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Selenium - Total	0.1959	mg/l	0.0020	6020	26 Jul 11 9:46	Claudette
Silver - Total	< 0.001	mg/l	0.0010	6020	25 Jul 11 16:18	Claudette
Thallium - Total	< 0.002	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Tin - Total	< 0.05	mg/l	0.0500	6020	25 Jul 11 16:18	Claudette
Vanadium - Total	0.0158	mg/l	0.0020	6020	25 Jul 11 16:18	Claudette
Zinc - Total	0.3984	mg/l	0.0100	6020	25 Jul 11 16:18	Claudette
Uranium	< 0.002	mg/l	0.002	6020	25 Jul 11 16:18	Claudette

All analyses were performed on the extract from Method 1312 (SPLP) with a modified solution to solids ratio of 4:1.

Approved by: *D. Jordan*

RL = Method Reporting Limit

Elevated "Less Than Result" (<): @ = Due to sample matrix
! = Due to sample quantity

= Due to sample concentration
+ = Due to extract volume

CERTIFICATION: MN LAB # 038-999-267 ND # ND-00016



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Page: 1 of 2

Duane Leingang
 Montana Dakota Utilities
 PO Box 40
 Mandan ND 58554

Report Date: 8 Sep 11
 Lab Number: 11-M2453
 Work Order #: 81-818
 Account #: 013479
 Date Sampled:
 Date Received: 28 Jun 11 9:00
 PO #: 131460 OP

Sample Description: Unit II Fly Ash
 Sample Site: MDU Heskett

	As Received Result		Method RL	Method Reference	Date Analyzed	Analyst
SPLP Extraction				1312	22 Jul 11	SS
pH	12.8	units	N/A	SM4500 H+ B	22 Jul 11 17:00	Claudette
Specific Conductance	27240	umhos/cm	N/A	SM2510-B	22 Jul 11 17:00	Claudette
Total Suspended Solids	13	mg/l	1	SM2540-D	22 Jul 11 14:00	CLB
Total Alkalinity	4570	mg/l CaCO3	4	SM2320-B	22 Jul 11 17:00	Claudette
Phenolphthalein Alk	4520	mg/l CaCO3	4	SM2320-B	22 Jul 11 17:00	Claudette
Bicarbonate	< 4	mg/l CaCO3	4	SM2320-B	22 Jul 11 17:00	Claudette
Carbonate	100	mg/l CaCO3	4	SM2320-B	22 Jul 11 17:00	Claudette
Hydroxide	4470	mg/l CaCO3	0	SM2320-B	22 Jul 11 17:00	Claudette
Tot Dis Solids(Summation)	16000	mg/l	NA	SM1030-F	3 Aug 11 8:40	Calculated
Total Hardness as CaCO3	1960	mg/l	NA	SM2340-B	3 Aug 11 8:40	Calculated
Hardness in grains/gallon	115	gr/gal	NA	SM2340-B	3 Aug 11 8:40	Calculated
Cation Summation	252	meq/L	NA	SM1030-F	9 Aug 11 9:09	Calculated
Anion Summation	247	meq/L	NA	SM1030-F	28 Jul 11 14:30	Calculated
Percent Error	1.00	%	NA	SM1030-F	9 Aug 11 9:09	Calculated
Sodium Adsorption Ratio	46.1		NA	USDA 20b	3 Aug 11 8:40	Calculated
Gross Alpha Radiation	Attached	pCi/l			22 Aug 11 2:03	
Radon 222	Attached				28 Jul 11 4:37	
Radium 226	Attached	pCi/l			22 Aug 11 22:20	
Radium 228	Attached	pCi/l			16 Aug 11 16:50	
Total Organic Carbon	1.6	mg/l	0.5	SM5310-C	1 Aug 11 8:00	Eric
Fluoride	3.60	mg/l	0.10	SM4500-F-C	4 Aug 11 17:00	CLB
Sulfate	7400	mg/l	5.00	ASTM D516-02	27 Jul 11 9:00	KMP
Chloride	66.0	mg/l	1.0	SM4500-Cl-E	27 Jul 11 14:00	KMP
Nitrate-Nitrite as N	0.38	mg/l	0.10	EPA 353.2	28 Jul 11 14:30	KMP
Ammonia-Nitrogen as N	15.0	mg/l	0.10	EPA 350.1	28 Jul 11 10:45	KMP
Phosphorus as P - Total	< 0.1	mg/l	0.10	EPA 365.1	28 Jul 11 13:00	KMP
Mercury - Total	< 0.0002	mg/l	0.0002	EPA 245.1	28 Jul 11 8:00	Eric
Chemical Oxygen Demand	9.4	mg/l	5.0	HACH 8000	1 Aug 11 8:30	Wayne
Calcium - Total	785	mg/l	1.0	6010	3 Aug 11 8:40	Stacy
Magnesium - Total	< 5	mg/l	1.0	6010	3 Aug 11 8:40	Stacy
Sodium - Total	4720	mg/l	1.0	6010	3 Aug 11 8:40	Stacy
Potassium - Total	275	mg/l	1.0	6010	3 Aug 11 8:40	Stacy
Aluminum - Total	< 1	mg/l	0.10	6010	9 Aug 11 9:09	Stacy
Iron - Total	< 1	mg/l	0.10	6010	9 Aug 11 9:09	Stacy
Strontium - Total	85.0	mg/l	0.10	6010	9 Aug 11 9:09	Stacy
Titanium - Total	< 1	mg/l	0.10	6010	9 Aug 11 9:09	Stacy
Boron - Total	< 1	mg/l	0.10	6010	11 Aug 11 8:40	Stacy

RL = Method Reporting Limit

Elevated "Less Than Result" (<): @ = Due to sample matrix
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= Due to sample concentration
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CERTIFICATION: MN LAB # 038-999-267 ND # ND-00016